



COMUNE DI VALGUARNERA C.

Libero Consorzio Comunale di Enna

LAVORI DI RISTRUTTURAZIONE DELL'ASILO NIDO DI CONTRADA MONTAGNA PROGETTO ESECUTIVO

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Il Progettista



Il Responsabile Unico
del Procedimento



Ing. Vittorio Giarratana

VISTI E PARERI

Sono illustrati con la presente i risultati dei calcoli che riguardano il progetto delle armature, la verifica delle tensioni di lavoro dei materiali e del terreno.

• **NORMATIVA DI RIFERIMENTO**

I calcoli sono condotti nel pieno rispetto della normativa vigente e, in particolare, la normativa cui viene fatto riferimento nelle fasi di calcolo, verifica e progettazione è costituita dalle *Norme Tecniche per le Costruzioni*, emanate con il D.M. 17/01/2018 pubblicato nel suppl. 8 G.U. 42 del 20/02/2018, nonché la Circolare del Ministero Infrastrutture e Trasporti del 21 Gennaio 2019, n. 7 “*Istruzioni per l'applicazione delle nuove norme tecniche per le costruzioni*”.

Per il calcolo delle strutture in oggetto si adotteranno i criteri della Geotecnica e della Scienza delle Costruzioni.

• **CAPACITÀ PORTANTE DI FONDAZIONI SUPERFICIALI**

La verifica della capacità portante consiste nel confronto tra la pressione verticale di esercizio in fondazione e la pressione limite per il terreno, valutata secondo *Brinch-Hansen*:

$$q_{lim} = q N_q Y_q i_q d_q b_q g_q s_q + c N_c Y_c i_c d_c b_c g_c s_c + \frac{1}{2} G B' N_g Y_g i_g b_g s_g$$

dove

Caratteristiche geometriche della fondazione:

q = carico sul piano di fondazione
 B = lato minore della fondazione
 L = lato maggiore della fondazione
 D = profondità della fondazione
 α = inclinazione base della fondazione
 G = peso specifico del terreno
 B' = larghezza di fondazione ridotta = $B - 2 e_B$
 L' = lunghezza di fondazione ridotta = $L - 2 e_L$

Caratteristiche di carico sulla fondazione:

H = risultante delle forze orizzontali
 N = risultante delle forze verticali
 e_B = eccentricità del carico verticale lungo B
 e_L = eccentricità del carico verticale lungo L
 F_{hB} = forza orizzontale lungo B
 F_{hL} = forza orizzontale lungo L

Caratteristiche del terreno di fondazione:

β = inclinazione terreno a valle
 $c = c_u$ = coesione non drenata (condizioni U)
 $c = c'$ = coesione drenata (condizioni D)
 Γ = peso specifico apparente (condizioni U)
 $\Gamma = \Gamma'$ = peso specifico sommerso (condizioni D)
 $\phi = 0$ = angolo di attrito interno (condizioni U)
 $\phi = \phi'$ = angolo di attrito interno (condizioni D)

Fattori di capacità portante:

$$N_q = \tan^2\left(\frac{\pi}{4} + \frac{\phi}{2}\right) \exp(\pi \cdot \tan \phi) \quad (\text{Prandtl-Cauchy-Meyerhof})$$

$$Nq = 2(Nq + 1) \tan \phi \quad (\text{Vesic})$$

$$Nc = \frac{Nq - 1}{\tan \phi} \quad \text{in condizioni D} \quad (\text{Reissner-Meyerhof})$$

$$Nc = 5,14 \quad \text{in condizioni U}$$

Indici di rigidezza (condizioni D):

$$Ir = \frac{G}{c' + q' \tan \phi} = \text{indice di rigidezza}$$

$$q' = \text{pressione litostatica efficace alla profondità } D + \frac{B}{2}$$

$$G = \frac{E}{2(1 + \mu)} = \text{modulo elastico tangenziale}$$

$$E = \text{modulo elastico normale}$$

$$\mu = \text{coefficiente di Poisson}$$

$$Icr = \frac{1}{2} \exp \left[\frac{3,3 - 0,45 \frac{B}{L}}{\tan(45 - \frac{\phi'}{2})} \right] = \text{indice di rigidezza critico}$$

Coefficienti di punzonamento (Vesic):

$$Yq = Yg = \exp \left[\left(0,6 \frac{B}{L} - 4,4 \right) \tan \phi' + \frac{3,07 \sin \phi' \log(2Ir)}{1 + \sin \phi'} \right] \text{ in condizioni drenate, per } Ir \leq Icr$$

$$Yc = Yq - \frac{1 - Yq}{Nq \times \tan \phi'}$$

Coefficienti di inclinazione del carico (Vesic):

$$ig = \left(\frac{1 - H}{N + B \times L \times c' \times \cot \text{ang} \phi'} \right)^{m+1}$$

$$iq = \left(\frac{1 - H}{N + B \times L \times c' \times \cot \phi'} \right)^m$$

$$ic = iq - \frac{1 - iq}{Nc \times \tan \phi'} \quad \text{in condizioni D}$$

$$ic = 1 - \frac{m \times H}{B \times L \times cu \times Nc} \quad \text{in condizioni U}$$

essendo:

$$m = mB \cos^2 \Theta + mL \sin^2 \Theta$$

$$mB = \frac{2 + \frac{B'}{L'}}{1 + \frac{B'}{L'}} \quad mL = \frac{2 + \frac{L'}{B'}}{1 + \frac{L'}{B'}} \quad \Theta = \tan^{-1} \frac{Fh \times B}{Fh \times L}$$

Coefficienti di affondamento del piano di posa (Brinch-Hansen):

$$dq = 1 + 2 \tan \phi (1 - \sin \phi)^2 \arctg \frac{D}{B'} \quad \text{per } D > B'$$

$$dq = 1 + 2 \frac{D}{B'} \tan \phi (1 - \sin \phi)^2 \quad \text{per } D \leq B'$$

$$dc = dq - \frac{1 - dq}{Nc \times \tan \phi} \quad \text{in condizioni D}$$

$$dc = 1 + 0,4 \arctan \frac{D}{B'} \quad \text{per } D > B' \text{ in condizioni U}$$

$$dc = 1 + 0,4 \frac{D}{B'} \quad \text{per } D \leq B' \text{ in condizioni U}$$

Coefficienti di inclinazione del piano di posa:

$$bg = \exp(-2,7\alpha \tan \phi)$$

$$bc = bq = \exp(-2\alpha \tan \phi) \quad \text{in condizioni D}$$

$$bc = 1 - \frac{\alpha}{147} \quad \text{in condizioni U}$$

$$bq = 1 \quad \text{in condizioni U)}$$

Coefficienti di inclinazione del terreno di fondazione:

$$gc = gq = \sqrt{1 - 0,5 \tan \beta} \quad \text{in condizioni D}$$

$$gc = 1 - \frac{\beta}{147} \quad \text{in condizioni U}$$

$$gq = 1 \quad \text{in condizioni U}$$

Coefficienti di forma (De Beer):

$$sg = 1 - 0,4 \frac{B'}{L'}$$

$$sq = 1 + \frac{B'}{L'} \tan \phi$$

$$sc = 1 + \frac{B' Nq}{L' Nc}$$

L'azione del sisma si traduce in accelerazioni nel sottosuolo (effetto cinematico) e nella fondazione, per l'azione delle forze d'inerzia generate nella struttura in elevazione (effetto inerziale). Tali effetti possono essere portati in conto mediante l'introduzione di coefficienti sismici rispettivamente denominati K_{hi} e I_{gk} , il primo definito dal rapporto tra le componenti orizzontale e verticale dei carichi trasmessi in fondazione ed il secondo funzione dell'accelerazione massima attesa al sito. L'effetto inerziale produce variazioni di tutti i coefficienti di capacità portante del carico limite in funzione del coefficiente sismico K_{hi} e viene portato in conto impiegando le formule comunemente adottate per calcolare i coefficienti correttivi del carico limite in funzione dell'inclinazione, rispetto alla verticale, del carico agente sul piano di posa. Nel caso in cui sia stato attivato il flag per tener conto degli effetti cinematici il valore I_{gk} modifica invece il solo coefficiente N_g ; il fattore N_g viene infatti moltiplicato sia per il coefficiente correttivo dell'effetto inerziale, sia per il coefficiente correttivo per l'effetto cinematico.

• CAPACITÀ PORTANTE DI FONDAZIONI SU PALI

a) Pali resistenti a compressione

Il carico ultimo del palo a compressione risulta:

$$Q_{lim} = Q_{punta} + Q_{later} - P_{palo} - P_{attr_neg}$$

Q_{punta}: RESISTENZA ALLA PUNTA

- In terreni coesivi in condizioni non drenate:

$$Q_{punta} = (C_{up} \times N_c + \sigma_v) \times A_p \times R_c$$

essendo

Cup = coesione non drenata terreno alla quota della punta

Nc = coeff. di capacità portante = 9

σ_v = tensione verticale totale in punta

Ap = area della punta del palo

Rc = coeff. di *Meyerhof* per le argille S/C

$$Rc = \frac{D+1}{2D+1} \quad \text{per pali trivellati} \qquad Rc = \frac{D+0,5}{2D} \quad \text{per pali infissi}$$

D = diametro del palo

- In terreni coesivi in condizioni drenate (secondo *Vesic*):

$$Q_{\text{punta}} = (\mu \times \sigma'_v \times Nq + c' \times Nc) \times Ap$$

essendo

$$\mu = \frac{1 + 2(1 - \sin \phi')}{3}$$

$$Nq = \frac{3}{3 - \sin \phi'} \exp \left[\left(\left(\frac{\pi}{2} - \phi' \right) \tan \phi' \right) \tan^2 \left(\frac{\pi}{4} + \frac{\phi'}{2} \right) \times Irr^{\frac{4 \sin \phi'}{3(1 + \sin \phi')}} \right]$$

Irr = indice di rigidezza ridotta

$$Irr \approx Ir = \text{indice di rigidezza} = \frac{G}{c' + \sigma'_v \tan \phi'}$$

G = modulo elastico di taglio

σ'_v = tensione verticale efficace in punta

$$Nc = (Nq - 1) \cot \phi'$$

- In terreni incoerenti (secondo *Berezantzev*):

$$Q_{\text{punta}} = \sigma'_v \times \alpha q \times Nq \times Ap$$

essendo

αq = coeff. di riduzione per effetto silos in funzione di L/D

Nq = calcolato con ϕ^* secondo *Kishida*:

$$\phi^* = \phi' - 3^\circ$$

pali trivellati

$$\phi^* = (\phi' + 40^\circ) / 2$$

per pali infissi

per

L = lunghezza del palo

Qlater: RESISTENZA LATERALE

- In terreni coesivi in condizioni non drenate:

$$Q_{\text{later}} = \alpha \times Cum \times As$$

essendo

Cum = coesione non drenata media lungo lo strato

As = area della superficie laterale del palo

α = coeff. riduttivo in funzione delle modalità esecutive:

- per pali infissi:

$$\alpha = 1$$

per $Cu \leq 25 \text{ kPa}$ ($0,25 \text{ kg/cm}^2$)

- per pali trivellati:	$\alpha = 1-0,011(Cu-25)$	per $25 < Cu < 70$ kPa
	$\alpha = 0,5$	per $Cu \geq 70$ kPa (0,70 kg/cm ²)
	$\alpha = 0,7$	per $Cu \leq 25$ kPa (0,25 kg/cm ²)
	$\alpha = 0,7-0,008(Cu-25)$	per $25 < Cu < 70$ kPa
	$\alpha = 0,35$	per $Cu \geq 70$ kPa (0,70 kg/cm ²)

- In terreni coesivi in condizioni drenate:

$$Q_{later} = (1 - \sin \phi') \cdot \sigma'_v(z) \cdot \mu \cdot A_s$$

essendo

$\sigma'_v(z)$ = tensione verticale efficace lungo il fusto del palo

μ = coefficiente di attrito:

$\mu = \tan \phi'$	per pali trivellati
$\mu = \tan (3/4 \cdot \phi')$	per pali infissi prefabbricati

- In terreni incoerenti:

$$Q_{later} = K \cdot \sigma'_v(z) \cdot \mu \cdot A_s$$

essendo

$\sigma'_v(z)$ = tensione verticale efficace lungo il fusto del palo

K = coefficiente di spinta:

$K = (1 - \sin \phi')$	per pali trivellati
$K = 1$	per pali infissi

μ = coefficiente di attrito:

$\mu = \tan \phi'$	per pali trivellati
$\mu = \tan (3/4 \cdot \phi')$	per pali infissi prefabbricati

Pp: PESO DEL PALO

Patr_neg: CARICO DA ATTRITO NEGATIVO

$Patr_neg = 0$	in terreni coesivi in condizioni non drenate
$Patr_neg = A_s \times \beta \times \sigma'_m$	in terreni incoerenti o coesivi in condizioni drenate

essendo

β = coeff. di *Lambe*

σ'_m = pressione verticale efficace media lungo lo strato deformabile

Il carico ammissibile risulta pari a:

$$Q_{amm} = \left(\frac{Q_{punta}}{\mu_P} + \frac{Q_{later} - P_{palo} - Patr_neg}{\mu_L} \right) \times E_g$$

dove:

μ_p = coefficiente di sicurezza del palo per resistenza di punta

μ_L = coefficiente di sicurezza del palo per resistenza laterale

E_g = coefficiente di efficienza dei pali in gruppo:

- in terreni coesivi:

a) per plinti rettangolari (secondo *Converse-La Barre*):

$$E_g = 1 - \arctan \frac{D}{i} \cdot \frac{(n-1)m + (m-1)n}{90mn}$$

con

m = numero delle file dei pali nel gruppo

n = numero di pali per ciascuna fila

i = interasse fra i pali

b) per plinti triangolari (secondo *Barla*):

$$E_g = 1 - \arctan \frac{D}{i} \cdot 7.05E - 03$$

c) per plinti rettangolari a cinque pali (secondo *Barla*):

$$E_g = 1 - \arctan \frac{D}{i} \cdot 10.85E - 03$$

- in terreni incoerenti:

$E_g = 1$

per pali infissi

$E_g = 2/3$

per pali trivellati

b) Pali resistenti a trazione

- Il carico ultimo del palo a trazione vale:

$$Q_{lim} = Q_{later} + P_{palo}$$

- Il carico ammissibile risulta invece pari a:

$$Q_{amm} = Q_{lim} / \mu_L$$

• CAPACITÀ PORTANTE DELLE PLATEE

La verifica agli S.L.U. delle platee di fondazione risulta particolarmente difficoltosa poiché tali fondazioni spesso hanno forme non rettangolari e pertanto non è possibile valutarne la capacità portante attraverso le classiche formule della geotecnica.

Per potere valutare la portanza delle platee si è quindi implementato un tipo di verifica in cui la fondazione viene modellata per intero (potendo essere costituita, nella forma più generale, da travi rovesce, plinti, pali e platee).

In particolare, gli elementi strutturali vengono modellati in campo elastico lineare, mentre il terreno viene modellato come un letto di molle:

a) lineari elastiche e non reagenti a trazione per le platee;

b) molle non lineari elasto-plastiche non reagenti a trazione per le travi *Winkler* ed i plinti diretti.

Per le molle elastiche delle platee viene calcolato anche il limite elastico, al fine di bloccare il calcolo del moltiplicatore dei carichi qualora venga raggiunto tale limite.

Il legame di tipo elastico reagente a sola compressione è ottenuto utilizzando come rigidezza all'origine la costante di *Winkler* del terreno. Il modello così ottenuto è in grado di tenere in conto dell'eterogeneità del terreno in maniera puntuale. Su tale modello viene quindi condotta un'analisi non lineare a controllo di forza immettendo le forze agenti sulla fondazione.

Il calcolo viene interrotto quando le molle delle platee attingono al loro limite elastico o qualora venga raggiunto uno stato di incipiente formazione di cerniere plastiche nelle travi *Winkler*. In corrispondenza a tali eventi viene calcolato il moltiplicatore dei carichi.

• CALCOLO DEI CEDIMENTI

Il calcolo viene eseguito sulla base della conoscenza delle tensioni nel sottosuolo.

$$\mu = \int \frac{\sigma(z)}{E} dz$$

essendo

E = modulo elastico o edometrico

$\sigma(z)$ = tensione verticale nel sottosuolo dovuta all'incremento di carico q

La distribuzione delle tensioni verticali viene valutata secondo l'espressione di *Steinbrenner*, considerando la pressione agente uniformemente su una superficie rettangolare di dimensioni B e L :

$$\sigma(z) = \frac{q}{4\pi} \left[\frac{2 \times M \times N \times \sqrt{V} \times (V+1)}{V(V+V1)} + \left| \arctan \frac{2 \times M \times N \times \sqrt{V}}{V-V1} \right| \right]$$

con:

$$M = B / z$$

$$N = L / z$$

$$V = M^2 + N^2 + 1$$

$$V1 = (M \times N)^2$$

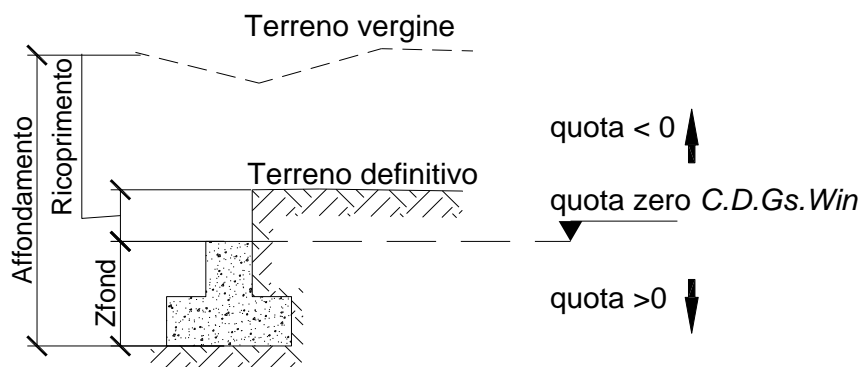
- **SPECIFICHE CAMPI TABELLA DI STAMPA**

Si riporta di seguito la spiegazione delle sigle usate nella tabella di stampa dei dati geometrici delle travi *Winkler*.

<i>Trave</i>	: <i>numero sequenziale della trave</i>
Asta3d	: <i>numero asta tipo in C.D.S. Win (spaziale)</i>
Filo Iniz	: <i>primo filo fisso</i>
Filo Fin.	: <i>secondo filo fisso</i>
<i>Nodo3d In.</i>	: <i>numero Nodo3d primo filo fisso</i>
Nodo3d Fin	: <i>numero Nodo3d secondo filo fisso</i>
X3d In.	: <i>ascissa Nodo3d Iniziale</i>
Y3d In.	: <i>ordinata Nodo3d Iniziale</i>
<i>Z3d In.</i>	: <i>quota Nodo3d Iniziale</i>
X3d Fin	: <i>ascissa Nodo3d finale</i>
Y3d Fin	: <i>ordinata Nodo3d finale</i>
Z3d Fin	: <i>quota Nodo3d finale</i>
<i>Xfond</i>	: <i>ascissa baricentro fondazione</i>
Yfond	: <i>ordinata baricentro fondazione</i>
Zfond	: <i>quota baricentro base di fondazione nel riferimento di C.D.Gs. Win</i>
Bfond	: <i>dimensione trasversale trave Winkler</i>
Lfond	: <i>dimensione longitudinale trave Winkler</i>

- SPECIFICHE CAMPI TABELLA DI STAMPA**

Si riporta di seguito la spiegazione delle sigle usate nella tabella di stampa della stratigrafia del terreno sottostante le travi *Winkler*.

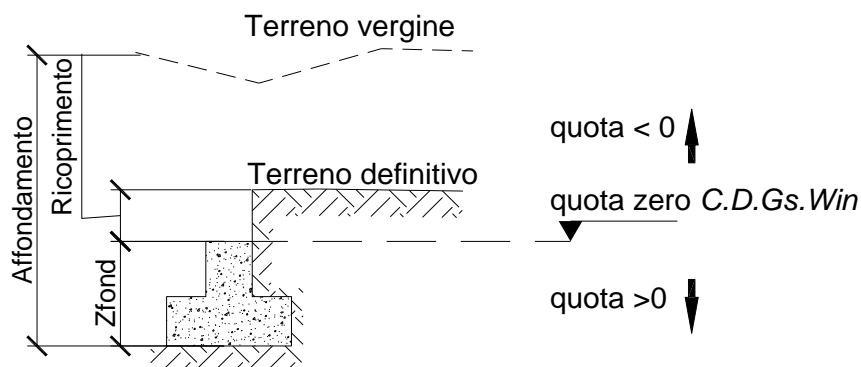


NOTA: La quota zero di *C.D.Gs. Win* coincide con la quota numero zero dell'alberello quote di *C.D.S. Win* ma cambia la convenzione nel segno: infatti in *C. D. Gs.* le quote sono positive crescenti procedendo verso il basso, mentre in *C. D. S.* le quote sono positive crescenti verso l'alto.

<i>Trave</i>	: <i>numero di trave</i>
Q.t.v.	: <i>quota terreno vergine</i>
Q.t.d.	: <i>quota definitiva terreno</i>
Q.falda	: <i>quota falda</i>
InclTer	: <i>inclinazione terreno</i>
Numero strato	: <i>Numero dello strato a cui si riferiscono i dati che seguono</i>
Sp.str.	: <i>Spessore strato. L'ultimo strato ha spessore indefinito, pertanto il relativo dato non viene stampato</i>
<i>Peso Sp</i>	: <i>peso specifico</i>
Fi	: <i>angolo di attrito interno in gradi</i>
C'	: <i>coesione drenata</i>
Cu	: <i>coesione non drenata</i>
Mod.El.	: <i>modulo elastico</i>
Poisson	: <i>coefficiente di Poisson</i>
Gr.Sovr	: <i>grado di sovraconsolidazione</i>
Mod.Ed	: <i>modulo edometrico</i>

- SPECIFICHE CAMPI TABELLA DI STAMPA**

Si riporta di seguito la spiegazione delle sigle usate nella tabella di stampa della stratigrafia del terreno sottostante i plinti.



NOTA: La quota zero di *C.D.Gs. Win* coincide con la quota numero zero dell'alberello quote di *C.D.S. Win* ma cambia la convenzione nel segno: infatti in *C. D. Gs.* le quote sono positive crescenti procedendo verso il basso, mentre in *C. D. S.* le quote sono positive crescenti verso l'alto.

Plinto : Numero di plinto

Q.t.v. : quota terreno vergine

Q.t.d. : quota definitiva terreno

Q.falda : quota falda

InclTer : inclinazione terreno

Num Str : Numero dello strato a cui si riferiscono i dati che seguono

Sp.str. : Spessore strato. L'ultimo strato ha spessore indefinito, pertanto il relativo dato non viene stampato

Peso Sp : peso specifico

Fi : angolo di attrito interno

C' : coesione drenata

Cu : coesione NON drenata

Mod.El. : modulo elastico

Poisson : coeff. Poisson

Coeff. Lambe : coefficiente beta di Lambe

Gr.Sovr : grado di sovraconsolidazione

Mod.Ed. : modulo edometrico

- **SPECIFICHE CAMPI TABELLA DI STAMPA**

Si riporta di seguito la spiegazione delle sigle usate nella tabella di stampa delle risultanti delle sollecitazioni agenti sull'area d'impronta delle travi *Winkler*, nel sistema di riferimento locale (y=asse trave).

<i>Trave</i>	: <i>numero di trave sequenziale</i>
Comb.	: <i>Numero della combinazione a cui si riferiscono i dati che seguono</i>
Rv	: <i>Risultante delle pressioni verticali</i>
Vx	: <i>Risultante delle sollecitazioni agenti parallelamente all'asse x locale dell' asta</i>
Vy	: <i>Risultante delle sollecitazioni agenti parallelamente all'asse y locale dell' asta</i>
Mrx	: <i>Momento risultante di asse vettore x nel sistema di riferimento locale dell' asta (momento flettente)</i>
Mry	: <i>Momento risultante di asse vettore y nel sistema di riferimento locale dell' asta (momento torcente)</i>

- **SPECIFICHE CAMPI TABELLA DI STAMPA**

Si riporta di seguito la spiegazione delle sigle usate sia nella tabella di stampa della portanza globale della fondazione, sia nella tabella della portanza di fondazione delle platee calcolata con analisi elastica del terreno:

Tabella 1: Moltiplicatori di Collasso

<i>Comb. Nro</i>	: Numero della combinazione
<i>Risultante</i>	: Valore della risultante delle forze trasmesse dalla fondazione per la combinazione attuale
<i>Resistenza</i>	: Valore della resistenza del terreno mobilitata in base al moltiplicatore dei carichi attuale
<i>Moltipl.Collasso</i>	: Valore del moltiplicatore dei carichi con cui è stato eseguito il calcolo. Poiche' tutti i coefficienti di sicurezza sono già stati considerati nei carichi e nelle caratteristiche dei materiali, un moltiplicatore = 1 significa che la verifica di portanza è soddisfatta.
<i>%Pl.Molle</i>	: Percentuale delle molle in fase plastica nella combinazione attuale
<i>STATUS</i>	: Per moltiplicatori di collasso < 1 mostra NOVERIF, altrimenti OK

Tabella 2: Abbassamenti

<i>Nodo3d</i>	: Numero del nodo3d a cui si riferisce la molla elasto-plastica
<i>SpostZ</i>	: Abbassamento della molla elasto-plastica in corrispondenza del nodo3d
<i>SpostZ/SpostEl</i>	: Fattore di plasticizzazione della molla:

FASE ELASTICA ≤ 1 ; FASE PLASTICA > 1

Se per alcuni nodi non è stato possibile ottenere la caratterizzazione geotecnica, allora tali nodi vengono esclusi dal modello di calcolo e la relativa molla viene contrassegnata in stampa con la sigla 'SCARTATA'

RELAZIONE GEOTECNICA

DATI GENERALI			
COEFFICIENTI PARZIALI GEOTECNICA			
		TABELLA M1	TABELLA M2
Tangente Resist. Taglio		1,00	
Peso Specifico		1,00	
Coesione Efficace (c'k)		1,00	
Resist. a taglio NON drenata (cuk)		1,00	
Tipo Approccio		Combinazione Unica: (A1+M1+R3)	
Tipo di fondazione		Su Pali Infissi	
		COEFFICIENTE R1	COEFFICIENTE R2
Capacita' Portante			2,30
Scorrimento			1,10
Resist. alla Base			1,15
Resist. Lat. a Compr.			1,15
Resist. Lat. a Traz.			1,25
Carichi Trasversali			1,30
Fattore di correlazione CSI per il calcolo di Rk pali			1,70

CRITERI DI PROGETTO GEOTECNICI - FONDAZIONI SUPERFICIALI																			
IDEN	CARATTERISTICHE DI SITO						IDEN	CARATTERISTICHE DI SITO						IDEN	CARATTERISTICHE DI SITO				
Crit N.ro	Falda (m)	Affond (m)	Ricopr (m)	Pend.X (grd)	Pend.Y (Grd)		Crit N.ro	Falda (m)	Affond (m)	Ricopr (m)	Pend.X (grd)	Pend.Y (Grd)		Crit N.ro	Falda (m)	Affond (m)	Ricopr (m)	Pend.X (grd)	Pend.Y (Grd)
1	0.00	0.00	0	0			2	1.30	0.00	0	0								

GEOMETRIA TRAVI WINKLER																
IDENTIFICATIVO						COORDINATE 3D ESTREMI ASTA WINKLER						DATI IMPRONTA				
Trave N.ro	Ast3d N.ro	Fil In.	Fil Fin	Nod3d Iniz.	Nod3d Fin.	X3dIn. (m)	Y3dIn. (m)	Z3dIn. (m)	X3dFin (m)	Y3dFin (m)	Z3dFin (m)	Xfond (m)	Yfond (m)	Zfond (m)	Bfond (m)	Lfond (m)
1	1	1	2	1	2	5,38	0,15	-1,00	9,55	0,15	-1,00	7,47	0,15	2,00	0,60	4,17
2	2	1	7	1	3	5,38	0,15	-1,00	5,18	2,25	-1,00	5,28	1,20	2,00	0,60	2,11
3	3	10	16	4	5	9,55	5,95	-1,00	9,55	9,80	-1,00	9,45	7,88	2,00	0,60	3,85
4	4	2	10	2	4	9,55	0,15	-1,00	9,55	5,95	-1,00	9,45	3,05	2,00	0,60	5,80
5	5	3	11	6	7	13,70	0,15	-1,00	13,70	5,95	-1,00	13,70	3,05	2,00	0,60	5,80
6	6	4	12	8	9	18,75	0,25	-1,00	18,75	5,95	-1,00	18,75	3,12	2,00	0,60	5,70
7	7	5	13	10	11	24,30	0,25	-1,00	24,30	5,95	-1,00	24,30	3,12	2,00	0,60	5,70
8	8	6	8	12	13	0,25	2,25	-1,00	0,15	6,05	-1,00	0,15	4,10	2,00	0,60	3,80
9	9	7	9	3	14	5,18	2,25	-1,00	5,18	5,95	-1,00	5,28	4,10	2,00	0,60	3,70
10	10	8	14	13	15	0,15	6,05	-1,00	0,15	9,90	-1,00	0,15	7,97	2,00	0,60	3,85
11	11	9	15	14	16	5,18	5,95	-1,00	5,18	9,80	-1,00	5,18	7,88	2,00	0,60	3,85
12	12	11	17	7	17	13,70	5,95	-1,00	13,70	9,80	-1,00	13,70	7,88	2,00	0,60	3,85
13	13	12	18	9	18	18,75	5,95	-1,00	18,85	9,80	-1,00	18,75	7,95	2,00	0,60	3,85
14	14	13	19	11	19	24,30	5,95	-1,00	24,20	9,80	-1,00	24,30	7,95	2,00	0,60	3,85
15	15	14	20	15	20	0,15	9,90	-1,00	0,25	15,20	-1,00	0,15	12,60	2,00	0,60	5,30
16	16	15	21	16	21	5,18	9,80	-1,00	5,18	15,20	-1,00	5,18	12,50	2,00	0,60	5,40
17	17	16	22	5	22	9,55	9,80	-1,00	9,45	15,10	-1,00	9,45	12,40	2,00	0,60	5,30
18	18	17	23	17	23	13,70	9,80	-1,00	13,70	15,20	-1,00	13,70	12,50	2,00	0,60	5,40
19	19	18	24	18	24	18,85	9,80	-1,00	18,85	15,20	-1,00	18,75	12,50	2,00	0,60	5,40
20	20	21	27	21	25	5,18	15,20	-1,00	5,28	21,00	-1,00	5,28	18,05	2,00	0,60	5,80
21	21	22	28	22	26	9,45	15,10	-1,00	9,45	21,10	-1,00	9,40	18,15	2,00	0,60	6,00
22	22	23	29	23	27	13,70	15,20	-1,00	13,70	21,10	-1,00	13,70	18,15	2,00	0,60	5,90
23	23	24	30	24	28	18,85	15,20	-1,00	18,85	21,10	-1,00	18,75	18,15	2,00	0,60	5,90
24	24	25	31	29	30	24,30	15,20	-1,00	24,30	21,10	-1,00	24,20	18,15	2,00	0,60	5,90
25	25	26	32	31	32	27,87	15,30	-1,00	27,87	21,00	-1,00	27,87	18,15	2,00	0,60	5,70
26	26	2	3	2	6	9,55	0,15	-1,00	13,70	0,15	-1,00	11,60	0,15	2,00	0,60	4,15
27	27	3	4	6	8	13,70	0,15	-1,00	18,75	0,25	-1,00	16,30	0,15	2,00	0,60	5,05
28	28	4	5	8	10	18,75	0,25	-1,00	24,30	0,25	-1,00	21,52	0,15	2,00	0,60	5,55
29	29	6	7	12	3	0,25	2,25	-1,00	5,18	2,25	-1,00	2,71	2,25	2,00	0,60	4,93
30	30	8	9	13	14	0,15	6,05	-1,00	5,18	5,95	-1,00	2,62	5,95	2,00	0,60	5,03
31	31	9	10	14	4	5,18	5,95	-1,00	9,55	5,95	-1,00	7,36	5,95	2,00	0,60	4,37
32	32	10	11	4	7	9,55	5,95	-1,00	13,70	5,95	-1,00	11,60	5,95	2,00	0,60	4,15
33	33	11	12	7	9	13,70	5,95	-1,00	18,75	5,95	-1,00	16,30	5,95	2,00	0,60	5,05
34	34	12	13	9	11	18,75	5,95	-1,00	24,30	5,95	-1,00	21,52	5,95	2,00	0,60	5,55
35	35	14	15	15	16	0,15	9,90	-1,00	5,18	9,80	-1,00	2,62	9,80	2,00	0,60	5,03
36	36	15	16	16	5	5,18	9,80	-1,00	9,55	9,80	-1,00	7,36	9,80	2,00	0,60	4,37
37	37	16	17	5	17	9,55	9,80	-1,00	13,70	9,80	-1,00	11,60	9,80	2,00	0,60	4,15
38	38	17	18	17	18	13,70	9,80	-1,00	18,85	9,80	-1,00	16,30	9,80	2,00	0,60	5,15
39	39	18	19	18	19	18,85	9,80	-1,00	24,20	9,80	-1,00	21,53	9,80	2,00	0,60	5,35
40	40	20	21	20	21	0,25	15,20	-1,00	5,18	15,20	-1,00	2,71	15,20	2,00	0,60	4,93
41	41	21	22	21	22	5,18	15,20	-1,00	9,45	15,10	-1,00	7,36	15,20	2,00	0,60	4,27

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE:C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

GEOMETRIA TRAVI WINKLER																
IDENTIFICATIVO						COORDINATE 3D ESTREMI ASTA WINKLER						DATI IMPRONTA				
Trave N.ro	Ast3d N.ro	Fil In.	Fil Fin	Nod3d Iniz.	Nod3d Fin.	X3dIn. (m)	Y3dIn. (m)	Z3dIn. (m)	X3dFin (m)	Y3dFin (m)	Z3dFin (m)	Xfond (m)	Yfond (m)	Zfond (m)	Bfond (m)	Lfond (m)
42	42	22	23	22	23	9,45	15,10	-1,00	13,70	15,20	-1,00	11,50	15,20	2,00	0,60	4,25
43	43	23	24	23	24	13,70	15,20	-1,00	18,85	15,20	-1,00	16,30	15,20	2,00	0,60	5,15
44	44	24	25	24	29	18,85	15,20	-1,00	24,30	15,20	-1,00	21,60	15,20	2,00	0,60	5,45
45	45	25	26	29	31	24,30	15,20	-1,00	27,87	15,30	-1,00	26,16	15,20	2,00	0,60	3,57
46	46	27	28	25	26	5,28	21,00	-1,00	9,45	21,10	-1,00	7,32	21,10	2,00	0,60	4,17
47	47	28	29	26	27	9,45	21,10	-1,00	13,70	21,10	-1,00	11,55	21,10	2,00	0,60	4,25
48	48	29	30	27	28	13,70	21,10	-1,00	18,85	21,10	-1,00	16,30	21,10	2,00	0,60	5,15
49	49	30	31	28	30	18,85	21,10	-1,00	24,30	21,10	-1,00	21,60	21,10	2,00	0,60	5,45
50	50	31	32	30	32	24,30	21,10	-1,00	27,87	21,00	-1,00	26,16	21,10	2,00	0,60	3,57

STRATIGRAFIA TRAVI WINKLER															
Trave N.ro	Q.t.v. (m)	Q.t.d. (m)	Q.falda (m)	Incl Grd	Kw kg/cmc	Numero Strato	Sp.str. (m)	Peso Sp kg/mc	Fi' (Grd)	C' kg/cmq	Cu kg/cmq	Mod.El. kg/cmq	Poisson	Gr.Sovr	Mod.Ed. kg/cmq
1	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
2	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
3	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
4	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
5	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
6	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
7	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
8	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
9	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
10	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
11	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
12	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
13	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
14	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
15	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
16	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
17	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
18	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
19	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
20	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
21	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
22	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
23	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00

RELAZIONE GEOTECNICA

STRATIGRAFIA TRAVI WINKLER															
Trave N.ro	Q.t.v. (m)	Q.t.d. (m)	Q.falda (m)	Incl Grd	Kw kg/cm	Numero Strato	Sp.str. (m)	Peso Sp kg/cm	Ft' (Grd)	C' kg/cm	Cu kg/cm	Mod.El. kg/cm	Poisson	Gr.Sovr	Mod.Ed. kg/cm
24	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
25	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
26	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
27	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
28	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
29	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
30	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
31	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
32	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
33	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
34	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
35	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
36	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
37	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
38	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
39	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
40	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
41	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
42	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
43	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
44	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
45	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
46	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
47	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
48	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
49	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00
50	0,70	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1,00	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1,00	100,00

RELAZIONE GEOTECNICA

COORDINATE NODI3D PLATEA															
IDENT. POSIZIONE NODO				IDENT. POSIZIONE NODO				IDENT. POSIZIONE NODO				IDENT. POSIZIONE NODO			
Nodo3d N.ro	Coord.X (m)	Coord.Y (m)	Coord.Z (m)	Nodo3d N.ro	Coord.X (m)	Coord.Y (m)	Coord.Z (m)	Nodo3d N.ro	Coord.X (m)	Coord.Y (m)	Coord.Z (m)	Nodo3d N.ro	Coord.X (m)	Coord.Y (m)	Coord.Z (m)
1	5,38	0,15	-1,00	3	5,18	2,25	-1,00	4	9,55	5,95	-1,00	5	9,55	9,80	-1,00
7	13,70	5,95	-1,00	8	18,75	0,25	-1,00	9	18,75	5,95	-1,00	10	24,30	0,25	-1,00
12	0,25	2,25	-1,00	14	5,18	5,95	-1,00	15	0,15	9,90	-1,00	16	5,18	9,80	-1,00
17	13,70	9,80	-1,00	18	18,85	9,80	-1,00	19	24,20	9,80	-1,00	20	0,25	15,20	-1,00
21	5,18	15,20	-1,00	22	9,45	15,10	-1,00	23	13,70	15,20	-1,00	24	18,85	15,20	-1,00
25	5,28	21,00	-1,00	31	27,87	15,30	-1,00	32	27,87	21,00	-1,00	65	6,42	0,15	-1,00
66	5,28	1,20	-1,00	67	9,55	6,91	-1,00	68	9,55	7,88	-1,00	69	9,55	8,84	-1,00
70	9,55	1,31	-1,00	71	9,55	2,47	-1,00	72	9,55	3,63	-1,00	73	9,55	4,79	-1,00
74	13,70	1,31	-1,00	75	13,70	2,47	-1,00	76	13,70	3,63	-1,00	77	13,70	4,79	-1,00
78	18,75	1,39	-1,00	79	18,75	2,53	-1,00	80	18,75	3,67	-1,00	81	18,75	4,81	-1,00
82	5,18	3,17	-1,00	83	5,18	4,10	-1,00	84	5,18	5,02	-1,00	85	5,18	6,91	-1,00
86	5,18	7,88	-1,00	87	5,18	8,84	-1,00	88	13,70	6,91	-1,00	89	13,70	7,88	-1,00
90	13,70	8,84	-1,00	91	18,77	6,91	-1,00	92	18,80	7,88	-1,00	93	18,83	8,84	-1,00
94	0,17	10,96	-1,00	95	0,19	12,02	-1,00	96	0,21	13,08	-1,00	97	0,23	14,14	-1,00
98	5,18	10,88	-1,00	99	5,18	11,96	-1,00	100	5,18	13,04	-1,00	101	5,18	14,12	-1,00
102	9,53	10,86	-1,00	103	9,51	11,92	-1,00	104	9,49	12,98	-1,00	105	9,47	14,04	-1,00
106	13,70	10,88	-1,00	107	13,70	11,96	-1,00	108	13,70	13,04	-1,00	109	13,70	14,12	-1,00
110	18,85	10,88	-1,00	111	18,85	11,96	-1,00	112	18,85	13,04	-1,00	113	18,85	14,12	-1,00
114	5,20	16,36	-1,00	115	5,22	17,52	-1,00	116	5,24	18,68	-1,00	117	5,26	19,84	-1,00
118	9,45	16,30	-1,00	119	9,45	17,50	-1,00	120	9,45	18,70	-1,00	121	9,45	19,90	-1,00
122	13,70	16,38	-1,00	123	13,70	17,56	-1,00	124	13,70	18,74	-1,00	125	13,70	19,92	-1,00
126	18,85	16,38	-1,00	127	18,85	17,56	-1,00	128	18,85	18,74	-1,00	129	18,85	19,92	-1,00
130	27,87	16,44	-1,00	131	27,87	17,58	-1,00	132	27,87	18,72	-1,00	133	27,87	19,86	-1,00
134	16,73	0,21	-1,00	135	17,74	0,23	-1,00	136	19,86	0,25	-1,00	137	20,97	0,25	-1,00
138	22,08	0,25	-1,00	139	23,19	0,25	-1,00	140	3,95	2,25	-1,00	141	2,71	2,25	-1,00
142	1,48	2,25	-1,00	143	1,16	6,03	-1,00	144	2,16	6,01	-1,00	145	3,17	5,99	-1,00
146	4,17	5,97	-1,00	147	8,46	5,95	-1,00	148	7,36	5,95	-1,00	149	6,27	5,95	-1,00
150	10,59	5,95	-1,00	151	11,63	5,95	-1,00	152	12,66	5,95	-1,00	153	14,71	5,95	-1,00
154	15,72	5,95	-1,00	155	16,73	5,95	-1,00	156	17,74	5,95	-1,00	157	19,86	5,95	-1,00
158	20,97	5,95	-1,00	159	22,08	5,95	-1,00	160	23,19	5,95	-1,00	161	1,16	9,88	-1,00
162	2,16	9,86	-1,00	163	3,17	9,84	-1,00	164	4,17	9,82	-1,00	165	8,46	9,80	-1,00
166	7,36	9,80	-1,00	167	6,27	9,80	-1,00	168	10,59	9,80	-1,00	169	11,63	9,80	-1,00
170	12,66	9,80	-1,00	171	14,73	9,80	-1,00	172	15,76	9,80	-1,00	173	16,79	9,80	-1,00
174	17,82	9,80	-1,00	175	19,92	9,80	-1,00	176	20,99	9,80	-1,00	177	22,06	9,80	-1,00
178	23,13	9,80	-1,00	179	1,48	15,20	-1,00	180	2,71	15,20	-1,00	181	3,95	15,20	-1,00
182	6,25	15,18	-1,00	183	7,31	15,15	-1,00	184	8,38	15,13	-1,00	185	10,51	15,13	-1,00
186	11,57	15,15	-1,00	187	12,64	15,18	-1,00	188	14,73	15,20	-1,00	189	15,76	15,20	-1,00
190	16,79	15,20	-1,00	191	17,82	15,20	-1,00	192	1,15	3,15	-1,00	193	2,15	3,15	-1,00
194	2,15	4,15	-1,00	195	1,15	4,15	-1,00	196	4,15	3,15	-1,00	197	3,15	3,15	-1,00
198	3,15	4,15	-1,00	199	4,15	4,15	-1,00	200	3,15	5,15	-1,00	201	2,15	5,15	-1,00
202	1,15	5,15	-1,00	203	4,15	5,15	-1,00	204	7,15	1,15	-1,00	205	6,15	1,15	-1,00
206	6,15	2,15	-1,00	207	7,15	2,15	-1,00	208	6,15	3,15	-1,00	209	7,15	3,15	-1,00
210	8,15	2,15	-1,00	211	8,15	3,15	-1,00	212	6,15	4,15	-1,00	213	7,15	4,15	-1,00
214	6,15	5,15	-1,00	215	7,15	5,15	-1,00	216	8,15	4,15	-1,00	217	8,15	5,15	-1,00
218	2,15	7,15	-1,00	219	3,15	7,15	-1,00	220	3,15	8,15	-1,00	221	2,15	8,15	-1,00
222	1,15	7,15	-1,00	223	1,15	8,15	-1,00	224	1,15	9,15	-1,00	225	2,15	9,15	-1,00
226	3,15	9,15	-1,00	227	4,15	8,15	-1,00	228	4,15	9,15	-1,00	229	4,15	7,15	-1,00
230	7,15	8,15	-1,00	231	7,15	7,15	-1,00	232	8,15	7,15	-1,00	233	8,15	8,15	-1,00
234	6,15	7,15	-1,00	235	6,15	8,15	-1,00	236	7,15	9,15	-1,00	237	6,15	9,15	-1,00
238	8,15	9,15	-1,00	239	8,15	1,15	-1,00	240	9,15	1,15	-1,00	241	9,15	2,15	-1,00
242	9,15	3,15	-1,00	243	9,15	4,15	-1,00	244	9,15	5,15	-1,00	245	11,15	1,15	-1,00
246	10,15	1,15	-1,00	247	10,15	2,15	-1,00	248	11,15	2,15	-1,00	249	11,15	3,15	-1,00
250	10,15	3,15	-1,00	251	12,15	1,15	-1,00	252	12,15	2,15	-1,00	253	13,15	1,15	-1,00
254	13,15	2,15	-1,00	255	12,15	3,15	-1,00	256	11,15	4,15	-1,00	257	10,15	4,15	-1,00
258	12,15	4,15	-1,00	259	13,15	3,15	-1,00	260	13,15	4,15	-1,00	261	12,15	5,15	-1,00
262	11,15	5,15	-1,00	263	10,15	5,15	-1,00	264	13,15	5,15	-1,00	265	9,15	7,15	-1,00
266	9,15	8,15	-1,00	267	9,15	9,15	-1,00	268	11,15	7,15	-1,00	269	10,15	7,15	-1,00
270	10,15	8,15	-1,00	271	11,15	8,15	-1,00	272	12,15	7,15	-1,00	273	13,15	7,15	-1,00
274	13,15	8,15	-1,00	275	12,15	8,15	-1,00	276	10,15	9,15	-1,00	277	11,15	9,15	-1,00
278	13,15	9,15	-1,00	279	12,15	9,15	-1,00	280	4,15	10,15	-1,00	281	3,15	10,15	-1,00
282	3,15	11,15	-1,00	283	4,15	11,15	-1,00	284	1,15	11,15	-1,00	285	2,15	11,15	-1,00
286	2,15	12,15	-1,00	287	1,15	12,15	-1,00	288	1,15	13,15	-1,00	289	2,15	13,15	-1,00
290	3,15	12,15	-1,00	291	3,15	13,15	-1,00	292	4,15	12,15	-1,00	293	4,15	13,15	-1,00
294	3,15	14,15	-1,00	295	2,15	14,15	-1,00	296	1,15	14,15	-1,00	297	6,15	10,15	-1,00
298	7,15	10,15	-1,00	299	7,15	11,15	-1,00	300	6,15	11,15	-1,00	301	8,15	10,15	-1,00
302	8,														

RELAZIONE GEOTECNICA

COORDINATE NODI3D PLATEA															
IDENT.		POSIZIONE NODO			IDENT.		POSIZIONE NODO			IDENT.		POSIZIONE NODO			
Nodo3d N.ro	Coord.X (m)	Coord.Y (m)	Coord.Z (m)	Nodo3d N.ro	Coord.X (m)	Coord.Y (m)	Coord.Z (m)	Nodo3d N.ro	Coord.X (m)	Coord.Y (m)	Coord.Z (m)	Nodo3d N.ro	Coord.X (m)	Coord.Y (m)	Coord.Z (m)
394	17,15	1,15	-1,00	395	18,15	1,15	-1,00	396	18,15	2,15	-1,00	397	18,15	3,15	-1,00
398	17,15	3,15	-1,00	399	17,15	4,15	-1,00	400	17,15	5,15	-1,00	401	18,15	4,15	-1,00
402	18,15	5,15	-1,00	403	14,15	8,15	-1,00	404	15,15	8,15	-1,00	405	15,15	7,15	-1,00
406	14,15	7,15	-1,00	407	16,15	7,15	-1,00	408	16,15	8,15	-1,00	409	15,15	9,15	-1,00
410	16,15	9,15	-1,00	411	14,15	9,15	-1,00	412	14,15	10,15	-1,00	413	15,15	10,15	-1,00
414	15,15	11,15	-1,00	415	14,15	11,15	-1,00	416	17,15	7,15	-1,00	417	17,15	8,15	-1,00
418	18,15	8,15	-1,00	419	18,15	7,15	-1,00	420	17,15	9,15	-1,00	421	18,15	9,15	-1,00
422	16,15	10,15	-1,00	423	17,15	10,15	-1,00	424	17,15	11,15	-1,00	425	16,15	11,15	-1,00
426	20,15	1,15	-1,00	427	19,15	1,15	-1,00	428	19,15	2,15	-1,00	429	20,15	2,15	-1,00
430	21,15	2,15	-1,00	431	21,15	1,15	-1,00	432	20,15	3,15	-1,00	433	19,15	3,15	-1,00
434	19,15	4,15	-1,00	435	20,15	4,15	-1,00	436	19,15	5,15	-1,00	437	20,15	5,15	-1,00
438	21,15	3,15	-1,00	439	21,15	4,15	-1,00	440	22,15	2,15	-1,00	441	22,15	3,15	-1,00
442	21,15	5,15	-1,00	443	22,15	4,15	-1,00	444	22,15	1,15	-1,00	445	23,15	2,15	-1,00
446	23,15	1,15	-1,00	447	23,15	3,15	-1,00	448	22,15	5,15	-1,00	449	23,15	4,15	-1,00
450	23,15	5,15	-1,00	451	20,15	8,15	-1,00	452	20,15	7,15	-1,00	453	19,15	7,15	-1,00
454	19,15	8,15	-1,00	455	21,15	8,15	-1,00	456	21,15	7,15	-1,00	457	19,15	9,15	-1,00
458	20,15	9,15	-1,00	459	21,15	9,15	-1,00	460	22,15	7,15	-1,00	461	22,15	8,15	-1,00
462	23,15	7,15	-1,00	463	23,15	8,15	-1,00	464	22,15	9,15	-1,00	465	23,15	9,15	-1,00
466	14,15	12,15	-1,00	467	15,15	12,15	-1,00	468	14,15	13,15	-1,00	469	15,15	13,15	-1,00
470	16,15	12,15	-1,00	471	15,15	14,15	-1,00	472	16,15	13,15	-1,00	473	16,15	14,15	-1,00
474	14,15	16,15	-1,00	475	15,15	16,15	-1,00	476	15,15	17,15	-1,00	477	14,15	17,15	-1,00
478	14,15	14,15	-1,00	479	17,15	12,15	-1,00	480	17,15	13,15	-1,00	481	18,15	12,15	-1,00
482	18,15	11,15	-1,00	483	18,15	10,15	-1,00	484	18,15	13,15	-1,00	485	18,15	14,15	-1,00
486	17,15	14,15	-1,00	487	16,15	16,15	-1,00	488	16,15	17,15	-1,00	489	15,15	18,15	-1,00
490	14,15	18,15	-1,00	491	15,15	19,15	-1,00	492	14,15	19,15	-1,00	493	16,15	18,15	-1,00
494	14,15	20,15	-1,00	495	15,15	20,15	-1,00	496	16,15	19,15	-1,00	497	17,15	17,15	-1,00
498	17,15	18,15	-1,00	499	16,15	20,15	-1,00	500	17,15	19,15	-1,00	501	17,15	16,15	-1,00
502	18,15	17,15	-1,00	503	18,15	16,15	-1,00	504	18,15	18,15	-1,00	505	18,15	19,15	-1,00
506	18,15	20,15	-1,00	507	17,15	20,15	-1,00	508	21,15	17,15	-1,00	509	20,15	17,15	-1,00
510	20,15	18,15	-1,00	511	21,15	18,15	-1,00	512	21,15	16,15	-1,00	513	22,15	16,15	-1,00
514	22,15	17,15	-1,00	515	22,15	18,15	-1,00	516	23,15	16,15	-1,00	517	23,15	17,15	-1,00
518	20,15	16,15	-1,00	519	21,15	19,15	-1,00	520	20,15	19,15	-1,00	521	24,15	16,15	-1,00
522	24,15	17,15	-1,00	523	25,15	16,15	-1,00	524	25,15	17,15	-1,00	525	26,15	16,15	-1,00
526	26,15	17,15	-1,00	527	25,15	18,15	-1,00	528	24,15	18,15	-1,00	529	23,15	18,15	-1,00
530	27,15	18,15	-1,00	531	27,15	17,15	-1,00	532	26,15	18,15	-1,00	533	27,15	16,15	-1,00
534	20,15	20,15	-1,00	535	21,15	20,15	-1,00	536	23,15	19,15	-1,00	537	22,15	19,15	-1,00
538	22,15	20,15	-1,00	539	23,15	20,15	-1,00	540	24,15	19,15	-1,00	541	24,15	20,15	-1,00
542	25,15	19,15	-1,00	543	25,15	20,15	-1,00	544	26,15	19,15	-1,00	545	27,15	19,15	-1,00
546	27,15	20,15	-1,00	547	26,15	20,15	-1,00	548	6,32	21,00	-1,00	549	7,36	21,00	-1,00
550	8,41	21,00	-1,00	551	9,45	21,00	-1,00	552	10,51	21,00	-1,00	553	11,57	21,00	-1,00
554	12,64	21,00	-1,00	555	14,73	21,00	-1,00	556	13,70	21,00	-1,00	557	15,76	21,00	-1,00
558	16,79	21,00	-1,00	559	17,82	21,00	-1,00	560	20,86	21,00	-1,00	561	19,85	21,00	-1,00
562	21,86	21,00	-1,00	563	22,86	21,00	-1,00	564	23,86	21,00	-1,00	565	24,87	21,00	-1,00
566	25,87	21,00	-1,00	567	26,87	21,00	-1,00	568	0,24	3,20	-1,00	569	0,23	4,15	-1,00
570	0,21	5,10	-1,00	571	0,20	6,05	-1,00	572	7,46	0,16	-1,00	573	0,19	7,01	-1,00
574	0,18	7,98	-1,00	575	0,16	8,94	-1,00	576	8,51	0,17	-1,00	577	9,55	0,17	-1,00
578	10,59	0,18	-1,00	579	11,62	0,18	-1,00	580	12,66	0,19	-1,00	581	13,70	0,19	-1,00
582	14,71	0,20	-1,00	583	15,72	0,20	-1,00	584	24,29	1,20	-1,00	585	24,28	2,15	-1,00
586	24,27	3,10	-1,00	587	24,26	4,05	-1,00	588	24,25	5,00	-1,00	589	24,24	5,95	-1,00
590	24,23	6,91	-1,00	591	24,22	7,87	-1,00	592	24,21	8,84	-1,00	593	18,85	21,00	-1,00
594	20,86	15,22	-1,00	595	19,85	15,21	-1,00	596	21,86	15,23	-1,00	597	22,86	15,24	-1,00
598	23,86	15,26	-1,00	599	24,87	15,27	-1,00	600	25,87	15,28	-1,00	601	26,87	15,29	-1,00

STRATIGRAFIA PLATEA															
Str. N.ro	Q.t.v. (m)	Q.t.d. (m)	Q.falda (m)	Incl Grd	Kw kg/cmc	Num Str	Sp.str. (m)	Peso Sp kg/mc	Fi' (Grd)	C' kg/cmq	Cu kg/cmq	Mod.El. kg/cmq	Poisson	Gr.Sovr (%)	Mod.Ed. kg/cmq
1	0,10	1,00		0	10,00	1	1,20	1800	14,00	0,00	0,00	500,00	0,20	1	500,00
						2		1940	25,00	0,12	0,21	700,00	0,25	1	100,00

[illegible][illegible]

RELAZIONE GEOTECNICA

COMBINAZIONI CARICHI - S.L.U. - A1

DESCRIZIONI	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
Corr. Tors. dir. 0	-1,00	1,00	-1,00	1,00	-1,00	1,00	-1,00	-1,00	1,00	-1,00	1,00	-1,00	1,00	-1,00	1,00
Corr. Tors. dir. 90	0,30	-0,30	-0,30	-0,30	-0,30	0,30	0,30	0,30	0,30	-0,30	-0,30	-0,30	-0,30	0,30	0,30
Sisma direz. grd 0	1,00	1,00	1,00	1,00	1,00	1,00	1,00	-1,00	-1,00	-1,00	-1,00	-1,00	-1,00	-1,00	-1,00
Sisma direz. grd 90	0,30	0,30	0,30	-0,30	-0,30	-0,30	-0,30	0,30	0,30	0,30	0,30	-0,30	-0,30	-0,30	-0,30

COMBINAZIONI CARICHI - S.L.U. - A1

DESCRIZIONI	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45
Peso Strutturale	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00
Perm.Non Strutturale	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00
Var.Abitazioni	0,30	0,30	0,30	0,30	0,30	0,30	0,30	0,30	0,30	0,30	0,30	0,30	0,30	0,30	0,30
Var.Neve h<=1000	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
Vento dir. 0	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
Vento dir. 90	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
Vento dir. 180	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
Vento dir. 270	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
Corr. Tors. dir. 0	0,30	-0,30	0,30	-0,30	0,30	-0,30	0,30	-0,30	-0,30	0,30	-0,30	0,30	-0,30	0,30	-0,30
Corr. Tors. dir. 90	1,00	1,00	-1,00	-1,00	-1,00	-1,00	1,00	1,00	1,00	1,00	-1,00	-1,00	-1,00	-1,00	1,00
Sisma direz. grd 0	0,30	0,30	0,30	0,30	0,30	0,30	0,30	0,30	-0,30	-0,30	-0,30	-0,30	-0,30	-0,30	-0,30
Sisma direz. grd 90	1,00	1,00	1,00	1,00	-1,00	-1,00	-1,00	-1,00	1,00	1,00	1,00	1,00	-1,00	-1,00	-1,00

COMBINAZIONI CARICHI - S.L.U. - A1

DESCRIZIONI	46
Peso Strutturale	1,00
Perm.Non Strutturale	1,00
Var.Abitazioni	0,30
Var.Neve h<=1000	0,00
Vento dir. 0	0,00
Vento dir. 90	0,00
Vento dir. 180	0,00
Vento dir. 270	0,00
Corr. Tors. dir. 0	0,30
Corr. Tors. dir. 90	1,00
Sisma direz. grd 0	-0,30
Sisma direz. grd 90	-1,00

COMBINAZIONI RARE - S.L.E.

DESCRIZIONI	1	2	3	4	5	6	7	8	9	10	11	12	13	14
Peso Strutturale	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00
Perm.Non Strutturale	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00	1,00
Var.Abitazioni	1,00	0,70	1,00	0,70	0,70	1,00	0,70	0,70	1,00	0,70	0,70	1,00	0,70	0,70
Var.Neve h<=1000	0,50	1,00	0,50	1,00	0,50	0,50	1,00	0,50	0,50	1,00	0,50	0,50	1,00	0,50
Vento dir. 0	0,00	0,00	0,60	0,60	1,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
Vento dir. 90	0,00	0,00	0,00	0,00	0,00	0,60	0,60	1,00	0,00	0,00	0,00	0,00	0,00	0,00
Vento dir. 180	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,60	0,60	1,00	0,00	0,00	0,00
Vento dir. 270	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,60	0,60	1,00
Corr. Tors. dir. 0	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
Corr. Tors. dir. 90	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
Sisma direz. grd 0	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
Sisma direz. grd 90	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00

COMBINAZIONI FREQUENTI - S.L.E.

DESCRIZIONI	1	2	3	4	5	6
Peso Strutturale	1,00	1,00	1,00	1,00	1,00	1,00
Perm.Non Strutturale	1,00	1,00	1,00	1,00	1,00	1,00
Var.Abitazioni	0,50	0,30	0,30	0,30	0,30	0,30
Var.Neve h<=1000	0,00	0,20	0,00	0,00	0,00	0,00
Vento dir. 0	0,00	0,00	0,20	0,00	0,00	0,00
Vento dir. 90	0,00	0,00	0,00	0,20	0,00	0,00
Vento dir. 180	0,00	0,00	0,00	0,00	0,20	0,00
Vento dir. 270	0,00	0,00	0,00	0,00	0,00	0,20
Corr. Tors. dir. 0	0,00	0,00	0,00	0,00	0,00	0,00
Corr. Tors. dir. 90	0,00	0,00	0,00	0,00	0,00	0,00
Sisma direz. grd 0	0,00	0,00	0,00	0,00	0,00	0,00
Sisma direz. grd 90	0,00	0,00	0,00	0,00	0,00	0,00

COMBINAZIONI PERMANENTI - S.L.E.

DESCRIZIONI	1
Peso Strutturale	1,00
Perm.Non Strutturale	1,00
Var.Abitazioni	0,30
Var.Neve h<=1000	0,00
Vento dir. 0	0,00
Vento dir. 90	0,00
Vento dir. 180	0,00
Vento dir. 270	0,00
Corr. Tors. dir. 0	0,00
Corr. Tors. dir. 90	0,00
Sisma direz. grd 0	0,00
Sisma direz. grd 90	0,00

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU

Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
1	A1/1	13105	0	0	2300	11489
	A1/2	12942	0	0	2457	11504
	A1/3	13069	0	38	486	11413
	A1/4	12907	0	38	643	11428
	A1/5	12626	0	63	1455	11040
	A1/6	12941	49	0	2440	11131
	A1/7	12778	50	0	2283	11145
	A1/8	12411	82	0	3422	10569
	A1/9	13141	0	38	4119	11565
	A1/10	12978	0	38	4276	11580
	A1/11	12745	0	64	7510	11293
	A1/12	13270	50	0	7047	11848
	A1/13	13107	51	0	7204	11863
	A1/14	12960	85	0	12390	11764
	X+ A1/21	8900	116	402	110	7862
	X- A1/30	9645	126	435	37734	9458
2	Y+ A1/40	7737	338	105	22861	5305
	Y- A1/46	10278	448	139	50099	10850
2	A1/1	5830	0	0	34562	2102
	A1/2	5748	0	0	34550	2105
	A1/3	5803	17	0	33788	2033
	A1/4	5720	17	0	33777	2036
	A1/5	5601	28	0	32322	1939
	A1/6	5764	0	22	32893	2047
	A1/7	5681	0	22	32882	2050
	A1/8	5536	0	36	30831	1962
	A1/9	5858	17	0	35336	2171
	A1/10	5776	17	0	35324	2174
	A1/11	5693	29	0	34901	2169
	A1/12	5897	0	22	36231	2156
	A1/13	5814	0	23	36220	2160
	A1/14	5758	0	38	36394	2145
	X+ A1/20	3834	173	50	19323	917
	X- A1/27	4409	199	58	35370	2338
3	Y+ A1/41	3554	48	155	13295	1347
	Y- A1/43	4561	62	199	38646	2120
3	A1/1	7395	0	0	2961	741
	A1/2	7219	0	0	2992	738
	A1/3	7386	21	0	2945	763
	A1/4	7210	21	0	2976	760
	A1/5	7066	35	0	2937	772
	A1/6	7394	0	28	2482	737
	A1/7	7218	0	28	2514	734
	A1/8	7079	0	47	2166	729
	A1/9	7404	21	0	2977	719

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/10	7228	21	0	3009	716
	A1/11	7096	36	0	2992	699
	A1/12	7396	0	28	3440	745
	A1/13	7220	0	28	3472	742
	A1/14	7082	0	47	3763	743
	X+ A1/20	4780	216	63	2861	768
	X- A1/27	4966	224	65	3257	314
	Y+ A1/41	4896	66	214	1852	422
	Y- A1/43	4904	66	214	5735	498
4	A1/1	10517	0	0	306743	126
	A1/2	10255	0	0	307580	136
	A1/3	10514	30	0	307055	106
	A1/4	10251	30	0	307892	116
	A1/5	10078	50	0	300549	103
	A1/6	10503	0	40	303991	119
	A1/7	10240	0	40	304828	130
	A1/8	10060	0	66	295442	125
	A1/9	10521	30	0	306432	146
	A1/10	10258	30	0	307269	156
	A1/11	10090	51	0	299510	169
	A1/12	10531	0	40	309499	132
	A1/13	10269	0	40	310336	143
	A1/14	10107	0	67	304622	147
	X+ A1/21	6969	315	91	222426	91
	X- A1/30	7042	318	92	216173	320
	Y+ A1/40	6876	93	300	190463	118
	Y- A1/46	7093	96	309	233627	204
5	A1/1	10591	0	0	286597	770
	A1/2	10324	0	0	287160	767
	A1/3	10608	31	0	287997	709
	A1/4	10341	30	0	288561	707
	A1/5	10162	51	0	280083	650
	A1/6	10566	0	40	285770	778
	A1/7	10299	0	40	286333	775
	A1/8	10093	0	66	276370	764
	A1/9	10575	30	0	285200	830
	A1/10	10308	30	0	285763	828
	A1/11	10107	51	0	275420	851
	A1/12	10616	0	40	287430	762
	A1/13	10349	0	40	287993	759
	A1/14	10176	0	67	279137	737
	X+ A1/21	7219	326	94	210510	181
	X- A1/30	6880	311	90	181952	1060
	Y+ A1/31	6842	93	299	191007	363
	Y- A1/37	7244	98	316	206181	181

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
6	A1/1	8870	0	0	185011	388
	A1/2	8621	0	0	186274	388
	A1/3	8877	26	0	185279	385
	A1/4	8628	25	0	186543	385
	A1/5	8469	42	0	185222	364
	A1/6	8852	0	34	183505	386
	A1/7	8602	0	33	184769	386
	A1/8	8426	0	55	182265	365
	A1/9	8863	26	0	184743	390
	A1/10	8614	25	0	186006	390
	A1/11	8445	42	0	184327	372
	A1/12	8889	0	34	186518	389
	A1/13	8640	0	34	187781	390
	A1/14	8488	0	56	187287	371
	X+ A1/21	5900	266	77	144089	222
	X- A1/30	5752	260	75	138616	272
	Y+ A1/31	5660	77	247	126959	221
	Y- A1/37	5950	81	260	150479	249
7	A1/1	20271	0	0	144380	16728
	A1/2	20077	0	0	144746	16719
	A1/3	20328	59	0	146194	16915
	A1/4	20134	59	0	146560	16906
	A1/5	19795	99	0	148053	16535
	A1/6	20111	0	76	129583	16490
	A1/7	19917	0	77	129949	16481
	A1/8	19432	0	128	120368	15828
	A1/9	20214	58	0	142551	16542
	A1/10	20020	59	0	142917	16533
	A1/11	19604	98	0	141981	15914
	A1/12	20432	0	77	159182	16967
	A1/13	20238	0	79	159548	16958
	A1/14	19967	0	131	169699	16622
	X+ A1/20	14870	671	195	167735	13694
	X- A1/27	13676	617	179	128835	9826
	Y+ A1/34	12888	174	562	11402	9951
	Y- A1/36	15302	207	668	232121	13621
8	A1/1	12597	0	0	51142	9025
	A1/2	12458	0	0	51621	9030
	A1/3	12480	36	0	47988	8795
	A1/4	12340	36	0	48467	8800
	A1/5	12044	60	0	47731	8415
	A1/6	12446	0	47	46025	8861
	A1/7	12306	0	48	46504	8866

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/8	11988	0	79	44460	8525
	A1/9	12715	37	0	54302	9255
	A1/10	12575	37	0	54781	9260
	A1/11	12436	62	0	58255	9182
	A1/12	12749	0	48	56265	9188
	A1/13	12609	0	49	56744	9194
	A1/14	12492	0	82	61526	9071
	X+ A1/21	7778	351	102	22407	4084
	X- A1/30	10228	462	134	88063	8844
	Y+ A1/40	7859	106	343	14079	5593
	Y- A1/46	10189	138	445	92628	8015
9	A1/1	6502	0	0	59134	180
	A1/2	6337	0	0	59670	189
	A1/3	6514	19	0	59027	138
	A1/4	6349	19	0	59563	147
	A1/5	6242	31	0	60397	131
	A1/6	6520	0	25	59087	166
	A1/7	6355	0	25	59623	175
	A1/8	6253	0	41	60497	178
	A1/9	6491	19	0	59240	222
	A1/10	6326	19	0	59776	230
	A1/11	6204	31	0	60752	270
	A1/12	6484	0	25	59180	194
	A1/13	6319	0	25	59716	202
	A1/14	6193	0	41	60652	223
	X+ A1/18	4446	201	58	47202	247
	X- A1/25	4207	190	55	49316	617
	Y+ A1/34	4459	60	195	47937	3
	Y- A1/36	4184	57	183	48151	176
10	A1/1	11436	0	0	33682	10025
	A1/2	11284	0	0	33744	10033
	A1/3	11384	33	0	32981	9891
	A1/4	11232	33	0	33043	9899
	A1/5	10956	55	0	31434	9523
	A1/6	11463	0	43	32767	10021
	A1/7	11311	0	44	32830	10029
	A1/8	11087	0	73	31078	9739
	A1/9	11488	33	0	34383	10159
	A1/10	11337	33	0	34446	10167
	A1/11	11130	56	0	33771	9970
	A1/12	11410	0	43	34597	10029
	A1/13	11258	0	44	34660	10038
	A1/14	10999	0	72	34128	9753
	X+ A1/18	7257	328	95	13296	5466
	X- A1/25	8333	376	109	27818	8239

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	Y+ A1/41	8124	110	354	17952	7279
	Y- A1/43	7667	104	335	31707	7276
11	A1/1	6180	0	0	686	731
	A1/2	5999	0	0	682	730
	A1/3	6179	18	0	424	757
	A1/4	5997	18	0	420	755
	A1/5	5847	29	0	243	744
	A1/6	6191	0	23	154	730
	A1/7	6010	0	23	150	728
	A1/8	5868	0	39	207	699
	A1/9	6182	18	0	948	706
	A1/10	6000	18	0	945	704
	A1/11	5852	29	0	1117	659
	A1/12	6170	0	23	1218	733
	A1/13	5988	0	23	1214	731
	A1/14	5832	0	38	1567	704
	X+ A1/18	3935	178	52	3473	717
	X- A1/25	3967	179	52	1982	191
	Y+ A1/34	4005	54	175	4424	519
	Y- A1/43	3848	52	168	5371	396
12	A1/1	7499	0	0	1174	1174
	A1/2	7321	0	0	1215	1171
	A1/3	7508	22	0	1147	1119
	A1/4	7330	22	0	1188	1116
	A1/5	7194	36	0	1223	1052
	A1/6	7500	0	28	1463	1168
	A1/7	7322	0	28	1504	1165
	A1/8	7179	0	47	1750	1134
	A1/9	7490	22	0	1201	1229
	A1/10	7312	22	0	1242	1226
	A1/11	7163	36	0	1313	1235
	A1/12	7499	0	28	884	1179
	A1/13	7320	0	28	925	1176
	A1/14	7177	0	47	785	1152
	X+ A1/15	5031	227	66	1397	195
	X- A1/24	4839	218	63	1934	1334
	Y+ A1/31	4966	67	217	3158	570
	Y- A1/37	4960	67	216	1385	628
13	A1/1	6828	0	0	44998	401
	A1/2	6658	0	0	45619	402
	A1/3	6832	20	0	44835	417
	A1/4	6662	20	0	45456	418
	A1/5	6517	33	0	46057	425

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/6	6874	0	26	44440	401
	A1/7	6704	0	26	45061	402
	A1/8	6588	0	43	45399	399
	A1/9	6824	20	0	45160	385
	A1/10	6655	20	0	45781	386
	A1/11	6505	33	0	46599	372
	A1/12	6782	0	26	45556	401
	A1/13	6612	0	26	46177	402
	A1/14	6435	0	42	47258	399
	X+ A1/15	4587	207	60	33618	460
	X- A1/24	4514	204	59	36936	130
	Y+ A1/31	4804	65	210	31857	343
	Y- A1/37	4119	56	180	40089	349
14	A1/1	13968	0	0	10177	10832
	A1/2	13818	0	0	10564	10835
	A1/3	14061	40	0	13188	11029
	A1/4	13911	41	0	13575	11033
	A1/5	13689	68	0	18128	10868
	A1/6	14176	0	54	15731	11014
	A1/7	14025	0	54	16118	11018
	A1/8	13880	0	91	22366	10843
	A1/9	13876	40	0	7171	10634
	A1/10	13725	41	0	7558	10638
	A1/11	13380	67	0	8099	10210
	A1/12	13761	0	52	4626	10650
	A1/13	13611	0	53	5013	10653
	A1/14	13189	0	87	3857	10236
	X+ A1/15	11033	498	144	62231	9974
	X- A1/24	9141	413	120	522	5911
	Y+ A1/31	11444	155	499	69487	9486
	Y- A1/37	8448	114	369	11349	6894
15	A1/1	15799	0	0	243454	12459
	A1/2	15586	0	0	243504	12494
	A1/3	15697	45	0	236916	12281
	A1/4	15485	46	0	236967	12316
	A1/5	15149	76	0	228260	11865
	A1/6	15929	0	60	245054	12635
	A1/7	15716	0	61	245104	12670
	A1/8	15535	0	102	241822	12455
	A1/9	15900	46	0	250011	12638
	A1/10	15687	46	0	250062	12673
	A1/11	15487	78	0	250085	12460
	A1/12	15669	0	59	241861	12284
	A1/13	15456	0	60	241912	12319
	A1/14	15101	0	99	236501	11870

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	X+ A1/18	10115	457	132	101615	7214
	X- A1/25	12206	551	160	238447	10901
	Y+ A1/41	12211	165	533	197089	10598
	Y- A1/43	10141	137	442	176775	7818
16	A1/1	9055	0	0	125317	90
	A1/2	8803	0	0	126059	85
	A1/3	9061	26	0	126382	119
	A1/4	8809	26	0	127124	113
	A1/5	8641	43	0	127071	96
	A1/6	9048	0	34	121780	87
	A1/7	8796	0	34	122522	81
	A1/8	8620	0	57	119401	43
	A1/9	9049	26	0	124254	62
	A1/10	8797	26	0	124997	56
	A1/11	8621	43	0	123525	1
	A1/12	9062	0	34	128861	94
	A1/13	8810	0	34	129603	88
	A1/14	8643	0	57	131202	55
	X+ A1/21	5964	269	78	114193	266
	X- A1/30	5844	264	76	92461	329
	Y+ A1/31	5854	79	255	70521	23
	Y- A1/37	5958	81	260	126404	75
17	A1/1	8759	0	0	29105	353
	A1/2	8513	0	0	29672	349
	A1/3	8752	25	0	28734	356
	A1/4	8506	25	0	29301	352
	A1/5	8323	42	0	30899	347
	A1/6	8748	0	33	31230	361
	A1/7	8502	0	33	31797	357
	A1/8	8317	0	55	35059	355
	A1/9	8765	25	0	29475	350
	A1/10	8520	25	0	30042	346
	A1/11	8346	42	0	32133	337
	A1/12	8769	0	33	26976	345
	A1/13	8524	0	33	27543	341
	A1/14	8352	0	55	27969	328
	X+ A1/21	5622	254	74	17966	252
	X- A1/30	5761	260	75	25475	190
	Y+ A1/40	5604	76	245	44424	290
	Y- A1/46	5771	78	252	11028	171
18	A1/1	8991	0	0	33202	1206
	A1/2	8732	0	0	33913	1201
	A1/3	8993	26	0	34047	1152

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU

Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/4	8734	26	0	34758	1147
	A1/5	8550	43	0	37712	1055
	A1/6	9004	0	34	35810	1204
	A1/7	8745	0	34	36521	1199
	A1/8	8569	0	56	40649	1142
	A1/9	8989	26	0	32355	1261
	A1/10	8730	26	0	33066	1256
	A1/11	8544	43	0	34891	1237
	A1/12	8978	0	34	30591	1209
	A1/13	8719	0	34	31302	1204
	A1/14	8524	0	56	31951	1150
X+	A1/15	5845	264	77	47143	185
X-	A1/24	5806	262	76	29534	1321
Y+	A1/31	5902	80	258	54956	567
Y-	A1/37	5700	77	249	14967	616
19	A1/1	14180	0	0	134526	10566
	A1/2	13948	0	0	133781	10603
	A1/3	14179	41	0	134413	10601
	A1/4	13947	41	0	133668	10639
	A1/5	13667	68	0	126604	10334
	A1/6	14178	0	54	128317	10549
	A1/7	13946	0	54	127573	10587
	A1/8	13665	0	90	116444	10247
	A1/9	14181	41	0	134634	10531
	A1/10	13949	41	0	133889	10568
	A1/11	13671	68	0	126971	10216
	A1/12	14182	0	54	140736	10583
	A1/13	13950	0	54	139991	10620
	A1/14	13673	0	90	137142	10303
X+	A1/20	9484	428	124	96007	7556
X-	A1/27	9504	429	124	97888	6816
Y-	A1/36	9503	129	415	129429	7382
Y+	A1/41	9477	128	413	37206	6924
20	A1/1	15671	0	0	412735	10642
	A1/2	15441	0	0	414041	10701
	A1/3	15629	45	0	404239	10548
	A1/4	15399	45	0	405545	10607
	A1/5	15127	76	0	395242	10325
	A1/6	15696	0	59	423721	10689
	A1/7	15466	0	60	425027	10748
	A1/8	15239	0	100	427712	10561
	A1/9	15713	45	0	421254	10737
	A1/10	15483	46	0	422561	10796
	A1/11	15267	76	0	423601	10640
	A1/12	15646	0	59	401746	10595

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/13	15415	0	60	403052	10654
	A1/14	15155	0	100	391088	10404
	X+ A1/15	10362	468	136	240282	6713
	X- A1/24	11244	507	147	417881	8693
	Y+ A1/40	11061	150	483	413557	8234
	Y- A1/46	10723	145	468	250043	7600
21	A1/1	10535	0	0	407265	182
	A1/2	10263	0	0	408532	191
	A1/3	10524	30	0	405453	170
	A1/4	10253	30	0	406720	179
	A1/5	10053	50	1	397769	192
	A1/6	10565	1	40	408472	187
	A1/7	10294	1	40	409739	197
	A1/8	10121	1	67	402800	221
	A1/9	10545	30	0	409085	193
	A1/10	10274	30	0	410352	203
	A1/11	10088	51	1	403822	232
	A1/12	10504	1	40	406062	176
	A1/13	10233	1	40	407329	186
	A1/14	10019	1	66	398784	202
	X+ A1/15	6872	312	85	272663	113
	X- A1/24	7095	322	88	310819	363
	Y+ A1/40	7180	102	312	303458	301
	Y- A1/46	6716	96	292	287207	234
22	A1/1	10972	0	0	425613	695
	A1/2	10696	0	0	427018	690
	A1/3	10973	32	0	426631	643
	A1/4	10696	32	0	428036	639
	A1/5	10478	52	0	420284	557
	A1/6	10984	0	42	427354	694
	A1/7	10707	0	42	428759	690
	A1/8	10496	0	69	421489	642
	A1/9	10972	32	0	424591	746
	A1/10	10695	32	0	425996	741
	A1/11	10476	52	0	416884	728
	A1/12	10961	0	42	423868	695
	A1/13	10684	0	41	425273	690
	A1/14	10458	0	69	415679	643
	X+ A1/18	7197	325	94	315240	202
	X- A1/25	7181	324	94	293873	871
	Y+ A1/34	7253	98	316	317518	150
	Y- A1/36	7078	96	309	290006	198
23	A1/1	12498	0	0	264188	570

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/2	12234	0	0	264801	556
	A1/3	12497	36	0	264065	608
	A1/4	12232	36	0	264677	594
	A1/5	12000	60	0	257147	592
	A1/6	12508	0	47	269298	566
	A1/7	12244	0	47	269911	553
	A1/8	12019	0	79	265869	523
	A1/9	12500	36	0	264317	532
	A1/10	12236	36	0	264930	518
	A1/11	12006	60	0	257568	466
	A1/12	12489	0	47	259078	573
	A1/13	12225	0	47	259690	560
	A1/14	11987	0	79	248836	535
	X+ A1/15	8305	375	109	191681	682
	X- A1/24	8343	377	109	194731	115
	Y+ A1/40	8380	113	366	220536	153
	Y- A1/46	8237	112	359	144616	168
24	A1/1	21574	0	0	47404	1637
	A1/2	21444	0	0	47074	1629
	A1/3	21563	62	0	48238	1392
	A1/4	21433	63	0	47907	1384
	A1/5	20947	105	0	45605	1071
	A1/6	21582	0	82	69683	1652
	A1/7	21453	0	83	69352	1644
	A1/8	20980	0	138	81346	1504
	A1/9	21585	62	0	46610	1883
	A1/10	21455	63	0	46279	1875
	A1/11	20984	105	0	42891	1888
	A1/12	21565	0	82	25138	1622
	A1/13	21436	0	83	24808	1614
	A1/14	20951	0	138	7105	1454
	X+ A1/15	14662	662	192	99824	1514
	X- A1/24	14893	672	195	86375	3629
	Y+ A1/40	14856	201	648	206536	1856
	Y- A1/43	14704	199	642	155895	1299
25	A1/1	17603	0	0	3412	13263
	A1/2	17402	0	0	3639	13356
	A1/3	17749	51	0	2647	13502
	A1/4	17548	52	0	2874	13595
	A1/5	17383	87	0	2976	13491
	A1/6	17603	0	67	29274	13260
	A1/7	17402	0	67	29047	13353
	A1/8	17139	0	113	50225	13087
	A1/9	17456	50	0	4128	13024
	A1/10	17255	51	0	4356	13117

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/11	16895	85	0	5446	12694
	A1/12	17602	0	67	36088	13266
	A1/13	17402	0	68	36315	13359
	A1/14	17139	0	113	58711	13098
	X+ A1/20	13828	624	181	91752	12173
	X- A1/27	10754	485	141	102961	7157
	Y+ A1/34	12871	174	562	212218	10578
	Y- A1/36	12720	172	555	266014	10384
26	A1/1	14506	0	0	1288	14078
	A1/2	14332	0	0	1534	14073
	A1/3	14514	0	42	1563	14098
	A1/4	14340	0	42	1809	14093
	A1/5	13966	0	70	3174	13617
	A1/6	14420	55	0	680	13823
	A1/7	14246	55	0	926	13818
	A1/8	13810	91	0	1703	13160
	A1/9	14497	0	42	1015	14058
	A1/10	14323	0	42	1261	14053
	A1/11	13938	0	70	2261	13550
	A1/12	14591	55	0	1899	14332
	A1/13	14417	56	0	2145	14327
	A1/14	14095	93	0	3733	14008
	X+ A1/21	9886	129	446	10022	10147
	X- A1/30	9719	127	439	4583	9744
	Y+ A1/31	8963	391	121	1434	7440
	Y- A1/37	10300	449	139	11993	11405
27	A1/1	14554	0	0	98222	13993
	A1/2	14337	0	0	98105	14004
	A1/3	14608	0	42	101881	14044
	A1/4	14391	0	42	101764	14056
	A1/5	14073	0	70	99561	13578
	A1/6	14385	54	0	104695	13590
	A1/7	14168	55	0	104578	13602
	A1/8	13701	90	0	104251	12821
	A1/9	14500	0	42	94575	13941
	A1/10	14283	0	42	94458	13953
	A1/11	13892	0	70	87384	13407
	A1/12	14723	56	0	91758	14396
	A1/13	14506	56	0	91641	14408
	A1/14	14264	94	0	82689	14165
	X+ A1/21	10601	139	478	92954	10636
	X- A1/30	9486	124	428	18688	9574
	Y+ A1/31	8511	371	115	127064	6267
	Y- A1/37	11136	486	151	36363	12416

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
28	A1/1	18233	0	0	375977	16270
	A1/2	17999	0	0	376584	16312
	A1/3	18256	0	53	377675	16297
	A1/4	18022	0	53	378282	16338
	A1/5	17682	0	88	373873	15875
	A1/6	17857	68	0	359051	15574
	A1/7	17624	68	0	359658	15615
	A1/8	17018	112	0	342832	14671
	A1/9	18210	0	52	374242	16243
	A1/10	17976	0	53	374849	16284
	A1/11	17606	0	88	368151	15786
	A1/12	18609	71	0	392890	16967
	A1/13	18375	71	0	393497	17008
	A1/14	18271	120	0	399231	16991
	X+ A1/20	13578	178	613	338622	13195
	X- A1/27	13069	171	590	300124	12576
	Y+ A1/34	9796	427	133	168398	6315
	Y- A1/36	15375	671	208	412640	16634
29	A1/1	12886	0	0	215995	8494
	A1/2	12707	0	0	216829	8548
	A1/3	12810	0	37	211243	8371
	A1/4	12630	0	37	212077	8425
	A1/5	12417	0	62	205917	8219
	A1/6	12757	48	0	205030	8247
	A1/7	12578	49	0	205864	8301
	A1/8	12330	81	0	195562	8012
	A1/9	12963	0	37	220768	8618
	A1/10	12783	0	38	221602	8672
	A1/11	12671	0	63	221792	8631
	A1/12	13015	49	0	226983	8742
	A1/13	12835	50	0	227817	8796
	A1/14	12759	84	0	232151	8837
	X+ A1/21	8447	111	381	137608	5485
	X- A1/30	10040	131	453	237683	8063
	Y+ A1/40	8195	358	111	90826	4681
	Y- A1/46	10180	444	138	264112	8505
30	A1/1	9181	0	0	239067	539
	A1/2	8957	0	0	240297	547
	A1/3	9161	0	26	236940	535
	A1/4	8937	0	26	238170	543
	A1/5	8751	0	44	233870	552
	A1/6	9177	35	0	236251	489
	A1/7	8953	35	0	237482	496

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/8	8777	58	0	232722	474
	A1/9	9200	0	27	241198	544
	A1/10	8976	0	26	242428	551
	A1/11	8816	0	44	240967	566
	A1/12	9184	35	0	241886	590
	A1/13	8960	35	0	243116	598
	A1/14	8789	58	0	242114	643
	X+ A1/20	5841	76	264	158095	485
	X- A1/27	6246	82	282	202375	583
	Y+ A1/41	6073	265	82	158692	16
	Y- A1/43	6122	267	83	201993	827
31	A1/1	6945	0	0	20027	922
	A1/2	6752	0	0	20239	919
	A1/3	6946	0	20	18711	909
	A1/4	6753	0	20	18924	906
	A1/5	6611	0	33	18905	855
	A1/6	6955	26	0	19441	927
	A1/7	6762	26	0	19654	924
	A1/8	6626	44	0	20122	885
	A1/9	6944	0	20	21343	936
	A1/10	6751	0	20	21555	933
	A1/11	6608	0	33	23291	900
	A1/12	6936	26	0	20611	918
	A1/13	6743	26	0	20824	915
	A1/14	6594	43	0	22072	870
	X+ A1/18	4526	59	204	3562	460
	X- A1/25	4505	59	203	30740	741
	Y+ A1/41	4564	199	62	18481	672
	Y- A1/43	4416	193	60	26643	593
32	A1/1	7423	0	0	5709	1719
	A1/2	7242	0	0	5623	1717
	A1/3	7417	0	21	5270	1717
	A1/4	7237	0	21	5185	1714
	A1/5	7096	0	35	4609	1666
	A1/6	7414	28	0	5331	1741
	A1/7	7233	28	0	5245	1739
	A1/8	7090	47	0	4710	1706
	A1/9	7428	0	21	6147	1721
	A1/10	7247	0	21	6062	1719
	A1/11	7113	0	36	6070	1673
	A1/12	7432	28	0	6086	1697
	A1/13	7251	28	0	6001	1695
	A1/14	7119	47	0	5969	1633
	X+ A1/20	4849	63	219	19	1091
	X- A1/27	4959	65	224	9019	1136

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU

Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	Y+ A1/41	4836	211	65	2371	1341
	Y- A1/43	4966	217	67	7805	1002
33	A1/1	8105	0	0	24321	1676
	A1/2	7873	0	0	24753	1676
	A1/3	8127	0	23	25935	1681
	A1/4	7894	0	23	26368	1681
	A1/5	7744	0	39	29162	1632
	A1/6	8109	31	0	22704	1745
	A1/7	7877	31	0	23137	1745
	A1/8	7714	51	0	23776	1739
	A1/9	8083	0	23	22706	1671
	A1/10	7851	0	23	23139	1671
	A1/11	7671	0	38	23779	1615
	A1/12	8101	31	0	25941	1607
	A1/13	7868	31	0	26374	1607
	A1/14	7700	51	0	29171	1508
	X+ A1/21	5465	72	247	44861	1032
	X- A1/30	5015	66	226	11487	932
	Y+ A1/31	5340	233	72	16691	1676
	Y- A1/37	5294	231	72	42242	635
34	A1/1	10212	0	0	347909	1982
	A1/2	9955	0	0	349821	1983
	A1/3	10224	0	29	348709	1996
	A1/4	9966	0	29	350621	1997
	A1/5	9777	0	49	346655	1943
	A1/6	10240	39	0	349348	2101
	A1/7	9983	39	0	351260	2101
	A1/8	9805	64	0	347720	2118
	A1/9	10201	0	29	347111	1968
	A1/10	9944	0	29	349023	1969
	A1/11	9740	0	49	343992	1897
	A1/12	10185	39	0	346471	1864
	A1/13	9927	39	0	348384	1864
	A1/14	9712	64	0	342925	1723
	X+ A1/15	6878	90	310	265575	1788
	X- A1/24	6650	87	300	249331	1515
	Y+ A1/31	6943	303	94	267213	2312
	Y- A1/37	6538	285	89	247000	568
35	A1/1	8710	0	0	203169	727
	A1/2	8488	0	0	204345	727
	A1/3	8692	0	25	202618	725
	A1/4	8470	0	25	203794	725
	A1/5	8304	0	42	201702	679

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/6	8739	33	0	205334	685
	A1/7	8517	33	0	206510	684
	A1/8	8383	55	0	206228	611
	A1/9	8728	0	25	203715	729
	A1/10	8506	0	25	204891	729
	A1/11	8365	0	42	203529	686
	A1/12	8681	33	0	200996	770
	A1/13	8459	33	0	202172	769
	A1/14	8286	55	0	198998	753
	X+ A1/18	5652	74	255	152326	266
	X- A1/25	6024	79	272	163225	319
	Y+ A1/41	6064	265	82	172208	56
	Y- A1/43	5590	244	76	136638	740
36	A1/1	7153	0	0	25970	770
	A1/2	6959	0	0	26272	769
	A1/3	7148	0	21	25033	767
	A1/4	6953	0	20	25335	766
	A1/5	6796	0	34	25572	738
	A1/6	7159	27	0	25530	750
	A1/7	6965	27	0	25832	749
	A1/8	6815	45	0	26400	710
	A1/9	7158	0	21	26910	773
	A1/10	6964	0	21	27212	772
	A1/11	6814	0	34	28700	749
	A1/12	7147	27	0	26412	790
	A1/13	6953	27	0	26713	789
	A1/14	6795	45	0	27869	777
	X+ A1/18	4579	60	207	11355	419
	X- A1/25	4692	61	212	30870	485
	Y+ A1/41	4687	204	63	21634	350
	Y- A1/43	4590	200	62	28468	666
37	A1/1	7571	0	0	4155	1212
	A1/2	7391	0	0	4050	1212
	A1/3	7566	0	22	3747	1213
	A1/4	7386	0	22	3642	1213
	A1/5	7241	0	36	3066	1191
	A1/6	7578	29	0	4643	1184
	A1/7	7399	29	0	4538	1184
	A1/8	7262	48	0	4559	1142
	A1/9	7576	0	22	4564	1211
	A1/10	7396	0	22	4459	1211
	A1/11	7258	0	36	4428	1187
	A1/12	7564	29	0	3667	1240
	A1/13	7384	29	0	3562	1240
	A1/14	7237	48	0	2933	1236

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	X+ A1/18	4949	65	223	934	789
	X- A1/25	5053	66	228	7540	770
	Y+ A1/41	5056	221	68	7215	626
	Y- A1/43	4944	216	67	303	1056
38	A1/1	8793	0	0	53751	118
	A1/2	8572	0	0	54398	112
	A1/3	8805	0	25	51556	125
	A1/4	8583	0	25	52203	119
	A1/5	8443	0	42	50371	97
	A1/6	8823	33	0	54879	107
	A1/7	8601	33	0	55525	101
	A1/8	8472	56	0	55909	67
	A1/9	8782	0	25	55950	111
	A1/10	8560	0	25	56597	105
	A1/11	8404	0	42	57694	75
	A1/12	8764	33	0	52623	129
	A1/13	8543	33	0	53269	124
	A1/14	8375	55	0	52149	105
	X+ A1/15	6005	79	271	20531	60
	X- A1/24	5763	75	260	66201	79
	Y+ A1/31	6075	265	82	42511	50
	Y- A1/37	5636	246	76	25444	129
39	A1/1	14348	0	0	270032	8797
	A1/2	14141	0	0	271004	8854
	A1/3	14397	0	41	274823	8863
	A1/4	14190	0	42	275795	8921
	A1/5	13995	0	70	276557	8807
	A1/6	14518	55	0	284458	9016
	A1/7	14311	55	0	285430	9073
	A1/8	14197	93	0	292615	9061
	A1/9	14299	0	41	265262	8731
	A1/10	14092	0	42	266233	8788
	A1/11	13833	0	69	260621	8587
	A1/12	14179	54	0	255617	8579
	A1/13	13971	54	0	256588	8636
	A1/14	13631	90	0	244546	8333
	X+ A1/15	10781	141	487	289938	7600
	X- A1/24	9788	128	442	193001	6257
	Y+ A1/31	11316	494	153	330623	8265
	Y- A1/37	8841	386	120	122245	5084
40	A1/1	13423	0	0	273815	9143
	A1/2	13227	0	0	274299	9173
	A1/3	13378	0	39	268612	9079

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/4	13183	0	39	269096	9109
	A1/5	12925	0	65	261367	8832
	A1/6	13475	51	0	282104	9252
	A1/7	13279	51	0	282588	9282
	A1/8	13086	86	0	283854	9120
	A1/9	13467	0	39	279016	9207
	A1/10	13271	0	39	279499	9236
	A1/11	13073	0	65	278707	9045
	A1/12	13370	51	0	265508	9034
	A1/13	13175	51	0	265992	9063
	A1/14	12912	85	0	256194	8756
X+	A1/18	8814	115	398	165898	5973
X-	A1/25	9730	127	439	273035	7283
Y+	A1/41	9704	423	131	282153	7441
Y-	A1/43	8875	387	120	150836	5706
41	A1/1	7331	0	0	66169	313
	A1/2	7139	0	0	66644	321
	A1/3	7345	0	21	67251	315
	A1/4	7153	0	21	67726	323
	A1/5	7010	0	35	68189	334
	A1/6	7319	28	0	65114	348
	A1/7	7127	28	0	65589	356
	A1/8	6968	46	0	64627	390
	A1/9	7318	0	21	65085	311
	A1/10	7126	0	21	65560	320
	A1/11	6966	0	35	64579	329
	A1/12	7343	28	0	67225	278
	A1/13	7151	28	0	67700	286
	A1/14	7008	46	0	68145	273
X+	A1/20	4925	64	222	63366	226
X-	A1/27	4646	61	210	40867	190
Y+	A1/34	4709	205	64	45027	574
Y-	A1/36	4891	213	66	61129	23
42	A1/1	6774	0	0	11355	676
	A1/2	6575	0	0	11145	672
	A1/3	6758	0	19	10533	676
	A1/4	6559	0	19	10323	673
	A1/5	6377	0	32	8919	647
	A1/6	6777	26	0	11139	635
	A1/7	6578	26	0	10928	632
	A1/8	6408	42	0	9929	579
	A1/9	6790	0	20	12180	675
	A1/10	6591	0	19	11969	672
	A1/11	6430	0	32	11664	646
	A1/12	6771	26	0	11573	716

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/13	6572	26	0	11362	713
	A1/14	6398	42	0	10652	714
	X+ A1/15	4121	54	186	2853	351
	X- A1/30	4440	58	200	15515	537
	Y+ A1/40	4350	190	59	7062	131
	Y- A1/46	4312	188	58	10918	759
43	A1/1	8497	0	0	135585	1580
	A1/2	8268	0	0	136388	1579
	A1/3	8496	0	24	133771	1580
	A1/4	8267	0	24	134573	1579
	A1/5	8101	0	41	131937	1530
	A1/6	8489	32	0	134577	1553
	A1/7	8259	32	0	135379	1551
	A1/8	8088	53	0	133280	1485
	A1/9	8497	0	24	137404	1580
	A1/10	8268	0	24	138207	1579
	A1/11	8103	0	41	137993	1531
	A1/12	8505	32	0	136596	1608
	A1/13	8276	32	0	137399	1606
	A1/14	8116	53	0	136646	1576
	X+ A1/21	5540	73	250	83642	1107
	X- A1/30	5550	73	250	121525	1111
	Y+ A1/40	5466	238	74	97884	840
	Y- A1/46	5590	244	76	114011	1253
44	A1/1	22132	0	0	507433	11595
	A1/2	21930	0	0	509705	11516
	A1/3	22105	0	64	502138	11583
	A1/4	21902	0	65	504410	11504
	A1/5	21290	0	106	485604	11067
	A1/6	21990	83	0	497251	11285
	A1/7	21787	84	0	499523	11206
	A1/8	21099	139	0	477459	10570
	A1/9	22160	0	64	512724	11606
	A1/10	21957	0	65	514996	11527
	A1/11	21382	0	107	503248	11106
	A1/12	22275	84	0	517615	11905
	A1/13	22072	86	0	519887	11826
	A1/14	21573	142	0	511399	11603
	X+ A1/20	14799	194	668	318778	8182
	X- A1/27	15358	201	693	427708	8381
	Y+ A1/41	13815	603	187	292567	5395
	Y- A1/43	15905	694	215	442939	9926
45	A1/1	15918	0	0	78547	10640

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/2	15798	0	0	78734	10575
	A1/3	15988	0	46	75525	10691
	A1/4	15868	0	47	75713	10626
	A1/5	15553	0	78	68691	10295
	A1/6	15662	59	0	82018	10180
	A1/7	15543	60	0	82205	10115
	A1/8	15011	99	0	79512	9444
	A1/9	15848	0	46	81586	10589
	A1/10	15728	0	46	81773	10524
	A1/11	15319	0	77	78792	10125
	A1/12	16173	61	0	75084	11100
	A1/13	16054	62	0	75271	11035
	A1/14	15862	104	0	67955	10977
	X+ A1/20	12352	162	558	1307	8882
	X- A1/27	10844	142	489	65392	7736
	Y+ A1/34	9494	414	129	53682	4250
	Y- A1/36	13136	573	178	6379	10851
46	A1/1	15507	0	0	50116	13168
	A1/2	15345	0	0	50625	13158
	A1/3	15428	0	44	47957	13072
	A1/4	15265	0	45	48466	13062
	A1/5	14903	0	75	49568	12598
	A1/6	15672	59	0	56228	13561
	A1/7	15509	60	0	56737	13551
	A1/8	15309	101	0	63352	13414
	A1/9	15587	0	45	52274	13265
	A1/10	15424	0	46	52783	13255
	A1/11	15168	0	76	56763	12919
	A1/12	15342	58	0	43994	12775
	A1/13	15180	59	0	44503	12765
	A1/14	14760	97	0	42963	12103
	X+ A1/15	10097	132	456	35848	8648
	X- A1/24	11752	154	530	80366	10635
	Y+ A1/40	12049	526	163	97810	12059
	Y- A1/46	9552	417	129	2800	5967
47	A1/1	15879	0	0	16359	16971
	A1/2	15698	0	0	16193	16967
	A1/3	15861	0	46	16302	16951
	A1/4	15680	0	46	16136	16947
	A1/5	15251	0	76	15126	16363
	A1/6	15953	60	0	16323	17195
	A1/7	15772	61	0	16156	17191
	A1/8	15403	101	0	15159	16770
	A1/9	15896	0	46	16417	16991
	A1/10	15715	0	46	16251	16987

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	A1/11	15309	0	77	15317	16430
	A1/12	15804	60	0	16397	16747
	A1/13	15624	61	0	16231	16742
	A1/14	15157	100	0	15283	16023
	X+ A1/15	10485	137	473	9466	11520
	X- A1/24	10851	142	490	10857	11934
	Y+ A1/40	11116	485	151	9970	12989
	Y- A1/46	10000	436	135	11509	9556
48	A1/1	19317	0	0	50115	21969
	A1/2	19107	0	0	50069	21950
	A1/3	19332	0	56	46324	21979
	A1/4	19121	0	56	46277	21960
	A1/5	18652	0	93	41250	21167
	A1/6	19449	74	0	52814	22329
	A1/7	19238	75	0	52768	22310
	A1/8	18847	124	0	52068	21750
	A1/9	19303	0	56	53930	21959
	A1/10	19093	0	56	53884	21940
	A1/11	18605	0	93	53927	21134
	A1/12	19186	73	0	47428	21609
	A1/13	18976	74	0	47382	21590
	A1/14	18410	121	0	43091	20550
	X+ A1/18	13298	174	600	11981	15187
	X- A1/24	13016	170	587	83861	15119
	Y+ A1/40	13819	603	187	68486	17097
	Y- A1/46	11821	516	160	34972	11663
49	A1/1	25965	0	0	218433	21613
	A1/2	25759	0	0	220347	21514
	A1/3	25952	0	75	213923	21618
	A1/4	25745	0	76	215837	21518
	A1/5	24991	0	125	206584	20678
	A1/6	26192	99	0	223131	22108
	A1/7	25985	101	0	225046	22008
	A1/8	25392	167	0	221932	21495
	A1/9	25980	0	75	222980	21610
	A1/10	25773	0	76	224895	21510
	A1/11	25038	0	125	221680	20664
	A1/12	25739	98	0	213757	21119
	A1/13	25533	99	0	215671	21019
	A1/14	24637	162	0	206307	19846
	X+ A1/15	17641	231	796	125437	15162
	X- A1/24	17965	235	811	222169	15135
	Y+ A1/40	19030	830	258	210620	17730
	Y- A1/46	15726	686	213	152245	10453

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLU

Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
50	A1/1	16139	0	0	90985	11085
	A1/2	16015	0	0	91162	11013
	A1/3	16224	0	47	87836	11164
	A1/4	16099	0	47	88013	11091
	A1/5	15769	0	79	80407	10739
	A1/6	16400	62	0	87775	11552
	A1/7	16275	63	0	87952	11480
	A1/8	16063	106	0	80304	11386
	A1/9	16055	0	46	94140	11008
	A1/10	15931	0	47	94317	10935
	A1/11	15489	0	78	90913	10479
	A1/12	15879	60	0	94200	10619
	A1/13	15754	61	0	94377	10547
	A1/14	15195	100	0	91012	9831
	X+ A1/15	12433	163	561	14562	9207
	X- A1/24	10705	140	483	80181	7647
	Y+ A1/31	13199	576	179	20213	11094
	Y- A1/37	9326	407	126	69976	4262

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD

Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
1	SLD/1	13105	0	0	2300	11489
	SLD/2	12942	0	0	2457	11504
	SLD/3	13069	0	38	486	11413
	SLD/4	12907	0	38	643	11428
	SLD/5	12626	0	63	1455	11040
	SLD/6	12941	49	0	2440	11131
	SLD/7	12778	50	0	2283	11145
	SLD/8	12411	82	0	3422	10569
	SLD/9	13141	0	38	4119	11565
	SLD/10	12978	0	38	4276	11580
	SLD/11	12745	0	64	7510	11293
	SLD/12	13270	50	0	7047	11848
	SLD/13	13107	51	0	7204	11863
	SLD/14	12960	85	0	12390	11764
	X+ SLD/21	8924	133	444	1224	7920
	X- SLD/30	9827	147	489	44630	9853
	Y+ SLD/40	7446	370	111	30755	4673
	Y- SLD/46	10631	529	159	60693	11622
2	SLD/1	5830	0	0	34562	2102
	SLD/2	5748	0	0	34550	2105
	SLD/3	5803	17	0	33788	2033

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/4	5720	17	0	33777	2036
	SLD/5	5601	28	0	32322	1939
	SLD/6	5764	0	22	32893	2047
	SLD/7	5681	0	22	32882	2050
	SLD/8	5536	0	36	30831	1962
	SLD/9	5858	17	0	35336	2171
	SLD/10	5776	17	0	35324	2174
	SLD/11	5693	29	0	34901	2169
	SLD/12	5897	0	22	36231	2156
	SLD/13	5814	0	23	36220	2160
	SLD/14	5758	0	38	36394	2145
	X+ SLD/20	3813	190	57	18618	810
	X- SLD/27	4509	224	67	38063	2532
	Y+ SLD/41	3447	51	171	10631	1312
	Y- SLD/43	4709	70	234	42405	2281
3	SLD/1	7395	0	0	2961	741
	SLD/2	7219	0	0	2992	738
	SLD/3	7386	21	0	2945	763
	SLD/4	7210	21	0	2976	760
	SLD/5	7066	35	0	2937	772
	SLD/6	7394	0	28	2482	737
	SLD/7	7218	0	28	2514	734
	SLD/8	7079	0	47	2166	729
	SLD/9	7404	21	0	2977	719
	SLD/10	7228	21	0	3009	716
	SLD/11	7096	36	0	2992	699
	SLD/12	7396	0	28	3440	745
	SLD/13	7220	0	28	3472	742
	SLD/14	7082	0	47	3763	743
	X+ SLD/20	4762	237	71	3047	816
	X- SLD/27	4987	248	74	3526	267
	Y+ SLD/41	4902	73	244	2877	396
	Y- SLD/43	4912	73	244	6632	490
4	SLD/1	10517	0	0	306743	126
	SLD/2	10255	0	0	307580	136
	SLD/3	10514	30	0	307055	106
	SLD/4	10251	30	0	307892	116
	SLD/5	10078	50	0	300549	103
	SLD/6	10503	0	40	303991	119
	SLD/7	10240	0	40	304828	130
	SLD/8	10060	0	66	295442	125
	SLD/9	10521	30	0	306432	146
	SLD/10	10258	30	0	307269	156
	SLD/11	10090	51	0	299510	169
	SLD/12	10531	0	40	309499	132

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/13	10269	0	40	310336	143
	SLD/14	10107	0	67	304622	147
	X+ SLD/21	6970	347	104	224977	135
	X- SLD/30	7059	351	105	217401	363
	Y+ SLD/40	6851	102	341	185108	115
	Y- SLD/46	7124	106	354	239209	223
5	SLD/1	10591	0	0	286597	770
	SLD/2	10324	0	0	287160	767
	SLD/3	10608	31	0	287997	709
	SLD/4	10341	30	0	288561	707
	SLD/5	10162	51	0	280083	650
	SLD/6	10566	0	40	285770	778
	SLD/7	10299	0	40	286333	775
	SLD/8	10093	0	66	276370	764
	SLD/9	10575	30	0	285200	830
	SLD/10	10308	30	0	285763	828
	SLD/11	10107	51	0	275420	851
	SLD/12	10616	0	40	287430	762
	SLD/13	10349	0	40	287993	759
	SLD/14	10176	0	67	279137	737
	X+ SLD/21	7275	362	108	214671	332
	X- SLD/30	6864	341	102	180067	1171
	Y+ SLD/31	6808	102	338	190696	330
	Y- SLD/37	7311	109	363	209714	102
6	SLD/1	8870	0	0	185011	388
	SLD/2	8621	0	0	186274	388
	SLD/3	8877	26	0	185279	385
	SLD/4	8628	25	0	186543	385
	SLD/5	8469	42	0	185222	364
	SLD/6	8852	0	34	183505	386
	SLD/7	8602	0	33	184769	386
	SLD/8	8426	0	55	182265	365
	SLD/9	8863	26	0	184743	390
	SLD/10	8614	25	0	186006	390
	SLD/11	8445	42	0	184327	372
	SLD/12	8889	0	34	186518	389
	SLD/13	8640	0	34	187781	390
	SLD/14	8488	0	56	187287	371
	X+ SLD/21	5928	295	88	145678	218
	X- SLD/30	5748	286	86	139047	278
	Y+ SLD/31	5630	84	280	124299	216
	Y- SLD/37	5993	89	298	153778	252
7	SLD/1	20271	0	0	144380	16728

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/2	20077	0	0	144746	16719
	SLD/3	20328	59	0	146194	16915
	SLD/4	20134	59	0	146560	16906
	SLD/5	19795	99	0	148053	16535
	SLD/6	20111	0	76	129583	16490
	SLD/7	19917	0	77	129949	16481
	SLD/8	19432	0	128	120368	15828
	SLD/9	20214	58	0	142551	16542
	SLD/10	20020	59	0	142917	16533
	SLD/11	19604	98	0	141981	15914
	SLD/12	20432	0	77	159182	16967
	SLD/13	20238	0	79	159548	16958
	SLD/14	19967	0	131	169699	16622
	X+ SLD/20	15096	751	225	181425	14237
	X- SLD/27	13649	679	204	134290	9550
	Y+ SLD/34	12630	188	628	13842	9601
	Y- SLD/36	15656	234	778	262805	14200
8	SLD/1	12597	0	0	51142	9025
	SLD/2	12458	0	0	51621	9030
	SLD/3	12480	36	0	47988	8795
	SLD/4	12340	36	0	48467	8800
	SLD/5	12044	60	0	47731	8415
	SLD/6	12446	0	47	46025	8861
	SLD/7	12306	0	48	46504	8866
	SLD/8	11988	0	79	44460	8525
	SLD/9	12715	37	0	54302	9255
	SLD/10	12575	37	0	54781	9260
	SLD/11	12436	62	0	58255	9182
	SLD/12	12749	0	48	56265	9188
	SLD/13	12609	0	49	56744	9194
	SLD/14	12492	0	82	61526	9071
	X+ SLD/21	7612	378	114	18525	3655
	X- SLD/30	10580	526	158	98080	9422
	Y+ SLD/40	7647	114	380	6315	5415
	Y- SLD/46	10567	158	525	104768	8451
9	SLD/1	6502	0	0	59134	180
	SLD/2	6337	0	0	59670	189
	SLD/3	6514	19	0	59027	138
	SLD/4	6349	19	0	59563	147
	SLD/5	6242	31	0	60397	131
	SLD/6	6520	0	25	59087	166
	SLD/7	6355	0	25	59623	175
	SLD/8	6253	0	41	60497	178
	SLD/9	6491	19	0	59240	222
	SLD/10	6326	19	0	59776	230

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/11	6204	31	0	60752	270
	SLD/12	6484	0	25	59180	194
	SLD/13	6319	0	25	59716	202
	SLD/14	6193	0	41	60652	223
	X+ SLD/15	4482	223	67	45863	414
	X- SLD/24	4192	208	63	48424	633
	Y+ SLD/31	4501	67	224	46567	133
	Y- SLD/37	4157	62	207	46834	92
10	SLD/1	11436	0	0	33682	10025
	SLD/2	11284	0	0	33744	10033
	SLD/3	11384	33	0	32981	9891
	SLD/4	11232	33	0	33043	9899
	SLD/5	10956	55	0	31434	9523
	SLD/6	11463	0	43	32767	10021
	SLD/7	11311	0	44	32830	10029
	SLD/8	11087	0	73	31078	9739
	SLD/9	11488	33	0	34383	10159
	SLD/10	11337	33	0	34446	10167
	SLD/11	11130	56	0	33771	9970
	SLD/12	11410	0	43	34597	10029
	SLD/13	11258	0	44	34660	10038
	SLD/14	10999	0	72	34128	9753
	X+ SLD/18	7172	357	107	11285	5188
	X- SLD/25	8476	421	126	28881	8548
	Y+ SLD/41	8230	123	409	16732	7387
	Y- SLD/43	7658	114	381	33972	7383
11	SLD/1	6180	0	0	686	731
	SLD/2	5999	0	0	682	730
	SLD/3	6179	18	0	424	757
	SLD/4	5997	18	0	420	755
	SLD/5	5847	29	0	243	744
	SLD/6	6191	0	23	154	730
	SLD/7	6010	0	23	150	728
	SLD/8	5868	0	39	207	699
	SLD/9	6182	18	0	948	706
	SLD/10	6000	18	0	945	704
	SLD/11	5852	29	0	1117	659
	SLD/12	6170	0	23	1218	733
	SLD/13	5988	0	23	1214	731
	SLD/14	5832	0	38	1567	704
	X+ SLD/18	3939	196	59	4368	769
	X- SLD/25	3977	198	59	2242	131
	Y+ SLD/41	4038	60	201	3657	336
	Y- SLD/43	3829	57	190	6569	381

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
12	SLD/1	7499	0	0	1174	1174
	SLD/2	7321	0	0	1215	1171
	SLD/3	7508	22	0	1147	1119
	SLD/4	7330	22	0	1188	1116
	SLD/5	7194	36	0	1223	1052
	SLD/6	7500	0	28	1463	1168
	SLD/7	7322	0	28	1504	1165
	SLD/8	7179	0	47	1750	1134
	SLD/9	7490	22	0	1201	1229
	SLD/10	7312	22	0	1242	1226
	SLD/11	7163	36	0	1313	1235
	SLD/12	7499	0	28	884	1179
	SLD/13	7320	0	28	925	1176
	SLD/14	7177	0	47	785	1152
	X+ SLD/15	5052	251	75	1486	66
	X- SLD/24	4819	240	72	2136	1447
	Y+ SLD/31	4974	74	247	3682	519
	Y- SLD/37	4967	74	247	2012	592
13	SLD/1	6828	0	0	44998	401
	SLD/2	6658	0	0	45619	402
	SLD/3	6832	20	0	44835	417
	SLD/4	6662	20	0	45456	418
	SLD/5	6517	33	0	46057	425
	SLD/6	6874	0	26	44440	401
	SLD/7	6704	0	26	45061	402
	SLD/8	6588	0	43	45399	399
	SLD/9	6824	20	0	45160	385
	SLD/10	6655	20	0	45781	386
	SLD/11	6505	33	0	46599	372
	SLD/12	6782	0	26	45556	401
	SLD/13	6612	0	26	46177	402
	SLD/14	6435	0	42	47258	399
	X+ SLD/15	4625	230	69	32889	496
	X- SLD/24	4536	226	68	36910	96
	Y+ SLD/31	4897	73	243	30628	355
	Y- SLD/37	4039	60	201	40945	362
14	SLD/1	13968	0	0	10177	10832
	SLD/2	13818	0	0	10564	10835
	SLD/3	14061	40	0	13188	11029
	SLD/4	13911	41	0	13575	11033
	SLD/5	13689	68	0	18128	10868
	SLD/6	14176	0	54	15731	11014
	SLD/7	14025	0	54	16118	11018

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/8	13880	0	91	22366	10843
	SLD/9	13876	40	0	7171	10634
	SLD/10	13725	41	0	7558	10638
	SLD/11	13380	67	0	8099	10210
	SLD/12	13761	0	52	4626	10650
	SLD/13	13611	0	53	5013	10653
	SLD/14	13189	0	87	3857	10236
X+	SLD/15	11385	566	170	72723	10545
X-	SLD/24	9093	452	136	2050	5622
Y+	SLD/31	11931	178	593	82802	9997
Y-	SLD/37	8176	122	406	18517	6749
15	SLD/1	15799	0	0	243454	12459
	SLD/2	15586	0	0	243504	12494
	SLD/3	15697	45	0	236916	12281
	SLD/4	15485	46	0	236967	12316
	SLD/5	15149	76	0	228260	11865
	SLD/6	15929	0	60	245054	12635
	SLD/7	15716	0	61	245104	12670
	SLD/8	15535	0	102	241822	12455
	SLD/9	15900	46	0	250011	12638
	SLD/10	15687	46	0	250062	12673
	SLD/11	15487	78	0	250085	12460
	SLD/12	15669	0	59	241861	12284
	SLD/13	15456	0	60	241912	12319
	SLD/14	15101	0	99	236501	11870
X+	SLD/18	9992	497	149	86993	6951
X-	SLD/25	12525	623	187	252790	11420
Y+	SLD/41	12563	187	625	202863	11095
Y-	SLD/43	9969	149	496	177402	7611
16	SLD/1	9055	0	0	125317	90
	SLD/2	8803	0	0	126059	85
	SLD/3	9061	26	0	126382	119
	SLD/4	8809	26	0	127124	113
	SLD/5	8641	43	0	127071	96
	SLD/6	9048	0	34	121780	87
	SLD/7	8796	0	34	122522	81
	SLD/8	8620	0	57	119401	43
	SLD/9	9049	26	0	124254	62
	SLD/10	8797	26	0	124997	56
	SLD/11	8621	43	0	123525	1
	SLD/12	9062	0	34	128861	94
	SLD/13	8810	0	34	129603	88
	SLD/14	8643	0	57	131202	55
X+	SLD/20	5984	297	89	114547	341
X-	SLD/27	5838	290	87	88214	379

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	Y+ SLD/34	5848	87	291	59439	48
	Y- SLD/36	5979	89	297	129482	113
17	SLD/1	8759	0	0	29105	353
	SLD/2	8513	0	0	29672	349
	SLD/3	8752	25	0	28734	356
	SLD/4	8506	25	0	29301	352
	SLD/5	8323	42	0	30899	347
	SLD/6	8748	0	33	31230	361
	SLD/7	8502	0	33	31797	357
	SLD/8	8317	0	55	35059	355
	SLD/9	8765	25	0	29475	350
	SLD/10	8520	25	0	30042	346
	SLD/11	8346	42	0	32133	337
	SLD/12	8769	0	33	26976	345
	SLD/13	8524	0	33	27543	341
	SLD/14	8352	0	55	27969	328
	X+ SLD/21	5614	279	84	15696	254
	X- SLD/30	5783	287	86	24795	180
	Y+ SLD/40	5589	83	278	48636	304
	Y- SLD/46	5798	86	288	6778	155
18	SLD/1	8991	0	0	33202	1206
	SLD/2	8732	0	0	33913	1201
	SLD/3	8993	26	0	34047	1152
	SLD/4	8734	26	0	34758	1147
	SLD/5	8550	43	0	37712	1055
	SLD/6	9004	0	34	35810	1204
	SLD/7	8745	0	34	36521	1199
	SLD/8	8569	0	56	40649	1142
	SLD/9	8989	26	0	32355	1261
	SLD/10	8730	26	0	33066	1256
	SLD/11	8544	43	0	34891	1237
	SLD/12	8978	0	34	30591	1209
	SLD/13	8719	0	34	31302	1204
	SLD/14	8524	0	56	31951	1150
	X+ SLD/15	5857	291	87	50494	65
	X- SLD/24	5810	289	87	29158	1442
	Y+ SLD/31	5929	88	295	60540	528
	Y- SLD/37	5676	85	282	10418	589
19	SLD/1	14180	0	0	134526	10566
	SLD/2	13948	0	0	133781	10603
	SLD/3	14179	41	0	134413	10601
	SLD/4	13947	41	0	133668	10639
	SLD/5	13667	68	0	126604	10334

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/6	14178	0	54	128317	10549
	SLD/7	13946	0	54	127573	10587
	SLD/8	13665	0	90	116444	10247
	SLD/9	14181	41	0	134634	10531
	SLD/10	13949	41	0	133889	10568
	SLD/11	13671	68	0	126971	10216
	SLD/12	14182	0	54	140736	10583
	SLD/13	13950	0	54	139991	10620
	SLD/14	13673	0	90	137142	10303
	X+ SLD/20	9484	471	141	99790	7647
	X- SLD/27	9508	473	142	102070	6751
	Y+ SLD/41	9474	141	471	26082	6876
	Y- SLD/43	9514	142	473	142382	7173
20	SLD/1	15671	0	0	412735	10642
	SLD/2	15441	0	0	414041	10701
	SLD/3	15629	45	0	404239	10548
	SLD/4	15399	45	0	405545	10607
	SLD/5	15127	76	0	395242	10325
	SLD/6	15696	0	59	423721	10689
	SLD/7	15466	0	60	425027	10748
	SLD/8	15239	0	100	427712	10561
	SLD/9	15713	45	0	421254	10737
	SLD/10	15483	46	0	422561	10796
	SLD/11	15267	76	0	423601	10640
	SLD/12	15646	0	59	401746	10595
	SLD/13	15415	0	60	403052	10654
	SLD/14	15155	0	100	391088	10404
	X+ SLD/15	10292	512	154	228658	6547
	X- SLD/24	11362	565	169	443851	8946
	Y+ SLD/40	11146	166	554	441115	8401
	Y- SLD/46	10722	160	533	236168	7606
21	SLD/1	10535	0	0	407265	182
	SLD/2	10263	0	0	408532	191
	SLD/3	10524	30	0	405453	170
	SLD/4	10253	30	0	406720	179
	SLD/5	10053	50	1	397769	192
	SLD/6	10565	1	40	408472	187
	SLD/7	10294	1	40	409739	197
	SLD/8	10121	1	67	402800	221
	SLD/9	10545	30	0	409085	193
	SLD/10	10274	30	0	410352	203
	SLD/11	10088	51	1	403822	232
	SLD/12	10504	1	40	406062	176
	SLD/13	10233	1	40	407329	186
	SLD/14	10019	1	66	398784	202

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	X+ SLD/15	6867	343	97	269725	93
	X- SLD/24	7137	357	101	315958	396
	Y+ SLD/40	7247	114	358	307334	323
	Y- SLD/46	6665	105	330	286966	238
22	SLD/1	10972	0	0	425613	695
	SLD/2	10696	0	0	427018	690
	SLD/3	10973	32	0	426631	643
	SLD/4	10696	32	0	428036	639
	SLD/5	10478	52	0	420284	557
	SLD/6	10984	0	42	427354	694
	SLD/7	10707	0	42	428759	690
	SLD/8	10496	0	69	421489	642
	SLD/9	10972	32	0	424591	746
	SLD/10	10695	32	0	425996	741
	SLD/11	10476	52	0	416884	728
	SLD/12	10961	0	42	423868	695
	SLD/13	10684	0	41	425273	690
	SLD/14	10458	0	69	415679	643
	X+ SLD/18	7206	358	107	318748	328
	X- SLD/25	7187	357	107	292858	972
	Y+ SLD/34	7276	109	362	321934	97
	Y- SLD/36	7057	105	351	287450	157
23	SLD/1	12498	0	0	264188	570
	SLD/2	12234	0	0	264801	556
	SLD/3	12497	36	0	264065	608
	SLD/4	12232	36	0	264677	594
	SLD/5	12000	60	0	257147	592
	SLD/6	12508	0	47	269298	566
	SLD/7	12244	0	47	269911	553
	SLD/8	12019	0	79	265869	523
	SLD/9	12500	36	0	264317	532
	SLD/10	12236	36	0	264930	518
	SLD/11	12006	60	0	257568	466
	SLD/12	12489	0	47	259078	573
	SLD/13	12225	0	47	259690	560
	SLD/14	11987	0	79	248836	535
	X+ SLD/15	8307	413	124	194718	758
	X- SLD/24	8353	415	125	198414	209
	Y+ SLD/40	8401	125	418	230847	116
	Y- SLD/46	8221	123	409	135689	133
24	SLD/1	21574	0	0	47404	1637
	SLD/2	21444	0	0	47074	1629
	SLD/3	21563	62	0	48238	1392

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/4	21433	63	0	47907	1384
	SLD/5	20947	105	0	45605	1071
	SLD/6	21582	0	82	69683	1652
	SLD/7	21453	0	83	69352	1644
	SLD/8	20980	0	138	81346	1504
	SLD/9	21585	62	0	46610	1883
	SLD/10	21455	63	0	46279	1875
	SLD/11	20984	105	0	42891	1888
	SLD/12	21565	0	82	25138	1622
	SLD/13	21436	0	83	24808	1614
	SLD/14	20951	0	138	7105	1454
	X+ SLD/15	14645	728	218	117389	2003
	X- SLD/24	14925	742	223	101093	4230
	Y+ SLD/40	14882	222	740	251871	2088
	Y- SLD/46	14733	220	732	152815	2119
25	SLD/1	17603	0	0	3412	13263
	SLD/2	17402	0	0	3639	13356
	SLD/3	17749	51	0	2647	13502
	SLD/4	17548	52	0	2874	13595
	SLD/5	17383	87	0	2976	13491
	SLD/6	17603	0	67	29274	13260
	SLD/7	17402	0	67	29047	13353
	SLD/8	17139	0	113	50225	13087
	SLD/9	17456	50	0	4128	13024
	SLD/10	17255	51	0	4356	13117
	SLD/11	16895	85	0	5446	12694
	SLD/12	17602	0	67	36088	13266
	SLD/13	17402	0	68	36315	13359
	SLD/14	17139	0	113	58711	13098
	X+ SLD/18	14238	708	212	66407	12824
26	X- SLD/25	10513	523	157	52825	6747
	Y+ SLD/34	13030	194	648	267299	10830
	Y- SLD/36	12841	192	638	332114	10587
26	SLD/1	14506	0	0	1288	14078
	SLD/2	14332	0	0	1534	14073
	SLD/3	14514	0	42	1563	14098
	SLD/4	14340	0	42	1809	14093
	SLD/5	13966	0	70	3174	13617
	SLD/6	14420	55	0	680	13823
	SLD/7	14246	55	0	926	13818
	SLD/8	13810	91	0	1703	13160
	SLD/9	14497	0	42	1015	14058
	SLD/10	14323	0	42	1261	14053
	SLD/11	13938	0	70	2261	13550
	SLD/12	14591	55	0	1899	14332

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/13	14417	56	0	2145	14327
	SLD/14	14095	93	0	3733	14008
	X+ SLD/21	9961	149	495	11282	10358
	X- SLD/30	9759	146	485	4691	9870
	Y+ SLD/31	8807	438	131	623	6972
	Y- SLD/37	10483	521	156	13858	11943
27	SLD/1	14554	0	0	98222	13993
	SLD/2	14337	0	0	98105	14004
	SLD/3	14608	0	42	101881	14044
	SLD/4	14391	0	42	101764	14056
	SLD/5	14073	0	70	99561	13578
	SLD/6	14385	54	0	104695	13590
	SLD/7	14168	55	0	104578	13602
	SLD/8	13701	90	0	104251	12821
	SLD/9	14500	0	42	94575	13941
	SLD/10	14283	0	42	94458	13953
	SLD/11	13892	0	70	87384	13407
	SLD/12	14723	56	0	91758	14396
	SLD/13	14506	56	0	91641	14408
	SLD/14	14264	94	0	82689	14165
	X+ SLD/21	10829	162	538	99180	10981
	X- SLD/30	9478	141	471	9193	9694
	Y+ SLD/31	8226	409	123	143189	5520
	Y- SLD/37	11517	573	172	29504	13227
28	SLD/1	18233	0	0	375977	16270
	SLD/2	17999	0	0	376584	16312
	SLD/3	18256	0	53	377675	16297
	SLD/4	18022	0	53	378282	16338
	SLD/5	17682	0	88	373873	15875
	SLD/6	17857	68	0	359051	15574
	SLD/7	17624	68	0	359658	15615
	SLD/8	17018	112	0	342832	14671
	SLD/9	18210	0	52	374242	16243
	SLD/10	17976	0	53	374849	16284
	SLD/11	17606	0	88	368151	15786
	SLD/12	18609	71	0	392890	16967
	SLD/13	18375	71	0	393497	17008
	SLD/14	18271	120	0	399231	16991
	X+ SLD/20	13880	207	690	355152	13722
	X- SLD/27	13263	198	659	308505	12973
	Y+ SLD/34	9151	455	136	142656	5115
	Y- SLD/36	16143	803	241	448787	18049
29	SLD/1	12886	0	0	215995	8494

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/2	12707	0	0	216829	8548
	SLD/3	12810	0	37	211243	8371
	SLD/4	12630	0	37	212077	8425
	SLD/5	12417	0	62	205917	8219
	SLD/6	12757	48	0	205030	8247
	SLD/7	12578	49	0	205864	8301
	SLD/8	12330	81	0	195562	8012
	SLD/9	12963	0	37	220768	8618
	SLD/10	12783	0	38	221602	8672
	SLD/11	12671	0	63	221792	8631
	SLD/12	13015	49	0	226983	8742
	SLD/13	12835	50	0	227817	8796
	SLD/14	12759	84	0	232151	8837
	X+ SLD/21	8359	125	416	134875	5367
	X- SLD/30	10288	153	511	256134	8490
	Y+ SLD/40	7999	398	119	73647	4291
	Y- SLD/46	10488	521	156	290842	9083
30	SLD/1	9181	0	0	239067	539
	SLD/2	8957	0	0	240297	547
	SLD/3	9161	0	26	236940	535
	SLD/4	8937	0	26	238170	543
	SLD/5	8751	0	44	233870	552
	SLD/6	9177	35	0	236251	489
	SLD/7	8953	35	0	237482	496
	SLD/8	8777	58	0	232722	474
	SLD/9	9200	0	27	241198	544
	SLD/10	8976	0	26	242428	551
	SLD/11	8816	0	44	240967	566
	SLD/12	9184	35	0	241886	590
	SLD/13	8960	35	0	243116	598
	SLD/14	8789	58	0	242114	643
	X+ SLD/20	5801	87	288	154992	497
	X- SLD/27	6292	94	313	208645	616
	Y+ SLD/41	6081	302	91	154533	94
	Y- SLD/43	6143	305	92	208807	923
31	SLD/1	6945	0	0	20027	922
	SLD/2	6752	0	0	20239	919
	SLD/3	6946	0	20	18711	909
	SLD/4	6753	0	20	18924	906
	SLD/5	6611	0	33	18905	855
	SLD/6	6955	26	0	19441	927
	SLD/7	6762	26	0	19654	924
	SLD/8	6626	44	0	20122	885
	SLD/9	6944	0	20	21343	936
	SLD/10	6751	0	20	21555	933

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/11	6608	0	33	23291	900
	SLD/12	6936	26	0	20611	918
	SLD/13	6743	26	0	20824	915
	SLD/14	6594	43	0	22072	870
	X+ SLD/18	4534	68	225	549	436
	X- SLD/25	4509	67	224	33480	777
	Y+ SLD/34	4590	228	68	8648	593
	Y- SLD/36	4405	219	66	18878	493
32	SLD/1	7423	0	0	5709	1719
	SLD/2	7242	0	0	5623	1717
	SLD/3	7417	0	21	5270	1717
	SLD/4	7237	0	21	5185	1714
	SLD/5	7096	0	35	4609	1666
	SLD/6	7414	28	0	5331	1741
	SLD/7	7233	28	0	5245	1739
	SLD/8	7090	47	0	4710	1706
	SLD/9	7428	0	21	6147	1721
	SLD/10	7247	0	21	6062	1719
	SLD/11	7113	0	36	6070	1673
	SLD/12	7432	28	0	6086	1697
	SLD/13	7251	28	0	6001	1695
	SLD/14	7119	47	0	5969	1633
	X+ SLD/20	4843	72	241	694	1075
	X- SLD/27	4976	74	247	10257	1128
	Y+ SLD/41	4824	240	72	2065	1387
	Y- SLD/43	4987	248	74	8875	962
33	SLD/1	8105	0	0	24321	1676
	SLD/2	7873	0	0	24753	1676
	SLD/3	8127	0	23	25935	1681
	SLD/4	7894	0	23	26368	1681
	SLD/5	7744	0	39	29162	1632
	SLD/6	8109	31	0	22704	1745
	SLD/7	7877	31	0	23137	1745
	SLD/8	7714	51	0	23776	1739
	SLD/9	8083	0	23	22706	1671
	SLD/10	7851	0	23	23139	1671
	SLD/11	7671	0	38	23779	1615
	SLD/12	8101	31	0	25941	1607
	SLD/13	7868	31	0	26374	1607
	SLD/14	7700	51	0	29171	1508
	X+ SLD/15	5532	83	275	39945	1398
	X- SLD/24	4986	74	248	494	1277
	Y+ SLD/31	5365	267	80	14749	1816
	Y- SLD/37	5307	264	79	46775	512

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
34	SLD/1	10212	0	0	347909	1982
	SLD/2	9955	0	0	349821	1983
	SLD/3	10224	0	29	348709	1996
	SLD/4	9966	0	29	350621	1997
	SLD/5	9777	0	49	346655	1943
	SLD/6	10240	39	0	349348	2101
	SLD/7	9983	39	0	351260	2101
	SLD/8	9805	64	0	347720	2118
	SLD/9	10201	0	29	347111	1968
	SLD/10	9944	0	29	349023	1969
	SLD/11	9740	0	49	343992	1897
	SLD/12	10185	39	0	346471	1864
	SLD/13	9927	39	0	348384	1864
	SLD/14	9712	64	0	342925	1723
	X+ SLD/15	6923	103	344	268456	1897
	X- SLD/24	6645	99	330	248773	1567
	Y+ SLD/31	7007	348	105	270783	2559
	Y- SLD/37	6499	323	97	245448	374
35	SLD/1	8710	0	0	203169	727
	SLD/2	8488	0	0	204345	727
	SLD/3	8692	0	25	202618	725
	SLD/4	8470	0	25	203794	725
	SLD/5	8304	0	42	201702	679
	SLD/6	8739	33	0	205334	685
	SLD/7	8517	33	0	206510	684
	SLD/8	8383	55	0	206228	611
	SLD/9	8728	0	25	203715	729
	SLD/10	8506	0	25	204891	729
	SLD/11	8365	0	42	203529	686
	SLD/12	8681	33	0	200996	770
	SLD/13	8459	33	0	202172	769
	SLD/14	8286	55	0	198998	753
	X+ SLD/18	5638	84	280	153074	227
	X- SLD/25	6089	91	303	166281	290
	Y+ SLD/41	6145	305	92	177750	39
	Y- SLD/43	5550	276	83	133167	818
36	SLD/1	7153	0	0	25970	770
	SLD/2	6959	0	0	26272	769
	SLD/3	7148	0	21	25033	767
	SLD/4	6953	0	20	25335	766
	SLD/5	6796	0	34	25572	738
	SLD/6	7159	27	0	25530	750
	SLD/7	6965	27	0	25832	749

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/8	6815	45	0	26400	710
	SLD/9	7158	0	21	26910	773
	SLD/10	6964	0	21	27212	772
	SLD/11	6814	0	34	28700	749
	SLD/12	7147	27	0	26412	790
	SLD/13	6953	27	0	26713	789
	SLD/14	6795	45	0	27869	777
	X+ SLD/18	4572	68	227	9007	398
	X- SLD/25	4709	70	234	32653	478
	Y+ SLD/41	4704	234	70	21359	310
	Y- SLD/43	4583	228	68	29924	705
37	SLD/1	7571	0	0	4155	1212
	SLD/2	7391	0	0	4050	1212
	SLD/3	7566	0	22	3747	1213
	SLD/4	7386	0	22	3642	1213
	SLD/5	7241	0	36	3066	1191
	SLD/6	7578	29	0	4643	1184
	SLD/7	7399	29	0	4538	1184
	SLD/8	7262	48	0	4559	1142
	SLD/9	7576	0	22	4564	1211
	SLD/10	7396	0	22	4459	1211
	SLD/11	7258	0	36	4428	1187
	SLD/12	7564	29	0	3667	1240
	SLD/13	7384	29	0	3562	1240
	SLD/14	7237	48	0	2933	1236
	X+ SLD/18	4942	74	246	1530	774
	X- SLD/25	5069	76	252	8738	751
	Y+ SLD/41	5074	252	76	8456	570
	Y- SLD/43	4933	245	74	966	1109
38	SLD/1	8793	0	0	53751	118
	SLD/2	8572	0	0	54398	112
	SLD/3	8805	0	25	51556	125
	SLD/4	8583	0	25	52203	119
	SLD/5	8443	0	42	50371	97
	SLD/6	8823	33	0	54879	107
	SLD/7	8601	33	0	55525	101
	SLD/8	8472	56	0	55909	67
	SLD/9	8782	0	25	55950	111
	SLD/10	8560	0	25	56597	105
	SLD/11	8404	0	42	57694	75
	SLD/12	8764	33	0	52623	129
	SLD/13	8543	33	0	53269	124
	SLD/14	8375	55	0	52149	105
	X+ SLD/15	6049	90	301	16381	70
	X- SLD/24	5755	86	286	71718	100

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	Y+ SLD/31	6140	305	92	43268	67
	Y- SLD/37	5590	278	83	21875	157
39	SLD/1	14348	0	0	270032	8797
	SLD/2	14141	0	0	271004	8854
	SLD/3	14397	0	41	274823	8863
	SLD/4	14190	0	42	275795	8921
	SLD/5	13995	0	70	276557	8807
	SLD/6	14518	55	0	284458	9016
	SLD/7	14311	55	0	285430	9073
	SLD/8	14197	93	0	292615	9061
	SLD/9	14299	0	41	265262	8731
	SLD/10	14092	0	42	266233	8788
	SLD/11	13833	0	69	260621	8587
	SLD/12	14179	54	0	255617	8579
	SLD/13	13971	54	0	256588	8636
	SLD/14	13631	90	0	244546	8333
	X+ SLD/15	11005	164	547	310774	7898
	X- SLD/24	9803	146	487	193318	6270
	Y+ SLD/31	11693	581	174	363435	8754
	Y- SLD/37	8591	427	128	102256	4767
40	SLD/1	13423	0	0	273815	9143
	SLD/2	13227	0	0	274299	9173
	SLD/3	13378	0	39	268612	9079
	SLD/4	13183	0	39	269096	9109
	SLD/5	12925	0	65	261367	8832
	SLD/6	13475	51	0	282104	9252
	SLD/7	13279	51	0	282588	9282
	SLD/8	13086	86	0	283854	9120
	SLD/9	13467	0	39	279016	9207
	SLD/10	13271	0	39	279499	9236
	SLD/11	13073	0	65	278707	9045
	SLD/12	13370	51	0	265508	9034
	SLD/13	13175	51	0	265992	9063
	SLD/14	12912	85	0	256194	8756
	X+ SLD/18	8756	131	435	160584	5915
	X- SLD/25	9865	147	490	290400	7503
	Y+ SLD/41	9847	490	147	303490	7722
	Y- SLD/43	8808	438	131	138898	5547
41	SLD/1	7331	0	0	66169	313
	SLD/2	7139	0	0	66644	321
	SLD/3	7345	0	21	67251	315
	SLD/4	7153	0	21	67726	323
	SLD/5	7010	0	35	68189	334

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/6	7319	28	0	65114	348
	SLD/7	7127	28	0	65589	356
	SLD/8	6968	46	0	64627	390
	SLD/9	7318	0	21	65085	311
	SLD/10	7126	0	21	65560	320
	SLD/11	6966	0	35	64579	329
	SLD/12	7343	28	0	67225	278
	SLD/13	7151	28	0	67700	286
	SLD/14	7008	46	0	68145	273
	X+ SLD/21	4961	74	247	66327	176
	X- SLD/30	4623	69	230	39066	132
	Y+ SLD/31	4695	233	70	43664	607
	Y- SLD/37	4923	245	73	63847	84
42	SLD/1	6774	0	0	11355	676
	SLD/2	6575	0	0	11145	672
	SLD/3	6758	0	19	10533	676
	SLD/4	6559	0	19	10323	673
	SLD/5	6377	0	32	8919	647
	SLD/6	6777	26	0	11139	635
	SLD/7	6578	26	0	10928	632
	SLD/8	6408	42	0	9929	579
	SLD/9	6790	0	20	12180	675
	SLD/10	6591	0	19	11969	672
	SLD/11	6430	0	32	11664	646
	SLD/12	6771	26	0	11573	716
	SLD/13	6572	26	0	11362	713
	SLD/14	6398	42	0	10652	714
	X+ SLD/15	4089	61	203	4699	330
	X- SLD/24	4489	67	223	16155	327
	Y+ SLD/40	4368	217	65	7272	55
	Y- SLD/46	4319	215	64	12105	842
43	SLD/1	8497	0	0	135585	1580
	SLD/2	8268	0	0	136388	1579
	SLD/3	8496	0	24	133771	1580
	SLD/4	8267	0	24	134573	1579
	SLD/5	8101	0	41	131937	1530
	SLD/6	8489	32	0	134577	1553
	SLD/7	8259	32	0	135379	1551
	SLD/8	8088	53	0	133280	1485
	SLD/9	8497	0	24	137404	1580
	SLD/10	8268	0	24	138207	1579
	SLD/11	8103	0	41	137993	1531
	SLD/12	8505	32	0	136596	1608
	SLD/13	8276	32	0	137399	1606
	SLD/14	8116	53	0	136646	1576

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	X+ SLD/20	5548	83	276	78660	1136
	X- SLD/27	5559	83	276	124562	1140
	Y+ SLD/41	5454	271	81	95217	803
	Y- SLD/43	5610	279	84	115430	1321
44	SLD/1	22132	0	0	507433	11595
	SLD/2	21930	0	0	509705	11516
	SLD/3	22105	0	64	502138	11583
	SLD/4	21902	0	65	504410	11504
	SLD/5	21290	0	106	485604	11067
	SLD/6	21990	83	0	497251	11285
	SLD/7	21787	84	0	499523	11206
	SLD/8	21099	139	0	477459	10570
	SLD/9	22160	0	64	512724	11606
	SLD/10	21957	0	65	514996	11527
	SLD/11	21382	0	107	503248	11106
	SLD/12	22275	84	0	517615	11905
	SLD/13	22072	86	0	519887	11826
	SLD/14	21573	142	0	511399	11603
	X+ SLD/20	14838	221	738	314112	8378
	X- SLD/27	15514	231	771	446100	8620
	Y+ SLD/41	13591	676	203	278415	4884
	Y- SLD/43	16211	806	242	466890	10563
45	SLD/1	15918	0	0	78547	10640
	SLD/2	15798	0	0	78734	10575
	SLD/3	15988	0	46	75525	10691
	SLD/4	15868	0	47	75713	10626
	SLD/5	15553	0	78	68691	10295
	SLD/6	15662	59	0	82018	10180
	SLD/7	15543	60	0	82205	10115
	SLD/8	15011	99	0	79512	9444
	SLD/9	15848	0	46	81586	10589
	SLD/10	15728	0	46	81773	10524
	SLD/11	15319	0	77	78792	10125
	SLD/12	16173	61	0	75084	11100
	SLD/13	16054	62	0	75271	11035
	SLD/14	15862	104	0	67955	10977
	X+ SLD/20	12709	190	632	8540	9349
	X- SLD/27	10881	162	541	69111	7960
	Y+ SLD/34	9154	455	137	56052	3568
	Y- SLD/36	13718	682	205	3237	11843
46	SLD/1	15507	0	0	50116	13168
	SLD/2	15345	0	0	50625	13158
	SLD/3	15428	0	44	47957	13072

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/4	15265	0	45	48466	13062
	SLD/5	14903	0	75	49568	12598
	SLD/6	15672	59	0	56228	13561
	SLD/7	15509	60	0	56737	13551
	SLD/8	15309	101	0	63352	13414
	SLD/9	15587	0	45	52274	13265
	SLD/10	15424	0	46	52783	13255
	SLD/11	15168	0	76	56763	12919
	SLD/12	15342	58	0	43994	12775
	SLD/13	15180	59	0	44503	12765
	SLD/14	14760	97	0	42963	12103
X+	SLD/15	10020	149	498	34386	8650
X-	SLD/24	12026	179	598	88328	11057
Y+	SLD/40	12423	618	185	110808	12870
Y-	SLD/46	9293	462	139	8277	5234
47	SLD/1	15879	0	0	16359	16971
	SLD/2	15698	0	0	16193	16967
	SLD/3	15861	0	46	16302	16951
	SLD/4	15680	0	46	16136	16947
	SLD/5	15251	0	76	15126	16363
	SLD/6	15953	60	0	16323	17195
	SLD/7	15772	61	0	16156	17191
	SLD/8	15403	101	0	15159	16770
	SLD/9	15896	0	46	16417	16991
	SLD/10	15715	0	46	16251	16987
	SLD/11	15309	0	77	15317	16430
	SLD/12	15804	60	0	16397	16747
	SLD/13	15624	61	0	16231	16742
	SLD/14	15157	100	0	15283	16023
X+	SLD/15	10492	156	522	9479	11604
X-	SLD/24	10936	163	544	11164	12106
Y+	SLD/40	11273	560	168	10092	13435
Y-	SLD/46	9874	491	147	12022	9131
48	SLD/1	19317	0	0	50115	21969
	SLD/2	19107	0	0	50069	21950
	SLD/3	19332	0	56	46324	21979
	SLD/4	19121	0	56	46277	21960
	SLD/5	18652	0	93	41250	21167
	SLD/6	19449	74	0	52814	22329
	SLD/7	19238	75	0	52768	22310
	SLD/8	18847	124	0	52068	21750
	SLD/9	19303	0	56	53930	21959
	SLD/10	19093	0	56	53884	21940
	SLD/11	18605	0	93	53927	21134
	SLD/12	19186	73	0	47428	21609

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI TRAVI WINKLER - SLD						
Trave N.ro	Combinazione N.ro	Rv (kg)	Vx (kg)	Vy (kg)	Mrx kg*cm	Mry kg*cm
	SLD/13	18976	74	0	47382	21590
	SLD/14	18410	121	0	43091	20550
	X+ SLD/15	13419	200	667	2213	15552
	X- SLD/24	13062	195	649	95368	15319
	Y+ SLD/31	14172	705	211	48160	17867
	Y- SLD/37	11668	580	174	6153	11056
49	SLD/1	25965	0	0	218433	21613
	SLD/2	25759	0	0	220347	21514
	SLD/3	25952	0	75	213923	21618
	SLD/4	25745	0	76	215837	21518
	SLD/5	24991	0	125	206584	20678
	SLD/6	26192	99	0	223131	22108
	SLD/7	25985	101	0	225046	22008
	SLD/8	25392	167	0	221932	21495
	SLD/9	25980	0	75	222980	21610
	SLD/10	25773	0	76	224895	21510
	SLD/11	25038	0	125	221680	20664
	SLD/12	25739	98	0	213757	21119
	SLD/13	25533	99	0	215671	21019
	SLD/14	24637	162	0	206307	19846
	X+ SLD/15	17767	265	883	120382	15503
	X- SLD/24	18159	271	903	237591	15470
	Y+ SLD/40	19502	970	291	224808	18728
	Y- SLD/46	15360	764	229	151641	9608
50	SLD/1	16139	0	0	90985	11085
	SLD/2	16015	0	0	91162	11013
	SLD/3	16224	0	47	87836	11164
	SLD/4	16099	0	47	88013	11091
	SLD/5	15769	0	79	80407	10739
	SLD/6	16400	62	0	87775	11552
	SLD/7	16275	63	0	87952	11480
	SLD/8	16063	106	0	80304	11386
	SLD/9	16055	0	46	94140	11008
	SLD/10	15931	0	47	94317	10935
	SLD/11	15489	0	78	90913	10479
	SLD/12	15879	60	0	94200	10619
	SLD/13	15754	61	0	94377	10547
	SLD/14	15195	100	0	91012	9831
	X+ SLD/15	12787	191	636	5886	9697
	X- SLD/24	10693	159	532	85394	7808
	Y+ SLD/31	13774	685	205	12025	12092
	Y- SLD/37	8920	443	133	74398	3528

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU

RELAZIONE GEOTECNICA

Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
1	A1/1	-1,61	3	A1/1	-3,08	4	A1/1	-3,56	5	A1/1	-3,26
	A1/2	-1,59		A1/2	-3,02		A1/2	-3,48		A1/2	-3,18
	A1/3	-1,60		A1/3	-3,08		A1/3	-3,56		A1/3	-3,25
	A1/4	-1,58		A1/4	-3,02		A1/4	-3,47		A1/4	-3,17
	A1/5	-1,54		A1/5	-2,97		A1/5	-3,40		A1/5	-3,11
	A1/6	-1,58		A1/6	-3,07		A1/6	-3,56		A1/6	-3,26
	A1/7	-1,56		A1/7	-3,02		A1/7	-3,47		A1/7	-3,18
	A1/8	-1,51		A1/8	-2,96		A1/8	-3,41		A1/8	-3,11
	A1/9	-1,62		A1/9	-3,08		A1/9	-3,57		A1/9	-3,26
	A1/10	-1,61		A1/10	-3,03		A1/10	-3,48		A1/10	-3,18
	A1/11	-1,58		A1/11	-2,98		A1/11	-3,41		A1/11	-3,12
	A1/12	-1,64		A1/12	-3,09		A1/12	-3,57		A1/12	-3,26
	A1/13	-1,62		A1/13	-3,03		A1/13	-3,48		A1/13	-3,18
	A1/14	-1,61		A1/14	-2,99		A1/14	-3,41		A1/14	-3,11
X+	A1/20	-1,03	X+	A1/20	-2,08	X+	A1/20	-2,31	X+	A1/18	-2,10
X-	A1/27	-1,30	X-	A1/27	-2,15	X-	A1/27	-2,37	X-	A1/25	-2,17
Y+	A1/41	-0,90	Y+	A1/41	-2,05	Y+	A1/41	-2,34	Y+	A1/41	-2,15
Y-	A1/43	-1,37	Y-	A1/43	-2,17	Y-	A1/43	-2,35	Y-	A1/43	-2,14
7	A1/1	-3,34	8	A1/1	-2,69	9	A1/1	-3,35	10	A1/1	-2,21
	A1/2	-3,26		A1/2	-2,64		A1/2	-3,25		A1/2	-2,19
	A1/3	-3,34		A1/3	-2,69		A1/3	-3,35		A1/3	-2,22
	A1/4	-3,26		A1/4	-2,65		A1/4	-3,25		A1/4	-2,20
	A1/5	-3,20		A1/5	-2,59		A1/5	-3,17		A1/5	-2,16
	A1/6	-3,33		A1/6	-2,64		A1/6	-3,36		A1/6	-2,15
	A1/7	-3,25		A1/7	-2,60		A1/7	-3,26		A1/7	-2,13
	A1/8	-3,18		A1/8	-2,51		A1/8	-3,18		A1/8	-2,04
	A1/9	-3,34		A1/9	-2,68		A1/9	-3,35		A1/9	-2,20
	A1/10	-3,25		A1/10	-2,64		A1/10	-3,25		A1/10	-2,18
	A1/11	-3,18		A1/11	-2,58		A1/11	-3,16		A1/11	-2,13
	A1/12	-3,35		A1/12	-2,73		A1/12	-3,34		A1/12	-2,27
	A1/13	-3,26		A1/13	-2,69		A1/13	-3,24		A1/13	-2,25
	A1/14	-3,20		A1/14	-2,66		A1/14	-3,15		A1/14	-2,24
X+	A1/21	-2,24	X+	A1/20	-1,92	X+	A1/15	-2,17	X+	A1/20	-1,75
X-	A1/30	-2,16	X-	A1/27	-1,86	X-	A1/24	-2,10	X-	A1/27	-1,56
Y+	A1/31	-2,15	Y+	A1/34	-1,46	Y+	A1/31	-2,19	Y+	A1/34	-1,12
Y-	A1/37	-2,24	Y-	A1/36	-2,14	Y-	A1/37	-2,06	Y-	A1/36	-2,00
12	A1/1	-1,69	14	A1/1	-2,94	15	A1/1	-2,62	16	A1/1	-3,17
	A1/2	-1,67		A1/2	-2,85		A1/2	-2,59		A1/2	-3,07
	A1/3	-1,66		A1/3	-2,94		A1/3	-2,61		A1/3	-3,17
	A1/4	-1,65		A1/4	-2,86		A1/4	-2,58		A1/4	-3,07
	A1/5	-1,61		A1/5	-2,79		A1/5	-2,52		A1/5	-2,99
	A1/6	-1,65		A1/6	-2,95		A1/6	-2,64		A1/6	-3,17
	A1/7	-1,64		A1/7	-2,86		A1/7	-2,60		A1/7	-3,08
	A1/8	-1,59		A1/8	-2,80		A1/8	-2,56		A1/8	-3,01
	A1/9	-1,71		A1/9	-2,94		A1/9	-2,63		A1/9	-3,17
	A1/10	-1,69		A1/10	-2,85		A1/10	-2,60		A1/10	-3,08
	A1/11	-1,68		A1/11	-2,78		A1/11	-2,55		A1/11	-3,00
	A1/12	-1,72		A1/12	-2,93		A1/12	-2,61		A1/12	-3,16
	A1/13	-1,70		A1/13	-2,85		A1/13	-2,57		A1/13	-3,07
	A1/14	-1,70		A1/14	-2,77		A1/14	-2,51		A1/14	-2,99
X+	A1/21	-1,03	X+	A1/15	-1,91	X+	A1/18	-1,71	X+	A1/18	-2,01
X-	A1/30	-1,48	X-	A1/24	-1,86	X-	A1/25	-1,93	X-	A1/25	-2,05
Y+	A1/40	-0,99	Y+	A1/31	-1,93	Y+	A1/41	-1,94	Y+	A1/41	-2,07
Y-	A1/46	-1,50	Y-	A1/37	-1,82	Y-	A1/43	-1,69	Y-	A1/43	-1,98
17	A1/1	-2,60	18	A1/1	-2,64	19	A1/1	-1,52	20	A1/1	-2,11
	A1/2	-2,54		A1/2	-2,59		A1/2	-1,51		A1/2	-2,09
	A1/3	-2,60		A1/3	-2,64		A1/3	-1,54		A1/3	-2,09
	A1/4	-2,54		A1/4	-2,59		A1/4	-1,52		A1/4	-2,06
	A1/5	-2,49		A1/5	-2,54		A1/5	-1,51		A1/5	-2,01
	A1/6	-2,60		A1/6	-2,65		A1/6	-1,56		A1/6	-2,13
	A1/7	-2,54		A1/7	-2,60		A1/7	-1,54		A1/7	-2,11
	A1/8	-2,49		A1/8	-2,56		A1/8	-1,54		A1/8	-2,08
	A1/9	-2,60		A1/9	-2,64		A1/9	-1,51		A1/9	-2,13
	A1/10	-2,53		A1/10	-2,59		A1/10	-1,49		A1/10	-2,11
	A1/11	-2,48		A1/11	-2,54		A1/11	-1,45		A1/11	-2,08
	A1/12	-2,59		A1/12	-2,63		A1/12	-1,49		A1/12	-2,08
	A1/13	-2,53		A1/13	-2,57		A1/13	-1,47		A1/13	-2,06
	A1/14	-2,48		A1/14	-2,52		A1/14	-1,42		A1/14	-2,01
X+	A1/15	-1,74	X+	A1/15	-1,80	X+	A1/15	-1,32	X+	A1/18	-1,27
X-	A1/24	-1,68	X-	A1/24	-1,78	X-	A1/24	-0,99	X-	A1/25	-1,72
Y+	A1/31	-1,75	Y+	A1/31	-1,86	Y+	A1/31	-1,38	Y+	A1/41	-1,69
Y-	A1/37	-1,67	Y-	A1/37	-1,67	Y-	A1/37	-0,88	Y-	A1/43	-1,33
21	A1/1	-3,30	22	A1/1	-3,41	23	A1/1	-4,47	24	A1/1	-3,64
	A1/2	-3,23		A1/2	-3,31		A1/2	-4,34		A1/2	-3,58
	A1/3	-3,30		A1/3	-3,41		A1/3	-4,47		A1/3	-3,64
	A1/4	-3,23		A1/4	-3,31		A1/4	-4,34		A1/4	-3,58
	A1/5	-3,17		A1/5	-3,22		A1/5	-4,22		A1/5	-3,50
	A1/6	-3,29		A1/6	-3,41		A1/6	-4,47		A1/6	-3,63
	A1/7	-3,22		A1/7	-3,31		A1/7	-4,34		A1/7	-3,57

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/8	-3,15		A1/8	-3,22		A1/8	-4,23		A1/8	-3,48
	A1/9	-3,29		A1/9	-3,41		A1/9	-4,48		A1/9	-3,64
	A1/10	-3,23		A1/10	-3,31		A1/10	-4,35		A1/10	-3,58
	A1/11	-3,16		A1/11	-3,23		A1/11	-4,23		A1/11	-3,49
	A1/12	-3,30		A1/12	-3,41		A1/12	-4,47		A1/12	-3,65
	A1/13	-3,24		A1/13	-3,31		A1/13	-4,34		A1/13	-3,59
	A1/14	-3,18		A1/14	-3,22		A1/14	-4,23		A1/14	-3,51
X+	A1/21	-2,25	X+	A1/15	-2,15	X+	A1/21	-2,79	X+	A1/20	-2,43
X-	A1/30	-2,17	X-	A1/24	-2,17	X-	A1/30	-2,85	X-	A1/27	-2,41
Y+	A1/31	-2,13	Y+	A1/40	-2,17	Y+	A1/40	-2,82	Y+	A1/34	-2,34
Y-	A1/37	-2,27	Y-	A1/46	-2,16	Y-	A1/46	-2,83	Y-	A1/36	-2,47
25	A1/1	-1,81	31	A1/1	-1,61	32	A1/1	-1,61	65	A1/1	-2,95
	A1/2	-1,80		A1/2	-1,60		A1/2	-1,59		A1/2	-2,91
	A1/3	-1,80		A1/3	-1,63		A1/3	-1,62		A1/3	-2,94
	A1/4	-1,78		A1/4	-1,62		A1/4	-1,61		A1/4	-2,90
	A1/5	-1,74		A1/5	-1,60		A1/5	-1,59		A1/5	-2,84
	A1/6	-1,84		A1/6	-1,58		A1/6	-1,64		A1/6	-2,90
	A1/7	-1,83		A1/7	-1,56		A1/7	-1,63		A1/7	-2,86
	A1/8	-1,81		A1/8	-1,51		A1/8	-1,62		A1/8	-2,78
	A1/9	-1,83		A1/9	-1,60		A1/9	-1,59		A1/9	-2,96
	A1/10	-1,81		A1/10	-1,58		A1/10	-1,58		A1/10	-2,92
	A1/11	-1,79		A1/11	-1,54		A1/11	-1,53		A1/11	-2,87
	A1/12	-1,78		A1/12	-1,65		A1/12	-1,57		A1/12	-2,99
	A1/13	-1,77		A1/13	-1,64		A1/13	-1,56		A1/13	-2,96
	A1/14	-1,72		A1/14	-1,63		A1/14	-1,50		A1/14	-2,93
X+	A1/15	-1,17	X+	A1/20	-1,40	X+	A1/15	-1,37	X+	A1/21	-2,01
X-	A1/24	-1,46	X-	A1/27	-1,06	X-	A1/24	-1,01	X-	A1/30	-2,23
Y+	A1/40	-1,51	Y+	A1/34	-0,95	Y+	A1/31	-1,44	Y+	A1/40	-1,69
Y-	A1/46	-1,07	Y-	A1/36	-1,47	Y-	A1/37	-0,89	Y-	A1/46	-2,41
66	A1/1	-2,57	67	A1/1	-2,39	68	A1/1	-1,54	69	A1/1	-1,42
	A1/2	-2,53		A1/2	-2,33		A1/2	-1,51		A1/2	-1,39
	A1/3	-2,56		A1/3	-2,39		A1/3	-1,54		A1/3	-1,42
	A1/4	-2,52		A1/4	-2,33		A1/4	-1,50		A1/4	-1,38
	A1/5	-2,47		A1/5	-2,28		A1/5	-1,48		A1/5	-1,36
	A1/6	-2,54		A1/6	-2,39		A1/6	-1,54		A1/6	-1,42
	A1/7	-2,50		A1/7	-2,34		A1/7	-1,51		A1/7	-1,38
	A1/8	-2,44		A1/8	-2,29		A1/8	-1,48		A1/8	-1,36
	A1/9	-2,58		A1/9	-2,39		A1/9	-1,54		A1/9	-1,42
	A1/10	-2,54		A1/10	-2,34		A1/10	-1,51		A1/10	-1,39
	A1/11	-2,51		A1/11	-2,29		A1/11	-1,48		A1/11	-1,36
	A1/12	-2,60		A1/12	-2,39		A1/12	-1,54		A1/12	-1,42
	A1/13	-2,56		A1/13	-2,33		A1/13	-1,51		A1/13	-1,39
	A1/14	-2,53		A1/14	-2,29		A1/14	-1,48		A1/14	-1,36
X+	A1/20	-1,69	X+	A1/18	-1,55	X+	A1/20	-1,00	X+	A1/20	-0,92
X-	A1/27	-1,93	X-	A1/25	-1,61	X-	A1/27	-1,04	X-	A1/27	-0,96
Y+	A1/41	-1,58	Y+	A1/41	-1,60	Y+	A1/41	-1,02	Y+	A1/41	-0,93
Y-	A1/43	-2,00	Y-	A1/43	-1,57	Y-	A1/43	-1,03	Y-	A1/43	-0,95
70	A1/1	-2,12	71	A1/1	-1,62	72	A1/1	-1,32	73	A1/1	-1,39
	A1/2	-2,08		A1/2	-1,57		A1/2	-1,27		A1/2	-1,35
	A1/3	-2,12		A1/3	-1,62		A1/3	-1,32		A1/3	-1,39
	A1/4	-2,08		A1/4	-1,57		A1/4	-1,27		A1/4	-1,35
	A1/5	-2,04		A1/5	-1,55		A1/5	-1,26		A1/5	-1,33
	A1/6	-2,12		A1/6	-1,62		A1/6	-1,32		A1/6	-1,39
	A1/7	-2,08		A1/7	-1,58		A1/7	-1,28		A1/7	-1,35
	A1/8	-2,04		A1/8	-1,56		A1/8	-1,26		A1/8	-1,33
	A1/9	-2,12		A1/9	-1,62		A1/9	-1,32		A1/9	-1,39
	A1/10	-2,08		A1/10	-1,57		A1/10	-1,27		A1/10	-1,35
	A1/11	-2,04		A1/11	-1,55		A1/11	-1,26		A1/11	-1,33
	A1/12	-2,13		A1/12	-1,62		A1/12	-1,32		A1/12	-1,39
	A1/13	-2,08		A1/13	-1,57		A1/13	-1,27		A1/13	-1,35
	A1/14	-2,05		A1/14	-1,55		A1/14	-1,26		A1/14	-1,33
X+	A1/21	-1,42	X+	A1/18	-1,09	X+	A1/18	-0,87	X+	A1/20	-0,91
X-	A1/30	-1,43	X-	A1/25	-1,09	X-	A1/25	-0,88	X-	A1/27	-0,93
Y+	A1/40	-1,39	Y+	A1/41	-1,10	Y+	A1/41	-0,88	Y+	A1/41	-0,90
Y-	A1/46	-1,45	Y-	A1/43	-1,07	Y-	A1/43	-0,87	Y-	A1/43	-0,93
74	A1/1	-2,25	75	A1/1	-1,70	76	A1/1	-1,26	77	A1/1	-1,33
	A1/2	-2,20		A1/2	-1,65		A1/2	-1,21		A1/2	-1,29
	A1/3	-2,26		A1/3	-1,70		A1/3	-1,26		A1/3	-1,33
	A1/4	-2,21		A1/4	-1,65		A1/4	-1,22		A1/4	-1,30
	A1/5	-2,17		A1/5	-1,63		A1/5	-1,20		A1/5	-1,27
	A1/6	-2,25		A1/6	-1,70		A1/6	-1,25		A1/6	-1,33
	A1/7	-2,20		A1/7	-1,65		A1/7	-1,21		A1/7	-1,29
	A1/8	-2,15		A1/8	-1,62		A1/8	-1,20		A1/8	-1,26
	A1/9	-2,25		A1/9	-1,69		A1/9	-1,25		A1/9	-1,33
	A1/10	-2,20		A1/10	-1,64		A1/10	-1,21		A1/10	-1,29
	A1/11	-2,15		A1/11	-1,62		A1/11	-1,20		A1/11	-1,27
	A1/12	-2,26		A1/12	-1,70		A1/12	-1,26		A1/12	-1,34
	A1/13	-2,21		A1/13	-1,65		A1/13	-1,22		A1/13	-1,30

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/14	-2,17		A1/14	-1,62		A1/14	-1,20		A1/14	-1,28
X+	A1/21	-1,55	X+	A1/21	-1,15	X+	A1/21	-0,85	X+	A1/21	-0,90
X-	A1/30	-1,45	X-	A1/30	-1,10	X-	A1/30	-0,82	X-	A1/30	-0,87
Y+	A1/31	-1,47	Y+	A1/31	-1,13	Y+	A1/31	-0,81	Y+	A1/31	-0,84
Y-	A1/37	-1,54	Y-	A1/37	-1,14	Y-	A1/37	-0,85	Y-	A1/37	-0,91
78	A1/1	-1,99	79	A1/1	-1,42	80	A1/1	-1,28	81	A1/1	-1,42
	A1/2	-1,95		A1/2	-1,38		A1/2	-1,24		A1/2	-1,38
	A1/3	-1,99		A1/3	-1,42		A1/3	-1,28		A1/3	-1,42
	A1/4	-1,95		A1/4	-1,38		A1/4	-1,24		A1/4	-1,38
	A1/5	-1,91		A1/5	-1,36		A1/5	-1,22		A1/5	-1,35
	A1/6	-1,98		A1/6	-1,42		A1/6	-1,28		A1/6	-1,42
	A1/7	-1,94		A1/7	-1,38		A1/7	-1,24		A1/7	-1,37
	A1/8	-1,90		A1/8	-1,36		A1/8	-1,22		A1/8	-1,33
	A1/9	-1,99		A1/9	-1,42		A1/9	-1,28		A1/9	-1,42
	A1/10	-1,94		A1/10	-1,38		A1/10	-1,24		A1/10	-1,37
	A1/11	-1,91		A1/11	-1,36		A1/11	-1,22		A1/11	-1,34
	A1/12	-1,99		A1/12	-1,42		A1/12	-1,28		A1/12	-1,43
	A1/13	-1,95		A1/13	-1,37		A1/13	-1,24		A1/13	-1,38
	A1/14	-1,92		A1/14	-1,35		A1/14	-1,22		A1/14	-1,35
X+	A1/21	-1,35	X+	A1/15	-0,96	X+	A1/21	-0,84	X+	A1/20	-0,93
X-	A1/30	-1,31	X-	A1/24	-0,94	X-	A1/30	-0,82	X-	A1/27	-0,90
Y+	A1/31	-1,29	Y+	A1/31	-0,97	Y+	A1/31	-0,83	Y+	A1/34	-0,86
Y-	A1/37	-1,37	Y-	A1/37	-0,91	Y-	A1/37	-0,84	Y-	A1/36	-0,95
82	A1/1	-3,35	83	A1/1	-2,89	84	A1/1	-2,70	85	A1/1	-3,02
	A1/2	-3,27		A1/2	-2,81		A1/2	-2,62		A1/2	-2,94
	A1/3	-3,36		A1/3	-2,89		A1/3	-2,70		A1/3	-3,03
	A1/4	-3,28		A1/4	-2,82		A1/4	-2,62		A1/4	-2,94
	A1/5	-3,23		A1/5	-2,77		A1/5	-2,57		A1/5	-2,86
	A1/6	-3,36		A1/6	-2,90		A1/6	-2,70		A1/6	-3,03
	A1/7	-3,28		A1/7	-2,82		A1/7	-2,63		A1/7	-2,94
	A1/8	-3,24		A1/8	-2,78		A1/8	-2,57		A1/8	-2,88
	A1/9	-3,34		A1/9	-2,88		A1/9	-2,69		A1/9	-3,02
	A1/10	-3,27		A1/10	-2,80		A1/10	-2,61		A1/10	-2,94
	A1/11	-3,22		A1/11	-2,75		A1/11	-2,55		A1/11	-2,86
	A1/12	-3,34		A1/12	-2,88		A1/12	-2,69		A1/12	-3,02
	A1/13	-3,26		A1/13	-2,80		A1/13	-2,61		A1/13	-2,93
	A1/14	-3,21		A1/14	-2,74		A1/14	-2,55		A1/14	-2,85
X+	A1/18	-2,33	X+	A1/15	-2,00	X+	A1/15	-1,81	X+	A1/18	-1,94
X-	A1/25	-2,22	X-	A1/24	-1,86	X-	A1/24	-1,70	X-	A1/25	-1,94
Y+	A1/34	-2,35	Y+	A1/31	-2,01	Y+	A1/31	-1,81	Y+	A1/34	-1,99
Y-	A1/36	-2,19	Y-	A1/37	-1,83	Y-	A1/37	-1,70	Y-	A1/36	-1,86
86	A1/1	-2,80	87	A1/1	-2,63	88	A1/1	-2,38	89	A1/1	-1,74
	A1/2	-2,72		A1/2	-2,56		A1/2	-2,32		A1/2	-1,70
	A1/3	-2,80		A1/3	-2,63		A1/3	-2,38		A1/3	-1,74
	A1/4	-2,72		A1/4	-2,56		A1/4	-2,32		A1/4	-1,70
	A1/5	-2,65		A1/5	-2,49		A1/5	-2,28		A1/5	-1,67
	A1/6	-2,81		A1/6	-2,64		A1/6	-2,38		A1/6	-1,74
	A1/7	-2,72		A1/7	-2,56		A1/7	-2,32		A1/7	-1,70
	A1/8	-2,66		A1/8	-2,50		A1/8	-2,27		A1/8	-1,67
	A1/9	-2,80		A1/9	-2,64		A1/9	-2,37		A1/9	-1,74
	A1/10	-2,72		A1/10	-2,56		A1/10	-2,32		A1/10	-1,70
	A1/11	-2,66		A1/11	-2,50		A1/11	-2,27		A1/11	-1,66
	A1/12	-2,80		A1/12	-2,63		A1/12	-2,38		A1/12	-1,74
	A1/13	-2,72		A1/13	-2,56		A1/13	-2,32		A1/13	-1,70
	A1/14	-2,65		A1/14	-2,49		A1/14	-2,27		A1/14	-1,67
X+	A1/18	-1,78	X+	A1/18	-1,66	X+	A1/21	-1,59	X+	A1/21	-1,17
X-	A1/25	-1,80	X-	A1/25	-1,69	X-	A1/30	-1,53	X-	A1/30	-1,13
Y+	A1/41	-1,82	Y+	A1/41	-1,69	Y+	A1/31	-1,57	Y+	A1/31	-1,15
Y-	A1/43	-1,75	Y-	A1/43	-1,67	Y-	A1/37	-1,57	Y-	A1/37	-1,15
90	A1/1	-1,65	91	A1/1	-2,05	92	A1/1	-1,51	93	A1/1	-1,76
	A1/2	-1,61		A1/2	-1,99		A1/2	-1,47		A1/2	-1,72
	A1/3	-1,66		A1/3	-2,05		A1/3	-1,51		A1/3	-1,76
	A1/4	-1,62		A1/4	-2,00		A1/4	-1,47		A1/4	-1,72
	A1/5	-1,59		A1/5	-1,95		A1/5	-1,44		A1/5	-1,69
	A1/6	-1,65		A1/6	-2,07		A1/6	-1,52		A1/6	-1,77
	A1/7	-1,61		A1/7	-2,01		A1/7	-1,48		A1/7	-1,73
	A1/8	-1,58		A1/8	-1,97		A1/8	-1,46		A1/8	-1,71
	A1/9	-1,65		A1/9	-2,05		A1/9	-1,51		A1/9	-1,76
	A1/10	-1,61		A1/10	-1,99		A1/10	-1,47		A1/10	-1,72
	A1/11	-1,58		A1/11	-1,94		A1/11	-1,44		A1/11	-1,69
	A1/12	-1,65		A1/12	-2,03		A1/12	-1,50		A1/12	-1,75
	A1/13	-1,61		A1/13	-1,98		A1/13	-1,46		A1/13	-1,71
	A1/14	-1,58		A1/14	-1,91		A1/14	-1,42		A1/14	-1,67
X+	A1/15	-1,11	X+	A1/15	-1,37	X+	A1/15	-1,01	X+	A1/15	-1,19
X-	A1/24	-1,07	X-	A1/24	-1,33	X-	A1/24	-1,00	X-	A1/24	-1,18
Y+	A1/31	-1,10	Y+	A1/31	-1,45	Y+	A1/31	-1,07	Y+	A1/31	-1,24
Y-	A1/37	-1,09	Y-	A1/37	-1,18	Y-	A1/37	-0,90	Y-	A1/37	-1,10

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
94	A1/1	-2,63	95	A1/1	-2,32	96	A1/1	-2,43	97	A1/1	-3,13
	A1/2	-2,59		A1/2	-2,28		A1/2	-2,39		A1/2	-3,09
	A1/3	-2,62		A1/3	-2,31		A1/3	-2,41		A1/3	-3,11
	A1/4	-2,58		A1/4	-2,27		A1/4	-2,38		A1/4	-3,07
	A1/5	-2,52		A1/5	-2,23		A1/5	-2,33		A1/5	-3,00
	A1/6	-2,65		A1/6	-2,34		A1/6	-2,45		A1/6	-3,15
	A1/7	-2,61		A1/7	-2,30		A1/7	-2,41		A1/7	-3,12
	A1/8	-2,58		A1/8	-2,28		A1/8	-2,39		A1/8	-3,08
	A1/9	-2,64		A1/9	-2,33		A1/9	-2,44		A1/9	-3,16
	A1/10	-2,60		A1/10	-2,29		A1/10	-2,41		A1/10	-3,12
	A1/11	-2,56		A1/11	-2,26		A1/11	-2,38		A1/11	-3,08
	A1/12	-2,60		A1/12	-2,30		A1/12	-2,41		A1/12	-3,11
	A1/13	-2,56		A1/13	-2,26		A1/13	-2,38		A1/13	-3,07
	A1/14	-2,50		A1/14	-2,21		A1/14	-2,33		A1/14	-3,00
	X+ A1/18	-1,76		X+ A1/18	-1,54		X+ A1/18	-1,56		X+ A1/18	-1,93
98	X- A1/25	-1,97	99	X- A1/25	-1,75	100	X- A1/25	-1,87	101	X- A1/25	-2,48
	Y+ A1/41	-2,04		Y+ A1/41	-1,79		Y+ A1/41	-1,85		Y+ A1/41	-2,41
	Y- A1/43	-1,64		Y- A1/43	-1,47		Y- A1/43	-1,59		Y- A1/43	-2,05
98	A1/1	-2,86	99	A1/1	-2,71	100	A1/1	-2,91	101	A1/1	-3,66
	A1/2	-2,77		A1/2	-2,62		A1/2	-2,83		A1/2	-3,58
	A1/3	-2,86		A1/3	-2,71		A1/3	-2,92		A1/3	-3,67
	A1/4	-2,77		A1/4	-2,62		A1/4	-2,83		A1/4	-3,58
	A1/5	-2,71		A1/5	-2,58		A1/5	-2,78		A1/5	-3,52
	A1/6	-2,87		A1/6	-2,71		A1/6	-2,91		A1/6	-3,65
	A1/7	-2,78		A1/7	-2,62		A1/7	-2,82		A1/7	-3,56
	A1/8	-2,73		A1/8	-2,58		A1/8	-2,77		A1/8	-3,48
	A1/9	-2,86		A1/9	-2,71		A1/9	-2,91		A1/9	-3,66
	A1/10	-2,78		A1/10	-2,62		A1/10	-2,82		A1/10	-3,57
	A1/11	-2,71		A1/11	-2,57		A1/11	-2,77		A1/11	-3,50
	A1/12	-2,85		A1/12	-2,70		A1/12	-2,92		A1/12	-3,68
	A1/13	-2,77		A1/13	-2,62		A1/13	-2,83		A1/13	-3,59
	A1/14	-2,70		A1/14	-2,57		A1/14	-2,79		A1/14	-3,53
	X+ A1/18	-1,85		X+ A1/18	-1,77		X+ A1/21	-1,96		X+ A1/21	-2,50
102	X- A1/25	-1,87	103	X- A1/25	-1,75	104	X- A1/30	-1,89	105	X- A1/30	-2,40
	Y+ A1/41	-1,90		Y+ A1/34	-1,78		Y+ A1/31	-1,87		Y+ A1/31	-2,33
	Y- A1/43	-1,77		Y- A1/36	-1,74		Y- A1/37	-1,97		Y- A1/37	-2,54
102	A1/1	-1,60	103	A1/1	-1,47	104	A1/1	-1,39	105	A1/1	-1,59
	A1/2	-1,56		A1/2	-1,42		A1/2	-1,35		A1/2	-1,55
	A1/3	-1,60		A1/3	-1,47		A1/3	-1,39		A1/3	-1,59
	A1/4	-1,56		A1/4	-1,42		A1/4	-1,34		A1/4	-1,55
	A1/5	-1,52		A1/5	-1,40		A1/5	-1,32		A1/5	-1,51
	A1/6	-1,60		A1/6	-1,47		A1/6	-1,38		A1/6	-1,59
	A1/7	-1,56		A1/7	-1,42		A1/7	-1,34		A1/7	-1,54
	A1/8	-1,53		A1/8	-1,40		A1/8	-1,31		A1/8	-1,50
	A1/9	-1,60		A1/9	-1,47		A1/9	-1,39		A1/9	-1,60
	A1/10	-1,56		A1/10	-1,43		A1/10	-1,35		A1/10	-1,55
	A1/11	-1,53		A1/11	-1,40		A1/11	-1,32		A1/11	-1,51
	A1/12	-1,60		A1/12	-1,47		A1/12	-1,39		A1/12	-1,60
	A1/13	-1,55		A1/13	-1,42		A1/13	-1,35		A1/13	-1,55
	A1/14	-1,52		A1/14	-1,40		A1/14	-1,32		A1/14	-1,52
	X+ A1/18	-1,03		X+ A1/21	-0,94		X+ A1/21	-0,90		X+ A1/21	-1,02
106	X- A1/25	-1,07	107	X- A1/30	-0,97	108	X- A1/30	-0,91	109	X- A1/30	-1,04
	Y+ A1/41	-1,07		Y+ A1/40	-0,95		Y+ A1/40	-0,87		Y+ A1/40	-0,98
	Y- A1/43	-1,04		Y- A1/46	-0,96		Y- A1/46	-0,93		Y- A1/46	-1,07
106	A1/1	-1,49	107	A1/1	-1,65	108	A1/1	-1,43	109	A1/1	-1,30
	A1/2	-1,45		A1/2	-1,60		A1/2	-1,38		A1/2	-1,26
	A1/3	-1,49		A1/3	-1,65		A1/3	-1,43		A1/3	-1,30
	A1/4	-1,45		A1/4	-1,60		A1/4	-1,38		A1/4	-1,26
	A1/5	-1,43		A1/5	-1,57		A1/5	-1,35		A1/5	-1,23
	A1/6	-1,50		A1/6	-1,66		A1/6	-1,43		A1/6	-1,29
	A1/7	-1,46		A1/7	-1,61		A1/7	-1,38		A1/7	-1,26
	A1/8	-1,43		A1/8	-1,58		A1/8	-1,36		A1/8	-1,22
	A1/9	-1,49		A1/9	-1,65		A1/9	-1,43		A1/9	-1,30
	A1/10	-1,45		A1/10	-1,60		A1/10	-1,38		A1/10	-1,26
	A1/11	-1,42		A1/11	-1,57		A1/11	-1,35		A1/11	-1,23
	A1/12	-1,49		A1/12	-1,65		A1/12	-1,43		A1/12	-1,30
	A1/13	-1,45		A1/13	-1,60		A1/13	-1,38		A1/13	-1,26
	A1/14	-1,41		A1/14	-1,57		A1/14	-1,35		A1/14	-1,23
	X+ A1/15	-1,00		X+ A1/15	-1,09		X+ A1/15	-0,92		X+ A1/21	-0,82
110	X- A1/24	-0,97	111	X- A1/24	-1,08	112	X- A1/24	-0,92	113	X- A1/30	-0,83
	Y+ A1/31	-1,02		Y+ A1/31	-1,11		Y+ A1/40	-0,92		Y+ A1/40	-0,81
	Y- A1/37	-0,93		Y- A1/37	-1,04		Y- A1/46	-0,91		Y- A1/46	-0,84
110	A1/1	-1,58	111	A1/1	-1,70	112	A1/1	-1,81	113	A1/1	-2,13
	A1/2	-1,56		A1/2	-1,67		A1/2	-1,78		A1/2	-2,10
	A1/3	-1,58		A1/3	-1,70		A1/3	-1,81		A1/3	-2,13
	A1/4	-1,56		A1/4	-1,67		A1/4	-1,78		A1/4	-2,10
	A1/5	-1,53		A1/5	-1,64		A1/5	-1,75		A1/5	-2,05
	A1/6	-1,59		A1/6	-1,70		A1/6	-1,81		A1/6	-2,12

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/7	-1,56		A1/7	-1,67		A1/7	-1,78		A1/7	-2,09
	A1/8	-1,54		A1/8	-1,64		A1/8	-1,74		A1/8	-2,04
	A1/9	-1,58		A1/9	-1,70		A1/9	-1,81		A1/9	-2,13
	A1/10	-1,56		A1/10	-1,67		A1/10	-1,78		A1/10	-2,10
	A1/11	-1,53		A1/11	-1,64		A1/11	-1,75		A1/11	-2,05
	A1/12	-1,58		A1/12	-1,69		A1/12	-1,81		A1/12	-2,14
	A1/13	-1,55		A1/13	-1,67		A1/13	-1,79		A1/13	-2,10
	A1/14	-1,52		A1/14	-1,64		A1/14	-1,75		A1/14	-2,06
X+	A1/15	-1,08	X+	A1/15	-1,15	X+	A1/20	-1,22	X+	A1/20	-1,43
X-	A1/24	-1,08	X-	A1/24	-1,15	X-	A1/27	-1,23	X-	A1/27	-1,43
Y+	A1/31	-1,12	Y+	A1/40	-1,16	Y+	A1/41	-1,19	Y+	A1/41	-1,36
Y-	A1/37	-1,02	Y-	A1/46	-1,13	Y-	A1/43	-1,24	Y-	A1/43	-1,47
114	A1/1	-2,19	115	A1/1	-2,82	116	A1/1	-2,34	117	A1/1	-2,85
	A1/2	-2,15		A1/2	-2,77		A1/2	-2,30		A1/2	-2,81
	A1/3	-2,19		A1/3	-2,82		A1/3	-2,33		A1/3	-2,83
	A1/4	-2,16		A1/4	-2,77		A1/4	-2,30		A1/4	-2,80
	A1/5	-2,12		A1/5	-2,73		A1/5	-2,26		A1/5	-2,74
	A1/6	-2,19		A1/6	-2,81		A1/6	-2,34		A1/6	-2,86
	A1/7	-2,15		A1/7	-2,77		A1/7	-2,30		A1/7	-2,83
	A1/8	-2,11		A1/8	-2,72		A1/8	-2,27		A1/8	-2,80
	A1/9	-2,19		A1/9	-2,82		A1/9	-2,34		A1/9	-2,86
	A1/10	-2,15		A1/10	-2,78		A1/10	-2,31		A1/10	-2,83
	A1/11	-2,11		A1/11	-2,74		A1/11	-2,28		A1/11	-2,80
	A1/12	-2,20		A1/12	-2,83		A1/12	-2,34		A1/12	-2,83
	A1/13	-2,16		A1/13	-2,78		A1/13	-2,31		A1/13	-2,80
	A1/14	-2,12		A1/14	-2,75		A1/14	-2,28		A1/14	-2,74
X+	A1/21	-1,51	X+	A1/21	-1,94	X+	A1/21	-1,55	X+	A1/15	-1,84
X-	A1/30	-1,46	X-	A1/30	-1,97	X-	A1/30	-1,71	X-	A1/24	-2,18
Y+	A1/31	-1,45	Y+	A1/40	-1,88	Y+	A1/40	-1,63	Y+	A1/40	-2,15
Y-	A1/37	-1,51	Y-	A1/46	-2,00	Y-	A1/46	-1,67	Y-	A1/46	-1,91
118	A1/1	-1,58	119	A1/1	-1,22	120	A1/1	-1,67	121	A1/1	-2,19
	A1/2	-1,53		A1/2	-1,18		A1/2	-1,62		A1/2	-2,15
	A1/3	-1,58		A1/3	-1,22		A1/3	-1,67		A1/3	-2,19
	A1/4	-1,53		A1/4	-1,18		A1/4	-1,62		A1/4	-2,15
	A1/5	-1,50		A1/5	-1,16		A1/5	-1,59		A1/5	-2,10
	A1/6	-1,59		A1/6	-1,23		A1/6	-1,67		A1/6	-2,20
	A1/7	-1,54		A1/7	-1,18		A1/7	-1,62		A1/7	-2,16
	A1/8	-1,51		A1/8	-1,17		A1/8	-1,60		A1/8	-2,12
	A1/9	-1,58		A1/9	-1,22		A1/9	-1,67		A1/9	-2,20
	A1/10	-1,53		A1/10	-1,18		A1/10	-1,62		A1/10	-2,15
	A1/11	-1,50		A1/11	-1,16		A1/11	-1,60		A1/11	-2,12
	A1/12	-1,58		A1/12	-1,22		A1/12	-1,67		A1/12	-2,19
	A1/13	-1,53		A1/13	-1,18		A1/13	-1,62		A1/13	-2,15
	A1/14	-1,49		A1/14	-1,16		A1/14	-1,59		A1/14	-2,10
X+	A1/18	-1,03	X+	A1/18	-0,81	X+	A1/15	-1,10	X+	A1/15	-1,44
X-	A1/25	-1,03	X-	A1/25	-0,81	X-	A1/24	-1,12	X-	A1/24	-1,51
Y+	A1/41	-1,07	Y+	A1/41	-0,83	Y+	A1/40	-1,12	Y+	A1/40	-1,51
Y-	A1/43	-0,96	Y-	A1/43	-0,77	Y-	A1/46	-1,10	Y-	A1/46	-1,44
122	A1/1	-1,39	123	A1/1	-1,24	124	A1/1	-1,48	125	A1/1	-2,00
	A1/2	-1,35		A1/2	-1,20		A1/2	-1,44		A1/2	-1,96
	A1/3	-1,39		A1/3	-1,24		A1/3	-1,48		A1/3	-2,00
	A1/4	-1,34		A1/4	-1,20		A1/4	-1,44		A1/4	-1,96
	A1/5	-1,31		A1/5	-1,18		A1/5	-1,42		A1/5	-1,92
	A1/6	-1,39		A1/6	-1,24		A1/6	-1,48		A1/6	-2,00
	A1/7	-1,35		A1/7	-1,20		A1/7	-1,44		A1/7	-1,96
	A1/8	-1,32		A1/8	-1,18		A1/8	-1,42		A1/8	-1,93
	A1/9	-1,39		A1/9	-1,24		A1/9	-1,48		A1/9	-2,00
	A1/10	-1,35		A1/10	-1,20		A1/10	-1,44		A1/10	-1,96
	A1/11	-1,32		A1/11	-1,18		A1/11	-1,42		A1/11	-1,92
	A1/12	-1,39		A1/12	-1,24		A1/12	-1,49		A1/12	-2,00
	A1/13	-1,34		A1/13	-1,20		A1/13	-1,44		A1/13	-1,96
	A1/14	-1,31		A1/14	-1,18		A1/14	-1,42		A1/14	-1,92
X+	A1/15	-0,88	X+	A1/15	-0,80	X+	A1/20	-0,99	X+	A1/18	-1,34
X-	A1/24	-0,90	X-	A1/24	-0,81	X-	A1/27	-0,98	X-	A1/25	-1,32
Y+	A1/40	-0,90	Y+	A1/40	-0,80	Y+	A1/34	-0,97	Y+	A1/34	-1,35
Y-	A1/46	-0,87	Y-	A1/46	-0,80	Y-	A1/36	-0,99	Y-	A1/36	-1,31
126	A1/1	-3,84	127	A1/1	-2,95	128	A1/1	-4,00	129	A1/1	-4,38
	A1/2	-3,75		A1/2	-2,87		A1/2	-3,89		A1/2	-4,30
	A1/3	-3,84		A1/3	-2,95		A1/3	-4,00		A1/3	-4,38
	A1/4	-3,75		A1/4	-2,87		A1/4	-3,89		A1/4	-4,30
	A1/5	-3,68		A1/5	-2,83		A1/5	-3,85		A1/5	-4,21
	A1/6	-3,83		A1/6	-2,95		A1/6	-4,00		A1/6	-4,39
	A1/7	-3,75		A1/7	-2,86		A1/7	-3,89		A1/7	-4,31
	A1/8	-3,67		A1/8	-2,83		A1/8	-3,84		A1/8	-4,23
	A1/9	-3,84		A1/9	-2,95		A1/9	-4,00		A1/9	-4,38
	A1/10	-3,75		A1/10	-2,87		A1/10	-3,89		A1/10	-4,30
	A1/11	-3,68		A1/11	-2,83		A1/11	-3,85		A1/11	-4,22
	A1/12	-3,84		A1/12	-2,96		A1/12	-4,01		A1/12	-4,37

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/13	-3,75		A1/13	-2,87		A1/13	-3,90		A1/13	-4,29
	A1/14	-3,68		A1/14	-2,84		A1/14	-3,86		A1/14	-4,20
X+	A1/20	-2,53	X+	A1/20	-1,97	X+	A1/20	-2,69	X+	A1/15	-2,93
X-	A1/27	-2,54	X-	A1/27	-1,98	X-	A1/27	-2,71	X-	A1/24	-2,95
Y+	A1/41	-2,52	Y+	A1/41	-1,94	Y+	A1/41	-2,64	Y+	A1/40	-2,99
Y-	A1/43	-2,55	Y-	A1/43	-2,00	Y-	A1/43	-2,73	Y-	A1/46	-2,86
130	A1/1	-2,40	131	A1/1	-1,90	132	A1/1	-2,48	133	A1/1	-2,38
	A1/2	-2,37		A1/2	-1,88		A1/2	-2,45		A1/2	-2,35
	A1/3	-2,42		A1/3	-1,91		A1/3	-2,50		A1/3	-2,40
	A1/4	-2,39		A1/4	-1,89		A1/4	-2,47		A1/4	-2,38
	A1/5	-2,37		A1/5	-1,87		A1/5	-2,45		A1/5	-2,35
	A1/6	-2,37		A1/6	-1,89		A1/6	-2,49		A1/6	-2,41
	A1/7	-2,34		A1/7	-1,87		A1/7	-2,46		A1/7	-2,38
	A1/8	-2,28		A1/8	-1,84		A1/8	-2,44		A1/8	-2,36
	A1/9	-2,38		A1/9	-1,89		A1/9	-2,47		A1/9	-2,36
	A1/10	-2,35		A1/10	-1,86		A1/10	-2,44		A1/10	-2,33
	A1/11	-2,30		A1/11	-1,83		A1/11	-2,39		A1/11	-2,28
	A1/12	-2,42		A1/12	-1,91		A1/12	-2,48		A1/12	-2,35
	A1/13	-2,40		A1/13	-1,88		A1/13	-2,44		A1/13	-2,33
	A1/14	-2,38		A1/14	-1,86		A1/14	-2,41		A1/14	-2,27
X+	A1/20	-1,97	X+	A1/20	-1,49	X+	A1/18	-1,95	X+	A1/18	-1,93
X-	A1/27	-1,54	X-	A1/27	-1,21	X-	A1/25	-1,58	X-	A1/25	-1,49
Y+	A1/34	-1,56	Y+	A1/34	-1,34	Y+	A1/34	-1,87	Y+	A1/34	-1,93
Y-	A1/36	-1,97	Y-	A1/36	-1,43	Y-	A1/36	-1,72	Y-	A1/36	-1,49
134	A1/1	-2,28	135	A1/1	-2,18	136	A1/1	-2,43	137	A1/1	-2,37
	A1/2	-2,25		A1/2	-2,15		A1/2	-2,39		A1/2	-2,33
	A1/3	-2,29		A1/3	-2,18		A1/3	-2,43		A1/3	-2,37
	A1/4	-2,25		A1/4	-2,15		A1/4	-2,39		A1/4	-2,33
	A1/5	-2,21		A1/5	-2,10		A1/5	-2,34		A1/5	-2,29
	A1/6	-2,26		A1/6	-2,15		A1/6	-2,38		A1/6	-2,33
	A1/7	-2,22		A1/7	-2,11		A1/7	-2,35		A1/7	-2,29
	A1/8	-2,15		A1/8	-2,04		A1/8	-2,27		A1/8	-2,23
	A1/9	-2,28		A1/9	-2,18		A1/9	-2,42		A1/9	-2,37
	A1/10	-2,24		A1/10	-2,14		A1/10	-2,38		A1/10	-2,33
	A1/11	-2,18		A1/11	-2,09		A1/11	-2,33		A1/11	-2,29
	A1/12	-2,31		A1/12	-2,22		A1/12	-2,47		A1/12	-2,41
	A1/13	-2,28		A1/13	-2,18		A1/13	-2,43		A1/13	-2,37
	A1/14	-2,24		A1/14	-2,15		A1/14	-2,40		A1/14	-2,36
X+	A1/21	-1,66	X+	A1/20	-1,55	X+	A1/20	-1,75	X+	A1/20	-1,72
X-	A1/30	-1,51	X-	A1/27	-1,50	X-	A1/27	-1,69	X-	A1/27	-1,69
Y+	A1/31	-1,32	Y+	A1/34	-1,20	Y+	A1/34	-1,33	Y+	A1/34	-1,33
Y-	A1/37	-1,76	Y-	A1/36	-1,72	Y-	A1/36	-1,94	Y-	A1/36	-1,92
138	A1/1	-2,58	139	A1/1	-3,25	140	A1/1	-2,16	141	A1/1	-2,96
	A1/2	-2,54		A1/2	-3,22		A1/2	-2,13		A1/2	-2,92
	A1/3	-2,58		A1/3	-3,26		A1/3	-2,15		A1/3	-2,95
	A1/4	-2,54		A1/4	-3,22		A1/4	-2,12		A1/4	-2,91
	A1/5	-2,50		A1/5	-3,16		A1/5	-2,08		A1/5	-2,86
	A1/6	-2,53		A1/6	-3,18		A1/6	-2,15		A1/6	-2,94
	A1/7	-2,49		A1/7	-3,14		A1/7	-2,12		A1/7	-2,89
	A1/8	-2,41		A1/8	-3,03		A1/8	-2,08		A1/8	-2,84
	A1/9	-2,57		A1/9	-3,25		A1/9	-2,17		A1/9	-2,98
	A1/10	-2,54		A1/10	-3,21		A1/10	-2,14		A1/10	-2,93
	A1/11	-2,50		A1/11	-3,15		A1/11	-2,11		A1/11	-2,91
	A1/12	-2,62		A1/12	-3,33		A1/12	-2,17		A1/12	-2,99
	A1/13	-2,59		A1/13	-3,29		A1/13	-2,13		A1/13	-2,94
	A1/14	-2,58		A1/14	-3,28		A1/14	-2,11		A1/14	-2,93
X+	A1/20	-1,90	X+	A1/20	-2,48	X+	A1/20	-1,42	X+	A1/21	-1,98
X-	A1/27	-1,88	X-	A1/27	-2,37	X-	A1/27	-1,61	X-	A1/30	-2,27
Y+	A1/34	-1,42	Y+	A1/34	-1,71	Y+	A1/41	-1,46	Y+	A1/40	-1,92
Y-	A1/36	-2,15	Y-	A1/36	-2,84	Y-	A1/43	-1,59	Y-	A1/46	-2,30
142	A1/1	-2,71	143	A1/1	-3,89	144	A1/1	-3,01	145	A1/1	-2,69
	A1/2	-2,67		A1/2	-3,82		A1/2	-2,93		A1/2	-2,61
	A1/3	-2,69		A1/3	-3,88		A1/3	-3,01		A1/3	-2,69
	A1/4	-2,65		A1/4	-3,80		A1/4	-2,93		A1/4	-2,61
	A1/5	-2,61		A1/5	-3,73		A1/5	-2,88		A1/5	-2,56
	A1/6	-2,67		A1/6	-3,88		A1/6	-3,01		A1/6	-2,70
	A1/7	-2,63		A1/7	-3,81		A1/7	-2,93		A1/7	-2,61
	A1/8	-2,57		A1/8	-3,73		A1/8	-2,88		A1/8	-2,57
	A1/9	-2,72		A1/9	-3,90		A1/9	-3,02		A1/9	-2,70
	A1/10	-2,69		A1/10	-3,83		A1/10	-2,94		A1/10	-2,61
	A1/11	-2,67		A1/11	-3,77		A1/11	-2,89		A1/11	-2,57
	A1/12	-2,75		A1/12	-3,90		A1/12	-3,01		A1/12	-2,69
	A1/13	-2,71		A1/13	-3,82		A1/13	-2,93		A1/13	-2,61
	A1/14	-2,70		A1/14	-3,76		A1/14	-2,89		A1/14	-2,56
X+	A1/21	-1,79	X+	A1/20	-2,51	X+	A1/20	-1,95	X+	A1/18	-1,73
X-	A1/30	-2,19	X-	A1/27	-2,74	X-	A1/27	-2,03	X-	A1/25	-1,79
Y+	A1/40	-1,65	Y+	A1/41	-2,57	Y+	A1/41	-1,99	Y+	A1/41	-1,79
Y-	A1/46	-2,27	Y-	A1/43	-2,71	Y-	A1/43	-2,01	Y-	A1/43	-1,73

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
146	A1/1	-2,79	147	A1/1	-3,51	148	A1/1	-3,03	149	A1/1	-3,00
	A1/2	-2,71		A1/2	-3,42		A1/2	-2,95		A1/2	-2,92
	A1/3	-2,79		A1/3	-3,50		A1/3	-3,03		A1/3	-3,01
	A1/4	-2,70		A1/4	-3,41		A1/4	-2,95		A1/4	-2,93
	A1/5	-2,64		A1/5	-3,34		A1/5	-2,89		A1/5	-2,86
	A1/6	-2,80		A1/6	-3,51		A1/6	-3,04		A1/6	-3,01
	A1/7	-2,71		A1/7	-3,42		A1/7	-2,95		A1/7	-2,92
	A1/8	-2,66		A1/8	-3,35		A1/8	-2,89		A1/8	-2,86
	A1/9	-2,79		A1/9	-3,52		A1/9	-3,03		A1/9	-3,00
	A1/10	-2,71		A1/10	-3,42		A1/10	-2,95		A1/10	-2,91
	A1/11	-2,65		A1/11	-3,36		A1/11	-2,88		A1/11	-2,84
	A1/12	-2,78		A1/12	-3,51		A1/12	-3,03		A1/12	-3,00
	A1/13	-2,70		A1/13	-3,42		A1/13	-2,94		A1/13	-2,91
	A1/14	-2,63		A1/14	-3,35		A1/14	-2,88		A1/14	-2,84
	X+ A1/18	-1,77		X+ A1/18	-2,23		X+ A1/18	-1,98		X+ A1/15	-2,01
150	X- A1/25	-1,83	151	X- A1/25	-2,37	152	X- A1/25	-1,97	153	X- A1/24	-1,87
	Y+ A1/41	-1,85		Y+ A1/41	-2,34		Y+ A1/34	-2,00		Y+ A1/31	-2,00
	Y- A1/43	-1,74		Y- A1/43	-2,30		Y- A1/36	-1,93		Y- A1/37	-1,90
150	A1/1	-3,22	151	A1/1	-3,28	152	A1/1	-3,72	153	A1/1	-3,23
	A1/2	-3,14		A1/2	-3,20		A1/2	-3,63		A1/2	-3,14
	A1/3	-3,22		A1/3	-3,27		A1/3	-3,71		A1/3	-3,24
	A1/4	-3,14		A1/4	-3,19		A1/4	-3,62		A1/4	-3,15
	A1/5	-3,08		A1/5	-3,13		A1/5	-3,55		A1/5	-3,10
	A1/6	-3,21		A1/6	-3,27		A1/6	-3,71		A1/6	-3,22
	A1/7	-3,13		A1/7	-3,19		A1/7	-3,62		A1/7	-3,14
	A1/8	-3,07		A1/8	-3,13		A1/8	-3,55		A1/8	-3,07
	A1/9	-3,21		A1/9	-3,28		A1/9	-3,72		A1/9	-3,21
	A1/10	-3,14		A1/10	-3,20		A1/10	-3,63		A1/10	-3,13
	A1/11	-3,08		A1/11	-3,14		A1/11	-3,57		A1/11	-3,05
	A1/12	-3,22		A1/12	-3,28		A1/12	-3,72		A1/12	-3,23
	A1/13	-3,14		A1/13	-3,20		A1/13	-3,63		A1/13	-3,14
	A1/14	-3,08		A1/14	-3,14		A1/14	-3,57		A1/14	-3,09
	X+ A1/21	-2,13		X+ A1/20	-2,14		X+ A1/20	-2,40		X+ A1/21	-2,28
154	X- A1/30	-2,11	155	X- A1/27	-2,21	156	X- A1/27	-2,52	157	X- A1/30	-1,98
	Y+ A1/31	-2,10		Y+ A1/41	-2,14		Y+ A1/41	-2,42		Y+ A1/31	-2,13
	Y- A1/37	-2,14		Y- A1/43	-2,20		Y- A1/43	-2,51		Y- A1/37	-2,20
154	A1/1	-3,22	155	A1/1	-2,61	156	A1/1	-2,53	157	A1/1	-3,14
	A1/2	-3,13		A1/2	-2,53		A1/2	-2,46		A1/2	-3,04
	A1/3	-3,23		A1/3	-2,62		A1/3	-2,53		A1/3	-3,14
	A1/4	-3,14		A1/4	-2,54		A1/4	-2,46		A1/4	-3,04
	A1/5	-3,09		A1/5	-2,49		A1/5	-2,40		A1/5	-2,98
	A1/6	-3,22		A1/6	-2,61		A1/6	-2,54		A1/6	-3,15
	A1/7	-3,13		A1/7	-2,54		A1/7	-2,46		A1/7	-3,05
	A1/8	-3,07		A1/8	-2,49		A1/8	-2,41		A1/8	-2,98
	A1/9	-3,21		A1/9	-2,60		A1/9	-2,53		A1/9	-3,14
	A1/10	-3,11		A1/10	-2,53		A1/10	-2,45		A1/10	-3,04
	A1/11	-3,05		A1/11	-2,47		A1/11	-2,39		A1/11	-2,96
	A1/12	-3,22		A1/12	-2,61		A1/12	-2,52		A1/12	-3,13
	A1/13	-3,13		A1/13	-2,53		A1/13	-2,45		A1/13	-3,03
	A1/14	-3,07		A1/14	-2,48		A1/14	-2,39		A1/14	-2,95
	X+ A1/21	-2,25		X+ A1/15	-1,75		X+ A1/15	-1,64		X+ A1/15	-2,06
158	X- A1/30	-1,97	159	X- A1/24	-1,63	160	X- A1/24	-1,61	161	X- A1/24	-1,96
	Y+ A1/31	-2,14		Y+ A1/31	-1,73		Y+ A1/31	-1,66		Y+ A1/31	-2,07
	Y- A1/37	-2,16		Y- A1/37	-1,68		Y- A1/37	-1,58		Y- A1/37	-1,95
158	A1/1	-2,59	159	A1/1	-2,91	160	A1/1	-4,26	161	A1/1	-3,81
	A1/2	-2,51		A1/2	-2,82		A1/2	-4,18		A1/2	-3,73
	A1/3	-2,60		A1/3	-2,91		A1/3	-4,26		A1/3	-3,80
	A1/4	-2,51		A1/4	-2,82		A1/4	-4,18		A1/4	-3,72
	A1/5	-2,46		A1/5	-2,78		A1/5	-4,11		A1/5	-3,65
	A1/6	-2,60		A1/6	-2,91		A1/6	-4,27		A1/6	-3,82
	A1/7	-2,51		A1/7	-2,83		A1/7	-4,19		A1/7	-3,75
	A1/8	-2,47		A1/8	-2,79		A1/8	-4,12		A1/8	-3,70
	A1/9	-2,59		A1/9	-2,91		A1/9	-4,25		A1/9	-3,81
	A1/10	-2,51		A1/10	-2,82		A1/10	-4,17		A1/10	-3,74
	A1/11	-2,46		A1/11	-2,78		A1/11	-4,09		A1/11	-3,68
	A1/12	-2,59		A1/12	-2,90		A1/12	-4,25		A1/12	-3,79
	A1/13	-2,50		A1/13	-2,81		A1/13	-4,17		A1/13	-3,71
	A1/14	-2,45		A1/14	-2,77		A1/14	-4,08		A1/14	-3,64
	X+ A1/15	-1,70		X+ A1/15	-1,93		X+ A1/15	-2,93		X+ A1/18	-2,54
162	X- A1/24	-1,68	163	X- A1/24	-1,94	164	X- A1/24	-2,84	165	X- A1/25	-2,69
	Y+ A1/31	-1,72		Y+ A1/40	-1,97		Y+ A1/31	-2,97		Y+ A1/41	-2,75
	Y- A1/37	-1,64		Y- A1/46	-1,87		Y- A1/37	-2,78		Y- A1/43	-2,45
162	A1/1	-2,51	163	A1/1	-1,61	164	A1/1	-1,39	165	A1/1	-1,57
	A1/2	-2,45		A1/2	-1,56		A1/2	-1,35		A1/2	-1,53
	A1/3	-2,51		A1/3	-1,60		A1/3	-1,39		A1/3	-1,57
	A1/4	-2,44		A1/4	-1,55		A1/4	-1,35		A1/4	-1,53
	A1/5	-2,41		A1/5	-1,52		A1/5	-1,31		A1/5	-1,50

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SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/6	-2,52		A1/6	-1,61		A1/6	-1,39		A1/6	-1,57
	A1/7	-2,45		A1/7	-1,56		A1/7	-1,35		A1/7	-1,53
	A1/8	-2,42		A1/8	-1,53		A1/8	-1,32		A1/8	-1,50
	A1/9	-2,52		A1/9	-1,61		A1/9	-1,40		A1/9	-1,58
	A1/10	-2,45		A1/10	-1,56		A1/10	-1,35		A1/10	-1,54
	A1/11	-2,42		A1/11	-1,53		A1/11	-1,33		A1/11	-1,51
	A1/12	-2,51		A1/12	-1,60		A1/12	-1,39		A1/12	-1,57
	A1/13	-2,44		A1/13	-1,55		A1/13	-1,35		A1/13	-1,53
	A1/14	-2,40		A1/14	-1,52		A1/14	-1,31		A1/14	-1,50
X+	A1/18	-1,67	X+	A1/18	-1,03	X+	A1/18	-0,86	X+	A1/18	-0,99
X-	A1/25	-1,73	X-	A1/25	-1,09	X-	A1/25	-0,94	X-	A1/25	-1,07
Y+	A1/41	-1,76	Y+	A1/41	-1,09	Y+	A1/41	-0,92	Y+	A1/41	-1,04
Y-	A1/43	-1,62	Y-	A1/43	-1,03	Y-	A1/43	-0,88	Y-	A1/43	-1,04
166	A1/1	-1,57	167	A1/1	-1,68	168	A1/1	-1,78	169	A1/1	-1,79
	A1/2	-1,53		A1/2	-1,63		A1/2	-1,74		A1/2	-1,74
	A1/3	-1,57		A1/3	-1,68		A1/3	-1,78		A1/3	-1,78
	A1/4	-1,53		A1/4	-1,63		A1/4	-1,74		A1/4	-1,74
	A1/5	-1,49		A1/5	-1,59		A1/5	-1,70		A1/5	-1,71
	A1/6	-1,57		A1/6	-1,68		A1/6	-1,78		A1/6	-1,79
	A1/7	-1,53		A1/7	-1,63		A1/7	-1,74		A1/7	-1,74
	A1/8	-1,50		A1/8	-1,59		A1/8	-1,70		A1/8	-1,71
	A1/9	-1,57		A1/9	-1,67		A1/9	-1,78		A1/9	-1,79
	A1/10	-1,53		A1/10	-1,63		A1/10	-1,74		A1/10	-1,74
	A1/11	-1,50		A1/11	-1,59		A1/11	-1,70		A1/11	-1,71
	A1/12	-1,57		A1/12	-1,67		A1/12	-1,78		A1/12	-1,78
	A1/13	-1,53		A1/13	-1,63		A1/13	-1,74		A1/13	-1,74
	A1/14	-1,49		A1/14	-1,58		A1/14	-1,70		A1/14	-1,71
X+	A1/18	-1,01	X+	A1/18	-1,09	X+	A1/15	-1,18	X+	A1/18	-1,17
X-	A1/25	-1,03	X-	A1/25	-1,06	X-	A1/24	-1,17	X-	A1/25	-1,20
Y+	A1/41	-1,03	Y+	A1/34	-1,09	Y+	A1/31	-1,18	Y+	A1/41	-1,20
Y-	A1/43	-1,01	Y-	A1/36	-1,05	Y-	A1/37	-1,17	Y-	A1/43	-1,17
170	A1/1	-1,65	171	A1/1	-1,59	172	A1/1	-1,48	173	A1/1	-1,53
	A1/2	-1,61		A1/2	-1,55		A1/2	-1,44		A1/2	-1,49
	A1/3	-1,64		A1/3	-1,60		A1/3	-1,48		A1/3	-1,53
	A1/4	-1,61		A1/4	-1,56		A1/4	-1,44		A1/4	-1,49
	A1/5	-1,57		A1/5	-1,53		A1/5	-1,42		A1/5	-1,46
	A1/6	-1,65		A1/6	-1,60		A1/6	-1,48		A1/6	-1,53
	A1/7	-1,61		A1/7	-1,55		A1/7	-1,44		A1/7	-1,49
	A1/8	-1,58		A1/8	-1,53		A1/8	-1,42		A1/8	-1,47
	A1/9	-1,65		A1/9	-1,59		A1/9	-1,47		A1/9	-1,53
	A1/10	-1,61		A1/10	-1,54		A1/10	-1,43		A1/10	-1,49
	A1/11	-1,58		A1/11	-1,51		A1/11	-1,40		A1/11	-1,46
	A1/12	-1,64		A1/12	-1,59		A1/12	-1,47		A1/12	-1,52
	A1/13	-1,61		A1/13	-1,55		A1/13	-1,43		A1/13	-1,48
	A1/14	-1,57		A1/14	-1,52		A1/14	-1,40		A1/14	-1,45
X+	A1/18	-1,06	X+	A1/15	-1,12	X+	A1/15	-1,03	X+	A1/15	-1,03
X-	A1/25	-1,12	X-	A1/24	-0,99	X-	A1/24	-0,94	X-	A1/24	-1,02
Y+	A1/41	-1,11	Y+	A1/31	-1,09	Y+	A1/31	-1,02	Y+	A1/31	-1,05
Y-	A1/43	-1,07	Y-	A1/37	-1,04	Y-	A1/37	-0,96	Y-	A1/37	-0,97
174	A1/1	-1,66	175	A1/1	-1,51	176	A1/1	-1,57	177	A1/1	-1,71
	A1/2	-1,63		A1/2	-1,48		A1/2	-1,54		A1/2	-1,69
	A1/3	-1,66		A1/3	-1,51		A1/3	-1,57		A1/3	-1,71
	A1/4	-1,62		A1/4	-1,49		A1/4	-1,54		A1/4	-1,69
	A1/5	-1,59		A1/5	-1,46		A1/5	-1,52		A1/5	-1,67
	A1/6	-1,67		A1/6	-1,52		A1/6	-1,58		A1/6	-1,73
	A1/7	-1,63		A1/7	-1,49		A1/7	-1,55		A1/7	-1,71
	A1/8	-1,61		A1/8	-1,47		A1/8	-1,54		A1/8	-1,70
	A1/9	-1,67		A1/9	-1,51		A1/9	-1,56		A1/9	-1,71
	A1/10	-1,63		A1/10	-1,48		A1/10	-1,54		A1/10	-1,68
	A1/11	-1,60		A1/11	-1,45		A1/11	-1,51		A1/11	-1,65
	A1/12	-1,66		A1/12	-1,50		A1/12	-1,55		A1/12	-1,69
	A1/13	-1,62		A1/13	-1,48		A1/13	-1,53		A1/13	-1,66
	A1/14	-1,59		A1/14	-1,44		A1/14	-1,50		A1/14	-1,63
X+	A1/15	-1,10	X+	A1/15	-1,07	X+	A1/15	-1,13	X+	A1/15	-1,28
X-	A1/24	-1,15	X-	A1/24	-1,01	X-	A1/24	-1,07	X-	A1/24	-1,19
Y+	A1/40	-1,17	Y+	A1/31	-1,09	Y+	A1/31	-1,17	Y+	A1/31	-1,36
Y-	A1/46	-1,06	Y-	A1/37	-0,97	Y-	A1/37	-1,00	Y-	A1/37	-1,05
178	A1/1	-2,26	179	A1/1	-3,33	180	A1/1	-3,61	181	A1/1	-2,57
	A1/2	-2,23		A1/2	-3,29		A1/2	-3,56		A1/2	-2,52
	A1/3	-2,27		A1/3	-3,31		A1/3	-3,61		A1/3	-2,56
	A1/4	-2,24		A1/4	-3,27		A1/4	-3,55		A1/4	-2,52
	A1/5	-2,22		A1/5	-3,21		A1/5	-3,49		A1/5	-2,47
	A1/6	-2,30		A1/6	-3,35		A1/6	-3,62		A1/6	-2,56
	A1/7	-2,27		A1/7	-3,31		A1/7	-3,57		A1/7	-2,52
	A1/8	-2,26		A1/8	-3,27		A1/8	-3,52		A1/8	-2,47
	A1/9	-2,24		A1/9	-3,35		A1/9	-3,62		A1/9	-2,57
	A1/10	-2,22		A1/10	-3,30		A1/10	-3,57		A1/10	-2,52
	A1/11	-2,18		A1/11	-3,26		A1/11	-3,52		A1/11	-2,48

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/12	-2,22		A1/12	-3,30		A1/12	-3,60		A1/12	-2,57
	A1/13	-2,19		A1/13	-3,26		A1/13	-3,55		A1/13	-2,52
	A1/14	-2,13		A1/14	-3,19		A1/14	-3,49		A1/14	-2,48
X+	A1/15	-1,79	X+	A1/18	-2,19	X+	A1/18	-2,43	X+	A1/21	-1,71
X-	A1/24	-1,55	X-	A1/25	-2,52	X-	A1/25	-2,57	X-	A1/30	-1,76
Y+	A1/31	-1,92	Y+	A1/41	-2,54	Y+	A1/41	-2,58	Y+	A1/40	-1,71
Y-	A1/37	-1,33	Y-	A1/43	-2,15	Y-	A1/43	-2,41	Y-	A1/46	-1,76
182	A1/1	-3,61	183	A1/1	-3,11	184	A1/1	-3,02	185	A1/1	-2,86
	A1/2	-3,52		A1/2	-3,03		A1/2	-2,93		A1/2	-2,78
	A1/3	-3,62		A1/3	-3,12		A1/3	-3,02		A1/3	-2,86
	A1/4	-3,53		A1/4	-3,03		A1/4	-2,93		A1/4	-2,77
	A1/5	-3,47		A1/5	-2,98		A1/5	-2,86		A1/5	-2,70
	A1/6	-3,59		A1/6	-3,11		A1/6	-3,02		A1/6	-2,86
	A1/7	-3,51		A1/7	-3,02		A1/7	-2,93		A1/7	-2,78
	A1/8	-3,43		A1/8	-2,96		A1/8	-2,86		A1/8	-2,71
	A1/9	-3,59		A1/9	-3,11		A1/9	-3,02		A1/9	-2,87
	A1/10	-3,51		A1/10	-3,02		A1/10	-2,93		A1/10	-2,78
	A1/11	-3,43		A1/11	-2,95		A1/11	-2,86		A1/11	-2,71
	A1/12	-3,62		A1/12	-3,12		A1/12	-3,02		A1/12	-2,86
	A1/13	-3,53		A1/13	-3,03		A1/13	-2,93		A1/13	-2,78
	A1/14	-3,47		A1/14	-2,98		A1/14	-2,87		A1/14	-2,70
X+	A1/20	-2,51	X+	A1/20	-2,11	X+	A1/21	-1,95	X+	A1/15	-1,78
X-	A1/27	-2,27	X-	A1/27	-1,96	X-	A1/30	-1,92	X-	A1/24	-1,85
Y+	A1/34	-2,33	Y+	A1/34	-2,00	Y+	A1/31	-1,92	Y+	A1/40	-1,83
Y-	A1/36	-2,48	Y-	A1/36	-2,09	Y-	A1/37	-1,95	Y-	A1/46	-1,81
186	A1/1	-3,01	187	A1/1	-3,14	188	A1/1	-2,86	189	A1/1	-2,69
	A1/2	-2,92		A1/2	-3,05		A1/2	-2,78		A1/2	-2,61
	A1/3	-3,00		A1/3	-3,13		A1/3	-2,87		A1/3	-2,70
	A1/4	-2,91		A1/4	-3,04		A1/4	-2,78		A1/4	-2,61
	A1/5	-2,83		A1/5	-2,95		A1/5	-2,72		A1/5	-2,57
	A1/6	-3,01		A1/6	-3,14		A1/6	-2,86		A1/6	-2,69
	A1/7	-2,93		A1/7	-3,05		A1/7	-2,78		A1/7	-2,61
	A1/8	-2,85		A1/8	-2,97		A1/8	-2,71		A1/8	-2,56
	A1/9	-3,02		A1/9	-3,15		A1/9	-2,86		A1/9	-2,69
	A1/10	-2,93		A1/10	-3,06		A1/10	-2,77		A1/10	-2,60
	A1/11	-2,86		A1/11	-2,99		A1/11	-2,70		A1/11	-2,55
	A1/12	-3,01		A1/12	-3,14		A1/12	-2,86		A1/12	-2,69
	A1/13	-2,92		A1/13	-3,05		A1/13	-2,78		A1/13	-2,61
	A1/14	-2,85		A1/14	-2,97		A1/14	-2,71		A1/14	-2,56
X+	A1/15	-1,82	X+	A1/21	-1,86	X+	A1/20	-1,90	X+	A1/20	-1,79
X-	A1/24	-2,00	X-	A1/30	-2,10	X-	A1/27	-1,75	X-	A1/27	-1,71
Y+	A1/40	-1,94	Y+	A1/40	-2,02	Y+	A1/34	-1,85	Y+	A1/34	-1,75
Y-	A1/46	-1,93	Y-	A1/46	-2,02	Y-	A1/36	-1,85	Y-	A1/36	-1,76
190	A1/1	-2,92	191	A1/1	-3,47	192	A1/1	-4,50	193	A1/1	-3,51
	A1/2	-2,83		A1/2	-3,39		A1/2	-4,43		A1/2	-3,44
	A1/3	-2,91		A1/3	-3,46		A1/3	-4,47		A1/3	-3,49
	A1/4	-2,83		A1/4	-3,39		A1/4	-4,39		A1/4	-3,43
	A1/5	-2,78		A1/5	-3,31		A1/5	-4,31		A1/5	-3,38
	A1/6	-2,91		A1/6	-3,47		A1/6	-4,45		A1/6	-3,48
	A1/7	-2,83		A1/7	-3,39		A1/7	-4,37		A1/7	-3,41
	A1/8	-2,78		A1/8	-3,32		A1/8	-4,28		A1/8	-3,36
	A1/9	-2,92		A1/9	-3,48		A1/9	-4,53		A1/9	-3,52
	A1/10	-2,84		A1/10	-3,40		A1/10	-4,46		A1/10	-3,46
	A1/11	-2,79		A1/11	-3,34		A1/11	-4,43		A1/11	-3,43
	A1/12	-2,92		A1/12	-3,48		A1/12	-4,55		A1/12	-3,54
	A1/13	-2,84		A1/13	-3,40		A1/13	-4,48		A1/13	-3,47
	A1/14	-2,79		A1/14	-3,34		A1/14	-4,46		A1/14	-3,45
X+	A1/21	-1,89	X+	A1/21	-2,23	X+	A1/21	-2,88	X+	A1/21	-2,33
X-	A1/30	-1,96	X-	A1/30	-2,38	X-	A1/30	-3,59	X-	A1/30	-2,64
Y+	A1/40	-1,91	Y+	A1/40	-2,27	Y+	A1/40	-2,80	Y+	A1/40	-2,24
Y-	A1/46	-1,95	Y-	A1/46	-2,36	Y-	A1/46	-3,64	Y-	A1/46	-2,69
194	A1/1	-3,24	195	A1/1	-3,63	196	A1/1	-3,50	197	A1/1	-3,17
	A1/2	-3,16		A1/2	-3,55		A1/2	-3,42		A1/2	-3,10
	A1/3	-3,23		A1/3	-3,61		A1/3	-3,49		A1/3	-3,16
	A1/4	-3,15		A1/4	-3,53		A1/4	-3,42		A1/4	-3,10
	A1/5	-3,10		A1/5	-3,47		A1/5	-3,37		A1/5	-3,05
	A1/6	-3,22		A1/6	-3,60		A1/6	-3,50		A1/6	-3,16
	A1/7	-3,14		A1/7	-3,53		A1/7	-3,42		A1/7	-3,09
	A1/8	-3,10		A1/8	-3,46		A1/8	-3,37		A1/8	-3,05
	A1/9	-3,25		A1/9	-3,64		A1/9	-3,50		A1/9	-3,18
	A1/10	-3,17		A1/10	-3,57		A1/10	-3,42		A1/10	-3,11
	A1/11	-3,13		A1/11	-3,53		A1/11	-3,38		A1/11	-3,08
	A1/12	-3,25		A1/12	-3,65		A1/12	-3,50		A1/12	-3,18
	A1/13	-3,17		A1/13	-3,58		A1/13	-3,42		A1/13	-3,12
	A1/14	-3,14		A1/14	-3,55		A1/14	-3,38		A1/14	-3,09
X+	A1/21	-2,11	X+	A1/21	-2,33	X+	A1/20	-2,33	X+	A1/20	-2,10
X-	A1/30	-2,32	X-	A1/30	-2,72	X-	A1/27	-2,41	X-	A1/27	-2,28
Y+	A1/40	-2,11	Y+	A1/40	-2,33	Y+	A1/41	-2,38	Y+	A1/41	-2,11

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SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	Y- A1/46	-2,31		Y- A1/46	-2,72		Y- A1/43	-2,39		Y- A1/43	-2,28
198	A1/1	-2,94	199	A1/1	-2,91	200	A1/1	-2,51	201	A1/1	-2,88
	A1/2	-2,86		A1/2	-2,83		A1/2	-2,43		A1/2	-2,81
	A1/3	-2,94		A1/3	-2,91		A1/3	-2,51		A1/3	-2,88
	A1/4	-2,86		A1/4	-2,83		A1/4	-2,43		A1/4	-2,80
	A1/5	-2,82		A1/5	-2,79		A1/5	-2,39		A1/5	-2,76
	A1/6	-2,94		A1/6	-2,92		A1/6	-2,51		A1/6	-2,88
	A1/7	-2,86		A1/7	-2,84		A1/7	-2,43		A1/7	-2,80
	A1/8	-2,82		A1/8	-2,80		A1/8	-2,40		A1/8	-2,76
	A1/9	-2,95		A1/9	-2,91		A1/9	-2,51		A1/9	-2,89
	A1/10	-2,87		A1/10	-2,83		A1/10	-2,43		A1/10	-2,81
	A1/11	-2,83		A1/11	-2,78		A1/11	-2,39		A1/11	-2,77
	A1/12	-2,94		A1/12	-2,90		A1/12	-2,50		A1/12	-2,89
	A1/13	-2,86		A1/13	-2,82		A1/13	-2,43		A1/13	-2,81
	A1/14	-2,83		A1/14	-2,77		A1/14	-2,39		A1/14	-2,77
	X+ A1/21	-1,94		X+ A1/18	-1,97		X+ A1/18	-1,63		X+ A1/21	-1,87
	X- A1/30	-2,00		X- A1/25	-1,92		X- A1/25	-1,67		X- A1/30	-1,98
	Y+ A1/40	-1,96		Y+ A1/34	-1,99		Y+ A1/41	-1,67		Y+ A1/40	-1,90
	Y- A1/46	-1,99		Y- A1/36	-1,88		Y- A1/43	-1,63		Y- A1/46	-1,97
202	A1/1	-3,37	203	A1/1	-2,57	204	A1/1	-4,10	205	A1/1	-4,58
	A1/2	-3,30		A1/2	-2,49		A1/2	-4,02		A1/2	-4,50
	A1/3	-3,36		A1/3	-2,57		A1/3	-4,10		A1/3	-4,57
	A1/4	-3,29		A1/4	-2,49		A1/4	-4,02		A1/4	-4,49
	A1/5	-3,23		A1/5	-2,44		A1/5	-3,96		A1/5	-4,41
	A1/6	-3,36		A1/6	-2,57		A1/6	-4,07		A1/6	-4,53
	A1/7	-3,29		A1/7	-2,50		A1/7	-3,99		A1/7	-4,46
	A1/8	-3,23		A1/8	-2,45		A1/8	-3,91		A1/8	-4,35
	A1/9	-3,38		A1/9	-2,57		A1/9	-4,10		A1/9	-4,59
	A1/10	-3,31		A1/10	-2,49		A1/10	-4,03		A1/10	-4,52
	A1/11	-3,27		A1/11	-2,44		A1/11	-3,96		A1/11	-4,45
	A1/12	-3,38		A1/12	-2,56		A1/12	-4,13		A1/12	-4,63
	A1/13	-3,31		A1/13	-2,48		A1/13	-4,05		A1/13	-4,55
	A1/14	-3,27		A1/14	-2,43		A1/14	-4,01		A1/14	-4,51
	X+ A1/21	-2,17		X+ A1/18	-1,68		X+ A1/21	-2,83		X+ A1/21	-3,09
	X- A1/30	-2,41		X- A1/25	-1,67		X- A1/30	-2,88		X- A1/30	-3,34
	Y+ A1/40	-2,21		Y+ A1/34	-1,71		Y+ A1/40	-2,55		Y+ A1/40	-2,80
	Y- A1/46	-2,39		Y- A1/36	-1,61		Y- A1/46	-3,03		Y- A1/46	-3,50
206	A1/1	-3,65	207	A1/1	-3,17	208	A1/1	-3,03	209	A1/1	-2,73
	A1/2	-3,58		A1/2	-3,09		A1/2	-2,95		A1/2	-2,65
	A1/3	-3,66		A1/3	-3,18		A1/3	-3,04		A1/3	-2,74
	A1/4	-3,58		A1/4	-3,10		A1/4	-2,96		A1/4	-2,66
	A1/5	-3,53		A1/5	-3,06		A1/5	-2,92		A1/5	-2,63
	A1/6	-3,64		A1/6	-3,17		A1/6	-3,04		A1/6	-2,74
	A1/7	-3,57		A1/7	-3,09		A1/7	-2,96		A1/7	-2,66
	A1/8	-3,51		A1/8	-3,04		A1/8	-2,92		A1/8	-2,63
	A1/9	-3,65		A1/9	-3,17		A1/9	-3,02		A1/9	-2,73
	A1/10	-3,57		A1/10	-3,09		A1/10	-2,94		A1/10	-2,65
	A1/11	-3,52		A1/11	-3,05		A1/11	-2,90		A1/11	-2,61
	A1/12	-3,66		A1/12	-3,18		A1/12	-3,02		A1/12	-2,73
	A1/13	-3,59		A1/13	-3,10		A1/13	-2,94		A1/13	-2,65
	A1/14	-3,54		A1/14	-3,06		A1/14	-2,89		A1/14	-2,61
	X+ A1/21	-2,51		X+ A1/21	-2,18		X+ A1/15	-2,12		X+ A1/15	-1,89
	X- A1/30	-2,47		X- A1/30	-2,12		X- A1/24	-1,96		X- A1/24	-1,77
	Y+ A1/31	-2,40		Y+ A1/31	-2,10		Y+ A1/31	-2,11		Y+ A1/31	-1,88
	Y- A1/37	-2,55		Y- A1/37	-2,19		Y- A1/37	-1,98		Y- A1/37	-1,80
210	A1/1	-3,00	211	A1/1	-2,53	212	A1/1	-2,74	213	A1/1	-2,61
	A1/2	-2,92		A1/2	-2,45		A1/2	-2,66		A1/2	-2,53
	A1/3	-3,00		A1/3	-2,53		A1/3	-2,75		A1/3	-2,61
	A1/4	-2,92		A1/4	-2,45		A1/4	-2,67		A1/4	-2,53
	A1/5	-2,88		A1/5	-2,42		A1/5	-2,63		A1/5	-2,50
	A1/6	-2,99		A1/6	-2,53		A1/6	-2,75		A1/6	-2,62
	A1/7	-2,91		A1/7	-2,45		A1/7	-2,67		A1/7	-2,53
	A1/8	-2,87		A1/8	-2,42		A1/8	-2,64		A1/8	-2,50
	A1/9	-2,99		A1/9	-2,53		A1/9	-2,73		A1/9	-2,60
	A1/10	-2,91		A1/10	-2,44		A1/10	-2,65		A1/10	-2,52
	A1/11	-2,87		A1/11	-2,41		A1/11	-2,61		A1/11	-2,48
	A1/12	-3,00		A1/12	-2,53		A1/12	-2,73		A1/12	-2,60
	A1/13	-2,92		A1/13	-2,44		A1/13	-2,65		A1/13	-2,52
	A1/14	-2,88		A1/14	-2,41		A1/14	-2,60		A1/14	-2,48
	X+ A1/21	-2,04		X+ A1/15	-1,71		X+ A1/15	-1,91		X+ A1/15	-1,79
	X- A1/30	-1,99		X- A1/24	-1,66		X- A1/24	-1,75		X- A1/24	-1,68
	Y+ A1/31	-1,99		Y+ A1/31	-1,71		Y+ A1/31	-1,91		Y+ A1/31	-1,79
	Y- A1/37	-2,04		Y- A1/37	-1,66		Y- A1/37	-1,74		Y- A1/37	-1,67
214	A1/1	-2,60	215	A1/1	-2,52	216	A1/1	-2,50	217	A1/1	-2,54
	A1/2	-2,52		A1/2	-2,45		A1/2	-2,41		A1/2	-2,46
	A1/3	-2,61		A1/3	-2,53		A1/3	-2,50		A1/3	-2,54
	A1/4	-2,53		A1/4	-2,45		A1/4	-2,42		A1/4	-2,46

Studio Tecnico Ing. Antonino Tricoli

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/5	-2,48		A1/5	-2,41		A1/5	-2,38		A1/5	-2,42
	A1/6	-2,61		A1/6	-2,53		A1/6	-2,50		A1/6	-2,54
	A1/7	-2,53		A1/7	-2,45		A1/7	-2,42		A1/7	-2,47
	A1/8	-2,48		A1/8	-2,41		A1/8	-2,39		A1/8	-2,43
	A1/9	-2,59		A1/9	-2,52		A1/9	-2,49		A1/9	-2,54
	A1/10	-2,52		A1/10	-2,44		A1/10	-2,41		A1/10	-2,47
	A1/11	-2,46		A1/11	-2,40		A1/11	-2,38		A1/11	-2,42
	A1/12	-2,59		A1/12	-2,52		A1/12	-2,49		A1/12	-2,54
	A1/13	-2,52		A1/13	-2,44		A1/13	-2,41		A1/13	-2,46
	A1/14	-2,46		A1/14	-2,39		A1/14	-2,37		A1/14	-2,42
X+	A1/15	-1,76	X+	A1/15	-1,69	X+	A1/18	-1,67	X+	A1/18	-1,65
X-	A1/24	-1,63	X-	A1/24	-1,62	X-	A1/25	-1,63	X-	A1/25	-1,68
Y+	A1/31	-1,76	Y+	A1/31	-1,70	Y+	A1/34	-1,67	Y+	A1/41	-1,68
Y-	A1/37	-1,64	Y-	A1/37	-1,60	Y-	A1/36	-1,61	Y-	A1/43	-1,64
218	A1/1	-3,16	219	A1/1	-2,84	220	A1/1	-2,60	221	A1/1	-2,85
	A1/2	-3,07		A1/2	-2,75		A1/2	-2,51		A1/2	-2,76
	A1/3	-3,15		A1/3	-2,84		A1/3	-2,59		A1/3	-2,84
	A1/4	-3,07		A1/4	-2,75		A1/4	-2,51		A1/4	-2,76
	A1/5	-3,01		A1/5	-2,70		A1/5	-2,47		A1/5	-2,71
	A1/6	-3,16		A1/6	-2,85		A1/6	-2,60		A1/6	-2,85
	A1/7	-3,07		A1/7	-2,76		A1/7	-2,52		A1/7	-2,77
	A1/8	-3,02		A1/8	-2,71		A1/8	-2,48		A1/8	-2,73
	A1/9	-3,16		A1/9	-2,85		A1/9	-2,60		A1/9	-2,85
	A1/10	-3,08		A1/10	-2,76		A1/10	-2,52		A1/10	-2,77
	A1/11	-3,03		A1/11	-2,71		A1/11	-2,48		A1/11	-2,73
	A1/12	-3,16		A1/12	-2,84		A1/12	-2,59		A1/12	-2,84
	A1/13	-3,07		A1/13	-2,75		A1/13	-2,51		A1/13	-2,76
	A1/14	-3,02		A1/14	-2,70		A1/14	-2,47		A1/14	-2,72
X+	A1/18	-2,04	X+	A1/18	-1,82	X+	A1/18	-1,66	X+	A1/18	-1,85
X-	A1/25	-2,14	X-	A1/25	-1,89	X-	A1/25	-1,74	X-	A1/25	-1,94
Y+	A1/41	-2,11	Y+	A1/41	-1,88	Y+	A1/41	-1,73	Y+	A1/41	-1,93
Y-	A1/43	-2,10	Y-	A1/43	-1,83	Y-	A1/43	-1,67	Y-	A1/43	-1,87
222	A1/1	-3,56	223	A1/1	-3,37	224	A1/1	-3,26	225	A1/1	-2,47
	A1/2	-3,48		A1/2	-3,29		A1/2	-3,19		A1/2	-2,40
	A1/3	-3,55		A1/3	-3,37		A1/3	-3,25		A1/3	-2,47
	A1/4	-3,47		A1/4	-3,29		A1/4	-3,18		A1/4	-2,40
	A1/5	-3,41		A1/5	-3,23		A1/5	-3,13		A1/5	-2,36
	A1/6	-3,56		A1/6	-3,38		A1/6	-3,27		A1/6	-2,48
	A1/7	-3,48		A1/7	-3,30		A1/7	-3,20		A1/7	-2,41
	A1/8	-3,42		A1/8	-3,25		A1/8	-3,16		A1/8	-2,38
	A1/9	-3,57		A1/9	-3,38		A1/9	-3,27		A1/9	-2,48
	A1/10	-3,49		A1/10	-3,30		A1/10	-3,20		A1/10	-2,41
	A1/11	-3,44		A1/11	-3,25		A1/11	-3,15		A1/11	-2,37
	A1/12	-3,56		A1/12	-3,37		A1/12	-3,25		A1/12	-2,47
	A1/13	-3,48		A1/13	-3,29		A1/13	-3,18		A1/13	-2,40
	A1/14	-3,43		A1/14	-3,24		A1/14	-3,12		A1/14	-2,36
X+	A1/20	-2,30	X+	A1/18	-2,19	X+	A1/18	-2,15	X+	A1/18	-1,63
X-	A1/27	-2,47	X-	A1/25	-2,34	X-	A1/25	-2,29	X-	A1/25	-1,70
Y+	A1/41	-2,39	Y+	A1/41	-2,31	Y+	A1/41	-2,31	Y+	A1/41	-1,71
Y-	A1/43	-2,42	Y-	A1/43	-2,25	Y-	A1/43	-2,13	Y-	A1/43	-1,61
226	A1/1	-2,19	227	A1/1	-2,68	228	A1/1	-2,38	229	A1/1	-2,88
	A1/2	-2,12		A1/2	-2,60		A1/2	-2,30		A1/2	-2,79
	A1/3	-2,19		A1/3	-2,68		A1/3	-2,37		A1/3	-2,88
	A1/4	-2,12		A1/4	-2,59		A1/4	-2,30		A1/4	-2,78
	A1/5	-2,08		A1/5	-2,54		A1/5	-2,25		A1/5	-2,72
	A1/6	-2,20		A1/6	-2,69		A1/6	-2,38		A1/6	-2,88
	A1/7	-2,13		A1/7	-2,60		A1/7	-2,31		A1/7	-2,79
	A1/8	-2,10		A1/8	-2,55		A1/8	-2,26		A1/8	-2,74
	A1/9	-2,20		A1/9	-2,69		A1/9	-2,38		A1/9	-2,88
	A1/10	-2,13		A1/10	-2,60		A1/10	-2,31		A1/10	-2,79
	A1/11	-2,10		A1/11	-2,55		A1/11	-2,26		A1/11	-2,73
	A1/12	-2,19		A1/12	-2,68		A1/12	-2,37		A1/12	-2,87
	A1/13	-2,12		A1/13	-2,59		A1/13	-2,30		A1/13	-2,78
	A1/14	-2,08		A1/14	-2,54		A1/14	-2,25		A1/14	-2,72
X+	A1/18	-1,40	X+	A1/18	-1,70	X+	A1/18	-1,49	X+	A1/18	-1,83
X-	A1/25	-1,48	X-	A1/25	-1,75	X-	A1/25	-1,58	X-	A1/25	-1,88
Y+	A1/41	-1,48	Y+	A1/41	-1,76	Y+	A1/41	-1,57	Y+	A1/41	-1,89
Y-	A1/43	-1,41	Y-	A1/43	-1,70	Y-	A1/43	-1,51	Y-	A1/43	-1,80
230	A1/1	-2,92	231	A1/1	-3,29	232	A1/1	-3,14	233	A1/1	-3,11
	A1/2	-2,83		A1/2	-3,20		A1/2	-3,05		A1/2	-3,02
	A1/3	-2,92		A1/3	-3,29		A1/3	-3,13		A1/3	-3,10
	A1/4	-2,83		A1/4	-3,19		A1/4	-3,05		A1/4	-3,02
	A1/5	-2,77		A1/5	-3,13		A1/5	-2,99		A1/5	-2,96
	A1/6	-2,92		A1/6	-3,29		A1/6	-3,14		A1/6	-3,11
	A1/7	-2,83		A1/7	-3,20		A1/7	-3,05		A1/7	-3,03
	A1/8	-2,78		A1/8	-3,13		A1/8	-3,00		A1/8	-2,97
	A1/9	-2,92		A1/9	-3,29		A1/9	-3,14		A1/9	-3,11
	A1/10	-2,83		A1/10	-3,20		A1/10	-3,06		A1/10	-3,03

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/11	-2,78		A1/11	-3,13		A1/11	-3,00		A1/11	-2,97
	A1/12	-2,91		A1/12	-3,29		A1/12	-3,14		A1/12	-3,11
	A1/13	-2,83		A1/13	-3,19		A1/13	-3,05		A1/13	-3,02
	A1/14	-2,77		A1/14	-3,12		A1/14	-2,99		A1/14	-2,97
X+	A1/18	-1,88	X+	A1/18	-2,13	X+	A1/18	-2,02	X+	A1/18	-2,00
X-	A1/25	-1,90	X-	A1/25	-2,14	X-	A1/25	-2,10	X-	A1/25	-2,07
Y+	A1/41	-1,91	Y+	A1/41	-2,15	Y+	A1/41	-2,08	Y+	A1/41	-2,05
Y-	A1/43	-1,87	Y-	A1/43	-2,10	Y-	A1/43	-2,05	Y-	A1/43	-2,04
234	A1/1	-3,13	235	A1/1	-2,82	236	A1/1	-2,51	237	A1/1	-2,56
	A1/2	-3,04		A1/2	-2,74		A1/2	-2,44		A1/2	-2,48
	A1/3	-3,13		A1/3	-2,82		A1/3	-2,51		A1/3	-2,56
	A1/4	-3,04		A1/4	-2,74		A1/4	-2,44		A1/4	-2,48
	A1/5	-2,97		A1/5	-2,67		A1/5	-2,39		A1/5	-2,43
	A1/6	-3,13		A1/6	-2,82		A1/6	-2,51		A1/6	-2,56
	A1/7	-3,04		A1/7	-2,74		A1/7	-2,44		A1/7	-2,49
	A1/8	-2,97		A1/8	-2,68		A1/8	-2,39		A1/8	-2,43
	A1/9	-3,13		A1/9	-2,82		A1/9	-2,51		A1/9	-2,56
	A1/10	-3,03		A1/10	-2,74		A1/10	-2,44		A1/10	-2,48
	A1/11	-2,96		A1/11	-2,68		A1/11	-2,39		A1/11	-2,42
	A1/12	-3,12		A1/12	-2,82		A1/12	-2,51		A1/12	-2,56
	A1/13	-3,03		A1/13	-2,74		A1/13	-2,44		A1/13	-2,48
	A1/14	-2,96		A1/14	-2,67		A1/14	-2,38		A1/14	-2,42
X+	A1/18	-2,03	X+	A1/18	-1,80	X+	A1/18	-1,61	X+	A1/18	-1,64
X-	A1/25	-1,99	X-	A1/25	-1,81	X-	A1/25	-1,64	X-	A1/25	-1,63
Y+	A1/34	-2,04	Y+	A1/41	-1,83	Y+	A1/41	-1,64	Y+	A1/34	-1,66
Y-	A1/36	-1,96	Y-	A1/43	-1,78	Y-	A1/43	-1,61	Y-	A1/36	-1,61
238	A1/1	-2,63	239	A1/1	-3,75	240	A1/1	-2,36	241	A1/1	-2,37
	A1/2	-2,56		A1/2	-3,67		A1/2	-2,31		A1/2	-2,31
	A1/3	-2,63		A1/3	-3,75		A1/3	-2,36		A1/3	-2,37
	A1/4	-2,56		A1/4	-3,67		A1/4	-2,31		A1/4	-2,31
	A1/5	-2,51		A1/5	-3,61		A1/5	-2,27		A1/5	-2,27
	A1/6	-2,63		A1/6	-3,73		A1/6	-2,35		A1/6	-2,37
	A1/7	-2,56		A1/7	-3,65		A1/7	-2,30		A1/7	-2,31
	A1/8	-2,51		A1/8	-3,58		A1/8	-2,26		A1/8	-2,27
	A1/9	-2,64		A1/9	-3,75		A1/9	-2,36		A1/9	-2,37
	A1/10	-2,57		A1/10	-3,67		A1/10	-2,31		A1/10	-2,31
	A1/11	-2,52		A1/11	-3,61		A1/11	-2,27		A1/11	-2,27
	A1/12	-2,63		A1/12	-3,76		A1/12	-2,36		A1/12	-2,37
	A1/13	-2,56		A1/13	-3,68		A1/13	-2,31		A1/13	-2,31
	A1/14	-2,51		A1/14	-3,64		A1/14	-2,28		A1/14	-2,27
X+	A1/18	-1,68	X+	A1/21	-2,56	X+	A1/21	-1,59	X+	A1/21	-1,58
X-	A1/25	-1,76	X-	A1/30	-2,57	X-	A1/30	-1,59	X-	A1/30	-1,58
Y+	A1/41	-1,73	Y+	A1/40	-2,39	Y+	A1/40	-1,53	Y+	A1/31	-1,58
Y-	A1/43	-1,73	Y-	A1/46	-2,66	Y-	A1/46	-1,62	Y-	A1/37	-1,58
242	A1/1	-1,76	243	A1/1	-1,82	244	A1/1	-1,65	245	A1/1	-3,14
	A1/2	-1,70		A1/2	-1,76		A1/2	-1,60		A1/2	-3,05
	A1/3	-1,76		A1/3	-1,82		A1/3	-1,65		A1/3	-3,14
	A1/4	-1,70		A1/4	-1,76		A1/4	-1,60		A1/4	-3,05
	A1/5	-1,68		A1/5	-1,73		A1/5	-1,57		A1/5	-3,01
	A1/6	-1,76		A1/6	-1,82		A1/6	-1,65		A1/6	-3,13
	A1/7	-1,70		A1/7	-1,76		A1/7	-1,60		A1/7	-3,05
	A1/8	-1,68		A1/8	-1,73		A1/8	-1,57		A1/8	-3,00
	A1/9	-1,76		A1/9	-1,82		A1/9	-1,65		A1/9	-3,13
	A1/10	-1,70		A1/10	-1,76		A1/10	-1,60		A1/10	-3,05
	A1/11	-1,68		A1/11	-1,73		A1/11	-1,58		A1/11	-3,00
	A1/12	-1,75		A1/12	-1,82		A1/12	-1,65		A1/12	-3,14
	A1/13	-1,70		A1/13	-1,76		A1/13	-1,60		A1/13	-3,06
	A1/14	-1,68		A1/14	-1,73		A1/14	-1,57		A1/14	-3,01
X+	A1/18	-1,17	X+	A1/18	-1,19	X+	A1/20	-1,06	X+	A1/21	-2,10
X-	A1/25	-1,17	X-	A1/25	-1,20	X-	A1/27	-1,10	X-	A1/30	-2,08
Y+	A1/34	-1,18	Y+	A1/41	-1,20	Y+	A1/41	-1,08	Y+	A1/31	-2,06
Y-	A1/36	-1,15	Y-	A1/43	-1,20	Y-	A1/43	-1,09	Y-	A1/37	-2,11
246	A1/1	-3,05	247	A1/1	-2,15	248	A1/1	-2,65	249	A1/1	-2,44
	A1/2	-2,98		A1/2	-2,09		A1/2	-2,56		A1/2	-2,35
	A1/3	-3,05		A1/3	-2,15		A1/3	-2,65		A1/3	-2,43
	A1/4	-2,98		A1/4	-2,09		A1/4	-2,56		A1/4	-2,35
	A1/5	-2,93		A1/5	-2,07		A1/5	-2,53		A1/5	-2,33
	A1/6	-3,05		A1/6	-2,16		A1/6	-2,65		A1/6	-2,44
	A1/7	-2,98		A1/7	-2,09		A1/7	-2,56		A1/7	-2,35
	A1/8	-2,93		A1/8	-2,07		A1/8	-2,53		A1/8	-2,33
	A1/9	-3,05		A1/9	-2,15		A1/9	-2,65		A1/9	-2,44
	A1/10	-2,98		A1/10	-2,09		A1/10	-2,56		A1/10	-2,35
	A1/11	-2,93		A1/11	-2,07		A1/11	-2,53		A1/11	-2,33
	A1/12	-3,06		A1/12	-2,15		A1/12	-2,65		A1/12	-2,44
	A1/13	-2,99		A1/13	-2,09		A1/13	-2,56		A1/13	-2,35
	A1/14	-2,94		A1/14	-2,07		A1/14	-2,53		A1/14	-2,33
X+	A1/21	-2,04	X+	A1/18	-1,43	X+	A1/21	-1,76	X+	A1/20	-1,61
X-	A1/30	-2,05	X-	A1/25	-1,44	X-	A1/30	-1,76	X-	A1/27	-1,62

Studio Tecnico Ing. Antonino Tricoli

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	Y+ A1/40	-2,00		Y+ A1/41	-1,44		Y+ A1/31	-1,76		Y+ A1/41	-1,61
	Y- A1/46	-2,07		Y- A1/43	-1,43		Y- A1/37	-1,76		Y- A1/43	-1,62
250	A1/1	-1,85	251	A1/1	-2,87	252	A1/1	-2,68	253	A1/1	-2,73
	A1/2	-1,79		A1/2	-2,79		A1/2	-2,60		A1/2	-2,66
	A1/3	-1,85		A1/3	-2,87		A1/3	-2,68		A1/3	-2,73
	A1/4	-1,79		A1/4	-2,79		A1/4	-2,60		A1/4	-2,67
	A1/5	-1,77		A1/5	-2,75		A1/5	-2,57		A1/5	-2,62
	A1/6	-1,85		A1/6	-2,86		A1/6	-2,68		A1/6	-2,72
	A1/7	-1,79		A1/7	-2,79		A1/7	-2,60		A1/7	-2,66
	A1/8	-1,77		A1/8	-2,74		A1/8	-2,56		A1/8	-2,60
	A1/9	-1,85		A1/9	-2,86		A1/9	-2,68		A1/9	-2,72
	A1/10	-1,79		A1/10	-2,79		A1/10	-2,59		A1/10	-2,66
	A1/11	-1,77		A1/11	-2,74		A1/11	-2,56		A1/11	-2,60
	A1/12	-1,85		A1/12	-2,87		A1/12	-2,68		A1/12	-2,73
	A1/13	-1,78		A1/13	-2,79		A1/13	-2,60		A1/13	-2,67
	A1/14	-1,76		A1/14	-2,75		A1/14	-2,56		A1/14	-2,62
X+	A1/18	-1,22	X+	A1/21	-1,94	X+	A1/21	-1,79	X+	A1/21	-1,87
X-	A1/25	-1,23	X-	A1/30	-1,88	X-	A1/30	-1,76	X-	A1/30	-1,77
Y+	A1/41	-1,24	Y+	A1/31	-1,89	Y+	A1/31	-1,77	Y+	A1/31	-1,79
Y-	A1/43	-1,22	Y-	A1/37	-1,93	Y-	A1/37	-1,79	Y-	A1/37	-1,86
254	A1/1	-2,12	255	A1/1	-2,46	256	A1/1	-2,59	257	A1/1	-2,12
	A1/2	-2,06		A1/2	-2,38		A1/2	-2,51		A1/2	-2,06
	A1/3	-2,13		A1/3	-2,46		A1/3	-2,59		A1/3	-2,12
	A1/4	-2,07		A1/4	-2,38		A1/4	-2,51		A1/4	-2,05
	A1/5	-2,04		A1/5	-2,35		A1/5	-2,47		A1/5	-2,03
	A1/6	-2,12		A1/6	-2,46		A1/6	-2,59		A1/6	-2,12
	A1/7	-2,06		A1/7	-2,38		A1/7	-2,51		A1/7	-2,05
	A1/8	-2,03		A1/8	-2,35		A1/8	-2,47		A1/8	-2,03
	A1/9	-2,12		A1/9	-2,46		A1/9	-2,59		A1/9	-2,12
	A1/10	-2,06		A1/10	-2,38		A1/10	-2,51		A1/10	-2,06
	A1/11	-2,03		A1/11	-2,35		A1/11	-2,48		A1/11	-2,03
	A1/12	-2,12		A1/12	-2,46		A1/12	-2,59		A1/12	-2,12
	A1/13	-2,06		A1/13	-2,38		A1/13	-2,51		A1/13	-2,06
	A1/14	-2,03		A1/14	-2,35		A1/14	-2,48		A1/14	-2,03
X+	A1/21	-1,44	X+	A1/21	-1,63	X+	A1/20	-1,70	X+	A1/20	-1,39
X-	A1/30	-1,38	X-	A1/30	-1,63	X-	A1/27	-1,73	X-	A1/27	-1,41
Y+	A1/31	-1,41	Y+	A1/31	-1,62	Y+	A1/41	-1,70	Y+	A1/41	-1,40
Y-	A1/37	-1,42	Y-	A1/37	-1,64	Y-	A1/43	-1,73	Y-	A1/43	-1,41
258	A1/1	-2,61	259	A1/1	-1,83	260	A1/1	-2,11	261	A1/1	-3,26
	A1/2	-2,53		A1/2	-1,77		A1/2	-2,04		A1/2	-3,17
	A1/3	-2,61		A1/3	-1,83		A1/3	-2,11		A1/3	-3,25
	A1/4	-2,53		A1/4	-1,77		A1/4	-2,04		A1/4	-3,17
	A1/5	-2,50		A1/5	-1,75		A1/5	-2,02		A1/5	-3,11
	A1/6	-2,61		A1/6	-1,83		A1/6	-2,10		A1/6	-3,25
	A1/7	-2,53		A1/7	-1,77		A1/7	-2,04		A1/7	-3,16
	A1/8	-2,49		A1/8	-1,74		A1/8	-2,01		A1/8	-3,10
	A1/9	-2,62		A1/9	-1,83		A1/9	-2,11		A1/9	-3,26
	A1/10	-2,53		A1/10	-1,77		A1/10	-2,04		A1/10	-3,17
	A1/11	-2,50		A1/11	-1,74		A1/11	-2,01		A1/11	-3,12
	A1/12	-2,62		A1/12	-1,83		A1/12	-2,12		A1/12	-3,26
	A1/13	-2,53		A1/13	-1,77		A1/13	-2,05		A1/13	-3,18
	A1/14	-2,50		A1/14	-1,75		A1/14	-2,02		A1/14	-3,13
X+	A1/20	-1,72	X+	A1/21	-1,22	X+	A1/21	-1,41	X+	A1/20	-2,12
X-	A1/27	-1,75	X-	A1/30	-1,20	X-	A1/30	-1,40	X-	A1/27	-2,19
Y+	A1/41	-1,70	Y+	A1/31	-1,20	Y+	A1/31	-1,35	Y+	A1/41	-2,11
Y-	A1/43	-1,76	Y-	A1/37	-1,22	Y-	A1/37	-1,43	Y-	A1/43	-2,20
262	A1/1	-2,77	263	A1/1	-2,21	264	A1/1	-2,19	265	A1/1	-2,57
	A1/2	-2,69		A1/2	-2,15		A1/2	-2,13		A1/2	-2,51
	A1/3	-2,77		A1/3	-2,21		A1/3	-2,19		A1/3	-2,57
	A1/4	-2,69		A1/4	-2,15		A1/4	-2,13		A1/4	-2,50
	A1/5	-2,65		A1/5	-2,11		A1/5	-2,09		A1/5	-2,45
	A1/6	-2,77		A1/6	-2,21		A1/6	-2,18		A1/6	-2,57
	A1/7	-2,69		A1/7	-2,15		A1/7	-2,12		A1/7	-2,51
	A1/8	-2,64		A1/8	-2,11		A1/8	-2,08		A1/8	-2,46
	A1/9	-2,77		A1/9	-2,21		A1/9	-2,19		A1/9	-2,57
	A1/10	-2,70		A1/10	-2,15		A1/10	-2,13		A1/10	-2,51
	A1/11	-2,65		A1/11	-2,11		A1/11	-2,09		A1/11	-2,47
	A1/12	-2,77		A1/12	-2,21		A1/12	-2,19		A1/12	-2,57
	A1/13	-2,70		A1/13	-2,15		A1/13	-2,14		A1/13	-2,51
	A1/14	-2,66		A1/14	-2,12		A1/14	-2,10		A1/14	-2,46
X+	A1/20	-1,82	X+	A1/21	-1,45	X+	A1/20	-1,44	X+	A1/18	-1,66
X-	A1/27	-1,85	X-	A1/30	-1,46	X-	A1/27	-1,46	X-	A1/25	-1,73
Y+	A1/41	-1,80	Y+	A1/40	-1,43	Y+	A1/41	-1,39	Y+	A1/41	-1,71
Y-	A1/43	-1,86	Y-	A1/46	-1,47	Y-	A1/43	-1,48	Y-	A1/43	-1,69
266	A1/1	-2,38	267	A1/1	-1,97	268	A1/1	-3,85	269	A1/1	-3,25
	A1/2	-2,32		A1/2	-1,93		A1/2	-3,76		A1/2	-3,18
	A1/3	-2,38		A1/3	-1,97		A1/3	-3,85		A1/3	-3,25

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/4	-2,32		A1/4	-1,92		A1/4	-3,76		A1/4	-3,17
	A1/5	-2,27		A1/5	-1,88		A1/5	-3,69		A1/5	-3,11
	A1/6	-2,38		A1/6	-1,97		A1/6	-3,85		A1/6	-3,25
	A1/7	-2,32		A1/7	-1,93		A1/7	-3,76		A1/7	-3,18
	A1/8	-2,28		A1/8	-1,89		A1/8	-3,69		A1/8	-3,12
	A1/9	-2,38		A1/9	-1,98		A1/9	-3,85		A1/9	-3,26
	A1/10	-2,33		A1/10	-1,93		A1/10	-3,76		A1/10	-3,18
	A1/11	-2,28		A1/11	-1,89		A1/11	-3,70		A1/11	-3,12
	A1/12	-2,38		A1/12	-1,98		A1/12	-3,85		A1/12	-3,25
	A1/13	-2,32		A1/13	-1,93		A1/13	-3,76		A1/13	-3,18
	A1/14	-2,28		A1/14	-1,89		A1/14	-3,70		A1/14	-3,12
X+	A1/20	-1,54	X+	A1/20	-1,27	X+	A1/20	-2,52	X+	A1/18	-2,12
X-	A1/27	-1,60	X-	A1/27	-1,33	X-	A1/27	-2,58	X-	A1/25	-2,18
Y+	A1/41	-1,57	Y+	A1/41	-1,30	Y+	A1/41	-2,54	Y+	A1/41	-2,16
Y-	A1/43	-1,58	Y-	A1/43	-1,32	Y-	A1/43	-2,57	Y-	A1/43	-2,15
270	A1/1	-3,12	271	A1/1	-3,43	272	A1/1	-3,51	273	A1/1	-2,86
	A1/2	-3,04		A1/2	-3,34		A1/2	-3,43		A1/2	-2,79
	A1/3	-3,11		A1/3	-3,42		A1/3	-3,51		A1/3	-2,86
	A1/4	-3,04		A1/4	-3,34		A1/4	-3,42		A1/4	-2,79
	A1/5	-2,98		A1/5	-3,28		A1/5	-3,36		A1/5	-2,74
	A1/6	-3,12		A1/6	-3,43		A1/6	-3,51		A1/6	-2,86
	A1/7	-3,04		A1/7	-3,34		A1/7	-3,42		A1/7	-2,79
	A1/8	-2,99		A1/8	-3,28		A1/8	-3,36		A1/8	-2,73
	A1/9	-3,12		A1/9	-3,43		A1/9	-3,51		A1/9	-2,86
	A1/10	-3,05		A1/10	-3,35		A1/10	-3,43		A1/10	-2,79
	A1/11	-2,99		A1/11	-3,29		A1/11	-3,37		A1/11	-2,74
	A1/12	-3,12		A1/12	-3,43		A1/12	-3,51		A1/12	-2,86
	A1/13	-3,04		A1/13	-3,34		A1/13	-3,43		A1/13	-2,79
	A1/14	-2,99		A1/14	-3,29		A1/14	-3,37		A1/14	-2,74
X+	A1/20	-2,04	X+	A1/20	-2,24	X+	A1/20	-2,29	X+	A1/20	-1,89
X-	A1/27	-2,09	X-	A1/27	-2,29	X-	A1/27	-2,36	X-	A1/27	-1,88
Y+	A1/41	-2,06	Y+	A1/41	-2,27	Y+	A1/41	-2,31	Y+	A1/34	-1,87
Y-	A1/43	-2,08	Y-	A1/43	-2,28	Y-	A1/43	-2,35	Y-	A1/36	-1,89
274	A1/1	-2,73	275	A1/1	-3,45	276	A1/1	-1,97	277	A1/1	-2,90
	A1/2	-2,67		A1/2	-3,37		A1/2	-1,92		A1/2	-2,84
	A1/3	-2,73		A1/3	-3,45		A1/3	-1,97		A1/3	-2,90
	A1/4	-2,67		A1/4	-3,36		A1/4	-1,92		A1/4	-2,83
	A1/5	-2,62		A1/5	-3,30		A1/5	-1,88		A1/5	-2,78
	A1/6	-2,73		A1/6	-3,45		A1/6	-1,97		A1/6	-2,91
	A1/7	-2,67		A1/7	-3,37		A1/7	-1,92		A1/7	-2,84
	A1/8	-2,62		A1/8	-3,31		A1/8	-1,88		A1/8	-2,79
	A1/9	-2,73		A1/9	-3,45		A1/9	-1,97		A1/9	-2,91
	A1/10	-2,67		A1/10	-3,37		A1/10	-1,92		A1/10	-2,84
	A1/11	-2,62		A1/11	-3,31		A1/11	-1,89		A1/11	-2,79
	A1/12	-2,73		A1/12	-3,45		A1/12	-1,97		A1/12	-2,90
	A1/13	-2,67		A1/13	-3,37		A1/13	-1,92		A1/13	-2,83
	A1/14	-2,62		A1/14	-3,31		A1/14	-1,89		A1/14	-2,78
X+	A1/21	-1,82	X+	A1/20	-2,26	X+	A1/21	-1,29	X+	A1/18	-1,91
X-	A1/30	-1,79	X-	A1/27	-2,30	X-	A1/30	-1,31	X-	A1/25	-1,94
Y+	A1/31	-1,81	Y+	A1/41	-2,28	Y+	A1/40	-1,29	Y+	A1/41	-1,93
Y-	A1/37	-1,81	Y-	A1/43	-2,29	Y-	A1/46	-1,31	Y-	A1/43	-1,92
278	A1/1	-2,48	279	A1/1	-2,93	280	A1/1	-1,73	281	A1/1	-1,76
	A1/2	-2,42		A1/2	-2,87		A1/2	-1,68		A1/2	-1,70
	A1/3	-2,48		A1/3	-2,93		A1/3	-1,73		A1/3	-1,76
	A1/4	-2,42		A1/4	-2,86		A1/4	-1,67		A1/4	-1,70
	A1/5	-2,37		A1/5	-2,81		A1/5	-1,64		A1/5	-1,67
	A1/6	-2,48		A1/6	-2,94		A1/6	-1,74		A1/6	-1,76
	A1/7	-2,42		A1/7	-2,87		A1/7	-1,68		A1/7	-1,71
	A1/8	-2,38		A1/8	-2,82		A1/8	-1,65		A1/8	-1,68
	A1/9	-2,48		A1/9	-2,94		A1/9	-1,74		A1/9	-1,76
	A1/10	-2,42		A1/10	-2,87		A1/10	-1,68		A1/10	-1,70
	A1/11	-2,37		A1/11	-2,82		A1/11	-1,65		A1/11	-1,68
	A1/12	-2,48		A1/12	-2,93		A1/12	-1,73		A1/12	-1,75
	A1/13	-2,42		A1/13	-2,86		A1/13	-1,67		A1/13	-1,70
	A1/14	-2,37		A1/14	-2,81		A1/14	-1,64		A1/14	-1,67
X+	A1/15	-1,64	X+	A1/18	-1,91	X+	A1/18	-1,08	X+	A1/18	-1,13
X-	A1/24	-1,64	X-	A1/25	-1,97	X-	A1/25	-1,16	X-	A1/25	-1,19
Y+	A1/40	-1,65	Y+	A1/41	-1,96	Y+	A1/41	-1,16	Y+	A1/41	-1,19
Y-	A1/46	-1,62	Y-	A1/43	-1,93	Y-	A1/43	-1,10	Y-	A1/43	-1,13
282	A1/1	-2,19	283	A1/1	-2,55	284	A1/1	-3,94	285	A1/1	-3,17
	A1/2	-2,11		A1/2	-2,47		A1/2	-3,86		A1/2	-3,07
	A1/3	-2,19		A1/3	-2,55		A1/3	-3,93		A1/3	-3,16
	A1/4	-2,11		A1/4	-2,47		A1/4	-3,85		A1/4	-3,07
	A1/5	-2,08		A1/5	-2,42		A1/5	-3,79		A1/5	-3,03
	A1/6	-2,19		A1/6	-2,56		A1/6	-3,97		A1/6	-3,18
	A1/7	-2,12		A1/7	-2,47		A1/7	-3,88		A1/7	-3,08
	A1/8	-2,09		A1/8	-2,43		A1/8	-3,84		A1/8	-3,05
	A1/9	-2,19		A1/9	-2,56		A1/9	-3,95		A1/9	-3,17

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/10	-2,12		A1/10	-2,47		A1/10	-3,87		A1/10	-3,08
	A1/11	-2,09		A1/11	-2,43		A1/11	-3,82		A1/11	-3,04
	A1/12	-2,19		A1/12	-2,55		A1/12	-3,92		A1/12	-3,16
	A1/13	-2,11		A1/13	-2,46		A1/13	-3,83		A1/13	-3,06
	A1/14	-2,08		A1/14	-2,42		A1/14	-3,76		A1/14	-3,02
X+	A1/18	-1,42	X+	A1/18	-1,64	X+	A1/18	-2,64	X+	A1/18	-2,11
X-	A1/25	-1,47	X-	A1/25	-1,68	X-	A1/25	-2,85	X-	A1/25	-2,19
Y+	A1/41	-1,48	Y+	A1/41	-1,70	Y+	A1/41	-2,92	Y+	A1/41	-2,22
Y-	A1/43	-1,41	Y-	A1/43	-1,62	Y-	A1/43	-2,52	Y-	A1/43	-2,05
286	A1/1	-2,64	287	A1/1	-3,44	288	A1/1	-3,77	289	A1/1	-2,95
	A1/2	-2,55		A1/2	-3,37		A1/2	-3,69		A1/2	-2,87
	A1/3	-2,63		A1/3	-3,43		A1/3	-3,75		A1/3	-2,95
	A1/4	-2,55		A1/4	-3,35		A1/4	-3,67		A1/4	-2,87
	A1/5	-2,52		A1/5	-3,31		A1/5	-3,62		A1/5	-2,83
	A1/6	-2,64		A1/6	-3,46		A1/6	-3,79		A1/6	-2,96
	A1/7	-2,56		A1/7	-3,39		A1/7	-3,71		A1/7	-2,88
	A1/8	-2,54		A1/8	-3,36		A1/8	-3,68		A1/8	-2,86
	A1/9	-2,64		A1/9	-3,45		A1/9	-3,78		A1/9	-2,96
	A1/10	-2,56		A1/10	-3,38		A1/10	-3,71		A1/10	-2,88
	A1/11	-2,53		A1/11	-3,34		A1/11	-3,67		A1/11	-2,85
	A1/12	-2,63		A1/12	-3,42		A1/12	-3,75		A1/12	-2,95
	A1/13	-2,54		A1/13	-3,35		A1/13	-3,67		A1/13	-2,86
	A1/14	-2,52		A1/14	-3,29		A1/14	-3,61		A1/14	-2,83
X+	A1/18	-1,75	X+	A1/18	-2,28	X+	A1/18	-2,45	X+	A1/18	-1,96
X-	A1/25	-1,83	X-	A1/25	-2,51	X-	A1/25	-2,80	X-	A1/25	-2,08
Y+	A1/41	-1,84	Y+	A1/41	-2,55	Y+	A1/41	-2,79	Y+	A1/41	-2,08
Y-	A1/43	-1,72	Y-	A1/43	-2,22	Y-	A1/43	-2,47	Y-	A1/43	-1,95
290	A1/1	-2,34	291	A1/1	-2,64	292	A1/1	-2,52	293	A1/1	-2,80
	A1/2	-2,26		A1/2	-2,55		A1/2	-2,44		A1/2	-2,71
	A1/3	-2,34		A1/3	-2,64		A1/3	-2,53		A1/3	-2,80
	A1/4	-2,26		A1/4	-2,55		A1/4	-2,44		A1/4	-2,71
	A1/5	-2,23		A1/5	-2,53		A1/5	-2,41		A1/5	-2,68
	A1/6	-2,34		A1/6	-2,64		A1/6	-2,53		A1/6	-2,79
	A1/7	-2,26		A1/7	-2,55		A1/7	-2,44		A1/7	-2,71
	A1/8	-2,24		A1/8	-2,53		A1/8	-2,40		A1/8	-2,66
	A1/9	-2,34		A1/9	-2,64		A1/9	-2,52		A1/9	-2,79
	A1/10	-2,26		A1/10	-2,55		A1/10	-2,44		A1/10	-2,71
	A1/11	-2,23		A1/11	-2,53		A1/11	-2,40		A1/11	-2,67
	A1/12	-2,34		A1/12	-2,64		A1/12	-2,52		A1/12	-2,80
	A1/13	-2,25		A1/13	-2,55		A1/13	-2,44		A1/13	-2,72
	A1/14	-2,23		A1/14	-2,53		A1/14	-2,40		A1/14	-2,68
X+	A1/18	-1,55	X+	A1/18	-1,76	X+	A1/18	-1,66	X+	A1/21	-1,88
X-	A1/25	-1,55	X-	A1/25	-1,76	X-	A1/25	-1,64	X-	A1/30	-1,83
Y+	A1/41	-1,56	Y+	A1/41	-1,76	Y+	A1/34	-1,66	Y+	A1/31	-1,81
Y-	A1/43	-1,53	Y-	A1/43	-1,76	Y-	A1/36	-1,65	Y-	A1/37	-1,89
294	A1/1	-3,26	295	A1/1	-3,69	296	A1/1	-5,05	297	A1/1	-1,74
	A1/2	-3,18		A1/2	-3,62		A1/2	-4,97		A1/2	-1,69
	A1/3	-3,26		A1/3	-3,68		A1/3	-5,02		A1/3	-1,74
	A1/4	-3,18		A1/4	-3,61		A1/4	-4,94		A1/4	-1,69
	A1/5	-3,14		A1/5	-3,55		A1/5	-4,85		A1/5	-1,65
	A1/6	-3,26		A1/6	-3,70		A1/6	-5,08		A1/6	-1,74
	A1/7	-3,18		A1/7	-3,63		A1/7	-5,00		A1/7	-1,69
	A1/8	-3,14		A1/8	-3,59		A1/8	-4,95		A1/8	-1,66
	A1/9	-3,26		A1/9	-3,70		A1/9	-5,08		A1/9	-1,74
	A1/10	-3,18		A1/10	-3,62		A1/10	-5,00		A1/10	-1,69
	A1/11	-3,14		A1/11	-3,58		A1/11	-4,94		A1/11	-1,65
	A1/12	-3,26		A1/12	-3,68		A1/12	-5,02		A1/12	-1,74
	A1/13	-3,18		A1/13	-3,60		A1/13	-4,94		A1/13	-1,69
	A1/14	-3,14		A1/14	-3,54		A1/14	-4,84		A1/14	-1,64
X+	A1/18	-2,17	X+	A1/18	-2,46	X+	A1/18	-3,24	X+	A1/18	-1,13
X-	A1/25	-2,22	X-	A1/25	-2,65	X-	A1/25	-3,84	X-	A1/25	-1,11
Y+	A1/41	-2,21	Y+	A1/41	-2,66	Y+	A1/41	-3,81	Y+	A1/34	-1,14
Y-	A1/43	-2,20	Y-	A1/43	-2,44	Y-	A1/43	-3,30	Y-	A1/36	-1,09
298	A1/1	-2,00	299	A1/1	-2,71	300	A1/1	-2,73	301	A1/1	-2,08
	A1/2	-1,95		A1/2	-2,63		A1/2	-2,64		A1/2	-2,02
	A1/3	-2,00		A1/3	-2,71		A1/3	-2,73		A1/3	-2,08
	A1/4	-1,95		A1/4	-2,63		A1/4	-2,64		A1/4	-2,02
	A1/5	-1,91		A1/5	-2,58		A1/5	-2,59		A1/5	-1,98
	A1/6	-2,01		A1/6	-2,71		A1/6	-2,73		A1/6	-2,08
	A1/7	-1,95		A1/7	-2,63		A1/7	-2,65		A1/7	-2,02
	A1/8	-1,91		A1/8	-2,58		A1/8	-2,60		A1/8	-1,98
	A1/9	-2,01		A1/9	-2,71		A1/9	-2,73		A1/9	-2,08
	A1/10	-1,95		A1/10	-2,63		A1/10	-2,64		A1/10	-2,03
	A1/11	-1,91		A1/11	-2,58		A1/11	-2,59		A1/11	-1,99
	A1/12	-2,00		A1/12	-2,71		A1/12	-2,72		A1/12	-2,08
	A1/13	-1,95		A1/13	-2,62		A1/13	-2,64		A1/13	-2,02
	A1/14	-1,90		A1/14	-2,57		A1/14	-2,58		A1/14	-1,98
X+	A1/18	-1,29	X+	A1/18	-1,76	X+	A1/18	-1,78	X+	A1/18	-1,32

Studio Tecnico Ing. Antonino Tricoli

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	X- A1/25	-1,30		X- A1/25	-1,76		X- A1/25	-1,76		X- A1/25	-1,40
	Y+ A1/41	-1,31		Y+ A1/41	-1,77		Y+ A1/34	-1,79		Y+ A1/41	-1,37
	Y- A1/43	-1,28		Y- A1/43	-1,74		Y- A1/36	-1,72		Y- A1/43	-1,36
302	A1/1	-2,80	303	A1/1	-2,59	304	A1/1	-2,63	305	A1/1	-2,79
	A1/2	-2,71		A1/2	-2,50		A1/2	-2,55		A1/2	-2,71
	A1/3	-2,79		A1/3	-2,59		A1/3	-2,63		A1/3	-2,79
	A1/4	-2,71		A1/4	-2,51		A1/4	-2,55		A1/4	-2,71
	A1/5	-2,66		A1/5	-2,46		A1/5	-2,51		A1/5	-2,67
	A1/6	-2,80		A1/6	-2,59		A1/6	-2,63		A1/6	-2,78
	A1/7	-2,71		A1/7	-2,50		A1/7	-2,55		A1/7	-2,70
	A1/8	-2,66		A1/8	-2,46		A1/8	-2,50		A1/8	-2,65
	A1/9	-2,80		A1/9	-2,59		A1/9	-2,63		A1/9	-2,79
	A1/10	-2,71		A1/10	-2,50		A1/10	-2,55		A1/10	-2,70
	A1/11	-2,67		A1/11	-2,46		A1/11	-2,50		A1/11	-2,65
	A1/12	-2,79		A1/12	-2,59		A1/12	-2,63		A1/12	-2,80
	A1/13	-2,71		A1/13	-2,51		A1/13	-2,55		A1/13	-2,71
	A1/14	-2,66		A1/14	-2,47		A1/14	-2,50		A1/14	-2,67
	X+ A1/18	-1,80		X+ A1/20	-1,69		X+ A1/20	-1,72		X+ A1/21	-1,87
	X- A1/25	-1,85		X- A1/27	-1,68		X- A1/27	-1,70		X- A1/30	-1,80
	Y+ A1/41	-1,84		Y+ A1/34	-1,67		Y+ A1/34	-1,71		Y+ A1/31	-1,79
	Y- A1/43	-1,82		Y- A1/36	-1,70		Y- A1/36	-1,71		Y- A1/37	-1,88
306	A1/1	-2,67	307	A1/1	-2,66	308	A1/1	-2,70	309	A1/1	-2,06
	A1/2	-2,59		A1/2	-2,58		A1/2	-2,62		A1/2	-2,00
	A1/3	-2,67		A1/3	-2,66		A1/3	-2,70		A1/3	-2,05
	A1/4	-2,59		A1/4	-2,57		A1/4	-2,62		A1/4	-2,00
	A1/5	-2,55		A1/5	-2,53		A1/5	-2,57		A1/5	-1,96
	A1/6	-2,66		A1/6	-2,66		A1/6	-2,69		A1/6	-2,06
	A1/7	-2,58		A1/7	-2,57		A1/7	-2,61		A1/7	-2,00
	A1/8	-2,53		A1/8	-2,53		A1/8	-2,56		A1/8	-1,96
	A1/9	-2,67		A1/9	-2,66		A1/9	-2,70		A1/9	-2,06
	A1/10	-2,58		A1/10	-2,58		A1/10	-2,62		A1/10	-2,00
	A1/11	-2,54		A1/11	-2,53		A1/11	-2,57		A1/11	-1,97
	A1/12	-2,68		A1/12	-2,66		A1/12	-2,71		A1/12	-2,05
	A1/13	-2,59		A1/13	-2,58		A1/13	-2,62		A1/13	-2,00
	A1/14	-2,55		A1/14	-2,54		A1/14	-2,58		A1/14	-1,96
	X+ A1/21	-1,78		X+ A1/21	-1,73		X+ A1/21	-1,78		X+ A1/18	-1,32
	X- A1/30	-1,72		X- A1/30	-1,74		X- A1/30	-1,75		X- A1/25	-1,37
	Y+ A1/31	-1,70		Y+ A1/40	-1,71		Y+ A1/31	-1,70		Y+ A1/41	-1,36
	Y- A1/37	-1,79		Y- A1/46	-1,75		Y- A1/37	-1,80		Y- A1/43	-1,34
310	A1/1	-1,91	311	A1/1	-1,63	312	A1/1	-3,69	313	A1/1	-3,23
	A1/2	-1,85		A1/2	-1,59		A1/2	-3,60		A1/2	-3,15
	A1/3	-1,91		A1/3	-1,63		A1/3	-3,69		A1/3	-3,24
	A1/4	-1,85		A1/4	-1,59		A1/4	-3,60		A1/4	-3,16
	A1/5	-1,82		A1/5	-1,56		A1/5	-3,55		A1/5	-3,10
	A1/6	-1,91		A1/6	-1,64		A1/6	-3,68		A1/6	-3,22
	A1/7	-1,85		A1/7	-1,59		A1/7	-3,60		A1/7	-3,14
	A1/8	-1,81		A1/8	-1,56		A1/8	-3,53		A1/8	-3,07
	A1/9	-1,91		A1/9	-1,64		A1/9	-3,69		A1/9	-3,23
	A1/10	-1,85		A1/10	-1,60		A1/10	-3,60		A1/10	-3,14
	A1/11	-1,82		A1/11	-1,57		A1/11	-3,54		A1/11	-3,08
	A1/12	-1,91		A1/12	-1,63		A1/12	-3,70		A1/12	-3,24
	A1/13	-1,85		A1/13	-1,59		A1/13	-3,61		A1/13	-3,16
	A1/14	-1,82		A1/14	-1,56		A1/14	-3,56		A1/14	-3,11
	X+ A1/21	-1,23		X+ A1/18	-1,05		X+ A1/21	-2,49		X+ A1/21	-2,21
	X- A1/30	-1,26		X- A1/25	-1,10		X- A1/30	-2,46		X- A1/30	-2,07
	Y+ A1/40	-1,23		Y+ A1/41	-1,09		Y+ A1/31	-2,41		Y+ A1/31	-2,06
	Y- A1/46	-1,26		Y- A1/43	-1,07		Y- A1/37	-2,52		Y- A1/37	-2,22
314	A1/1	-2,95	315	A1/1	-2,95	316	A1/1	-3,52	317	A1/1	-3,04
	A1/2	-2,87		A1/2	-2,87		A1/2	-3,44		A1/2	-2,97
	A1/3	-2,96		A1/3	-2,96		A1/3	-3,52		A1/3	-3,04
	A1/4	-2,87		A1/4	-2,87		A1/4	-3,44		A1/4	-2,97
	A1/5	-2,82		A1/5	-2,83		A1/5	-3,39		A1/5	-2,93
	A1/6	-2,94		A1/6	-2,95		A1/6	-3,51		A1/6	-3,04
	A1/7	-2,86		A1/7	-2,86		A1/7	-3,43		A1/7	-2,97
	A1/8	-2,80		A1/8	-2,81		A1/8	-3,36		A1/8	-2,92
	A1/9	-2,94		A1/9	-2,94		A1/9	-3,51		A1/9	-3,04
	A1/10	-2,86		A1/10	-2,86		A1/10	-3,43		A1/10	-2,97
	A1/11	-2,80		A1/11	-2,81		A1/11	-3,36		A1/11	-2,93
	A1/12	-2,96		A1/12	-2,95		A1/12	-3,52		A1/12	-3,05
	A1/13	-2,87		A1/13	-2,87		A1/13	-3,44		A1/13	-2,98
	A1/14	-2,82		A1/14	-2,82		A1/14	-3,39		A1/14	-2,94
	X+ A1/21	-2,00		X+ A1/20	-2,01		X+ A1/21	-2,42		X+ A1/21	-2,09
	X- A1/30	-1,87		X- A1/27	-1,87		X- A1/30	-2,28		X- A1/30	-2,04
	Y+ A1/31	-1,88		Y+ A1/34	-1,92		Y+ A1/31	-2,30		Y+ A1/31	-2,00
	Y- A1/37	-1,99		Y- A1/36	-1,99		Y- A1/37	-2,42		Y- A1/37	-2,11
318	A1/1	-2,71	319	A1/1	-2,87	320	A1/1	-2,75	321	A1/1	-2,43
	A1/2	-2,62		A1/2	-2,78		A1/2	-2,67		A1/2	-2,35

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/3	-2,71		A1/3	-2,87		A1/3	-2,76		A1/3	-2,43
	A1/4	-2,63		A1/4	-2,79		A1/4	-2,67		A1/4	-2,35
	A1/5	-2,59		A1/5	-2,73		A1/5	-2,62		A1/5	-2,32
	A1/6	-2,70		A1/6	-2,86		A1/6	-2,75		A1/6	-2,43
	A1/7	-2,62		A1/7	-2,78		A1/7	-2,67		A1/7	-2,35
	A1/8	-2,59		A1/8	-2,71		A1/8	-2,62		A1/8	-2,32
	A1/9	-2,70		A1/9	-2,87		A1/9	-2,75		A1/9	-2,43
	A1/10	-2,62		A1/10	-2,78		A1/10	-2,66		A1/10	-2,34
	A1/11	-2,59		A1/11	-2,72		A1/11	-2,61		A1/11	-2,31
	A1/12	-2,71		A1/12	-2,88		A1/12	-2,75		A1/12	-2,43
	A1/13	-2,63		A1/13	-2,79		A1/13	-2,67		A1/13	-2,34
	A1/14	-2,59		A1/14	-2,74		A1/14	-2,61		A1/14	-2,31
X+	A1/21	-1,83	X+	A1/21	-1,89	X+	A1/18	-1,82	X+	A1/18	-1,62
X-	A1/30	-1,77	X-	A1/30	-1,84	X-	A1/25	-1,75	X-	A1/25	-1,57
Y+	A1/31	-1,78	Y+	A1/31	-1,80	Y+	A1/34	-1,81	Y+	A1/34	-1,62
Y-	A1/37	-1,83	Y-	A1/37	-1,91	Y-	A1/36	-1,77	Y-	A1/36	-1,57
322	A1/1	-2,07	323	A1/1	-1,72	324	A1/1	-3,16	325	A1/1	-3,94
	A1/2	-2,01		A1/2	-1,67		A1/2	-3,08		A1/2	-3,86
	A1/3	-2,07		A1/3	-1,72		A1/3	-3,15		A1/3	-3,93
	A1/4	-2,01		A1/4	-1,67		A1/4	-3,07		A1/4	-3,85
	A1/5	-1,97		A1/5	-1,63		A1/5	-3,03		A1/5	-3,79
	A1/6	-2,07		A1/6	-1,71		A1/6	-3,17		A1/6	-3,95
	A1/7	-2,00		A1/7	-1,66		A1/7	-3,09		A1/7	-3,87
	A1/8	-1,96		A1/8	-1,62		A1/8	-3,06		A1/8	-3,83
	A1/9	-2,07		A1/9	-1,72		A1/9	-3,17		A1/9	-3,95
	A1/10	-2,01		A1/10	-1,67		A1/10	-3,09		A1/10	-3,88
	A1/11	-1,97		A1/11	-1,63		A1/11	-3,06		A1/11	-3,84
	A1/12	-2,08		A1/12	-1,73		A1/12	-3,15		A1/12	-3,93
	A1/13	-2,02		A1/13	-1,68		A1/13	-3,07		A1/13	-3,86
	A1/14	-1,98		A1/14	-1,64		A1/14	-3,03		A1/14	-3,80
X+	A1/21	-1,34	X+	A1/21	-1,11	X+	A1/15	-2,09	X+	A1/15	-2,59
X-	A1/30	-1,36	X-	A1/30	-1,12	X-	A1/24	-2,22	X-	A1/24	-2,85
Y+	A1/40	-1,29	Y+	A1/40	-1,06	Y+	A1/40	-2,21	Y+	A1/40	-2,79
Y-	A1/46	-1,39	Y-	A1/46	-1,14	Y-	A1/46	-2,11	Y-	A1/46	-2,71
326	A1/1	-4,70	327	A1/1	-3,60	328	A1/1	-3,15	329	A1/1	-2,76
	A1/2	-4,63		A1/2	-3,52		A1/2	-3,08		A1/2	-2,68
	A1/3	-4,67		A1/3	-3,59		A1/3	-3,14		A1/3	-2,76
	A1/4	-4,60		A1/4	-3,51		A1/4	-3,07		A1/4	-2,68
	A1/5	-4,52		A1/5	-3,46		A1/5	-3,04		A1/5	-2,65
	A1/6	-4,74		A1/6	-3,62		A1/6	-3,14		A1/6	-2,76
	A1/7	-4,66		A1/7	-3,54		A1/7	-3,07		A1/7	-2,68
	A1/8	-4,62		A1/8	-3,51		A1/8	-3,03		A1/8	-2,65
	A1/9	-4,72		A1/9	-3,61		A1/9	-3,15		A1/9	-2,76
	A1/10	-4,65		A1/10	-3,54		A1/10	-3,08		A1/10	-2,68
	A1/11	-4,60		A1/11	-3,50		A1/11	-3,05		A1/11	-2,65
	A1/12	-4,66		A1/12	-3,58		A1/12	-3,15		A1/12	-2,76
	A1/13	-4,59		A1/13	-3,50		A1/13	-3,08		A1/13	-2,68
	A1/14	-4,49		A1/14	-3,44		A1/14	-3,05		A1/14	-2,65
X+	A1/15	-3,06	X+	A1/15	-2,36	X+	A1/21	-2,12	X+	A1/21	-1,85
X-	A1/24	-3,56	X-	A1/24	-2,61	X-	A1/30	-2,20	X-	A1/30	-1,87
Y+	A1/40	-3,59	Y+	A1/40	-2,63	Y+	A1/40	-2,12	Y+	A1/40	-1,85
Y-	A1/46	-3,01	Y-	A1/46	-2,33	Y-	A1/46	-2,21	Y-	A1/46	-1,87
330	A1/1	-2,47	331	A1/1	-2,94	332	A1/1	-3,38	333	A1/1	-2,73
	A1/2	-2,39		A1/2	-2,86		A1/2	-3,30		A1/2	-2,64
	A1/3	-2,47		A1/3	-2,94		A1/3	-3,37		A1/3	-2,73
	A1/4	-2,39		A1/4	-2,86		A1/4	-3,29		A1/4	-2,64
	A1/5	-2,36		A1/5	-2,82		A1/5	-3,24		A1/5	-2,60
	A1/6	-2,48		A1/6	-2,95		A1/6	-3,39		A1/6	-2,73
	A1/7	-2,39		A1/7	-2,87		A1/7	-3,31		A1/7	-2,64
	A1/8	-2,37		A1/8	-2,83		A1/8	-3,27		A1/8	-2,60
	A1/9	-2,47		A1/9	-2,95		A1/9	-3,38		A1/9	-2,73
	A1/10	-2,39		A1/10	-2,87		A1/10	-3,31		A1/10	-2,65
	A1/11	-2,36		A1/11	-2,83		A1/11	-3,26		A1/11	-2,60
	A1/12	-2,47		A1/12	-2,94		A1/12	-3,36		A1/12	-2,73
	A1/13	-2,39		A1/13	-2,86		A1/13	-3,29		A1/13	-2,64
	A1/14	-2,36		A1/14	-2,82		A1/14	-3,23		A1/14	-2,60
X+	A1/15	-1,64	X+	A1/15	-1,94	X+	A1/15	-2,21	X+	A1/21	-1,75
X-	A1/24	-1,65	X-	A1/24	-2,02	X-	A1/24	-2,37	X-	A1/30	-1,81
Y+	A1/40	-1,66	Y+	A1/40	-2,02	Y+	A1/40	-2,38	Y+	A1/40	-1,79
Y-	A1/46	-1,62	Y-	A1/46	-1,94	Y-	A1/46	-2,20	Y-	A1/46	-1,79
334	A1/1	-2,32	335	A1/1	-2,36	336	A1/1	-2,71	337	A1/1	-2,47
	A1/2	-2,25		A1/2	-2,29		A1/2	-2,62		A1/2	-2,41
	A1/3	-2,32		A1/3	-2,35		A1/3	-2,70		A1/3	-2,47
	A1/4	-2,25		A1/4	-2,28		A1/4	-2,62		A1/4	-2,40
	A1/5	-2,21		A1/5	-2,23		A1/5	-2,56		A1/5	-2,36
	A1/6	-2,32		A1/6	-2,35		A1/6	-2,70		A1/6	-2,48
	A1/7	-2,25		A1/7	-2,28		A1/7	-2,62		A1/7	-2,41
	A1/8	-2,21		A1/8	-2,23		A1/8	-2,56		A1/8	-2,37

Studio Tecnico Ing. Antonino Tricoli

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/9	-2,32		A1/9	-2,36		A1/9	-2,71		A1/9	-2,48
	A1/10	-2,25		A1/10	-2,29		A1/10	-2,62		A1/10	-2,41
	A1/11	-2,22		A1/11	-2,24		A1/11	-2,57		A1/11	-2,36
	A1/12	-2,32		A1/12	-2,36		A1/12	-2,71		A1/12	-2,47
	A1/13	-2,25		A1/13	-2,29		A1/13	-2,62		A1/13	-2,40
	A1/14	-2,21		A1/14	-2,25		A1/14	-2,57		A1/14	-2,36
X+	A1/21	-1,49	X+	A1/21	-1,51	X+	A1/21	-1,71	X+	A1/18	-1,61
X-	A1/30	-1,54	X-	A1/30	-1,56	X-	A1/30	-1,79	X-	A1/25	-1,64
Y+	A1/40	-1,51	Y+	A1/40	-1,48	Y+	A1/40	-1,74	Y+	A1/41	-1,64
Y-	A1/46	-1,53	Y-	A1/46	-1,57	Y-	A1/46	-1,78	Y-	A1/43	-1,61
338	A1/1	-2,99	339	A1/1	-2,62	340	A1/1	-2,89	341	A1/1	-1,67
	A1/2	-2,91		A1/2	-2,54		A1/2	-2,80		A1/2	-1,63
	A1/3	-2,99		A1/3	-2,61		A1/3	-2,88		A1/3	-1,67
	A1/4	-2,90		A1/4	-2,54		A1/4	-2,79		A1/4	-1,63
	A1/5	-2,85		A1/5	-2,47		A1/5	-2,72		A1/5	-1,59
	A1/6	-2,99		A1/6	-2,61		A1/6	-2,89		A1/6	-1,67
	A1/7	-2,91		A1/7	-2,53		A1/7	-2,80		A1/7	-1,63
	A1/8	-2,86		A1/8	-2,47		A1/8	-2,73		A1/8	-1,60
	A1/9	-2,99		A1/9	-2,62		A1/9	-2,89		A1/9	-1,67
	A1/10	-2,91		A1/10	-2,54		A1/10	-2,80		A1/10	-1,63
	A1/11	-2,86		A1/11	-2,48		A1/11	-2,74		A1/11	-1,60
	A1/12	-2,99		A1/12	-2,62		A1/12	-2,89		A1/12	-1,67
	A1/13	-2,90		A1/13	-2,54		A1/13	-2,80		A1/13	-1,62
	A1/14	-2,85		A1/14	-2,49		A1/14	-2,74		A1/14	-1,59
X+	A1/18	-1,95	X+	A1/21	-1,65	X+	A1/21	-1,79	X+	A1/18	-1,09
X-	A1/25	-1,99	X-	A1/30	-1,71	X-	A1/30	-1,90	X-	A1/25	-1,10
Y+	A1/41	-1,99	Y+	A1/40	-1,63	Y+	A1/40	-1,84	Y+	A1/41	-1,10
Y-	A1/43	-1,95	Y-	A1/46	-1,72	Y-	A1/46	-1,87	Y-	A1/43	-1,09
342	A1/1	-2,29	343	A1/1	-2,31	344	A1/1	-3,00	345	A1/1	-2,73
	A1/2	-2,24		A1/2	-2,26		A1/2	-2,91		A1/2	-2,64
	A1/3	-2,29		A1/3	-2,31		A1/3	-2,99		A1/3	-2,72
	A1/4	-2,24		A1/4	-2,25		A1/4	-2,91		A1/4	-2,64
	A1/5	-2,20		A1/5	-2,21		A1/5	-2,86		A1/5	-2,59
	A1/6	-2,30		A1/6	-2,32		A1/6	-3,00		A1/6	-2,73
	A1/7	-2,24		A1/7	-2,26		A1/7	-2,92		A1/7	-2,64
	A1/8	-2,20		A1/8	-2,22		A1/8	-2,87		A1/8	-2,60
	A1/9	-2,29		A1/9	-2,32		A1/9	-3,00		A1/9	-2,73
	A1/10	-2,24		A1/10	-2,26		A1/10	-2,91		A1/10	-2,64
	A1/11	-2,20		A1/11	-2,22		A1/11	-2,87		A1/11	-2,60
	A1/12	-2,29		A1/12	-2,31		A1/12	-2,99		A1/12	-2,72
	A1/13	-2,24		A1/13	-2,25		A1/13	-2,91		A1/13	-2,64
	A1/14	-2,19		A1/14	-2,21		A1/14	-2,85		A1/14	-2,59
X+	A1/18	-1,51	X+	A1/18	-1,50	X+	A1/18	-1,95	X+	A1/15	-1,76
X-	A1/25	-1,53	X-	A1/25	-1,56	X-	A1/25	-2,00	X-	A1/24	-1,80
Y+	A1/41	-1,53	Y+	A1/41	-1,56	Y+	A1/41	-2,01	Y+	A1/40	-1,80
Y-	A1/43	-1,50	Y-	A1/43	-1,51	Y-	A1/43	-1,93	Y-	A1/46	-1,76
346	A1/1	-2,37	347	A1/1	-1,84	348	A1/1	-2,17	349	A1/1	-2,71
	A1/2	-2,30		A1/2	-1,79		A1/2	-2,11		A1/2	-2,63
	A1/3	-2,37		A1/3	-1,84		A1/3	-2,17		A1/3	-2,71
	A1/4	-2,30		A1/4	-1,79		A1/4	-2,11		A1/4	-2,62
	A1/5	-2,26		A1/5	-1,75		A1/5	-2,07		A1/5	-2,57
	A1/6	-2,38		A1/6	-1,84		A1/6	-2,18		A1/6	-2,71
	A1/7	-2,31		A1/7	-1,80		A1/7	-2,11		A1/7	-2,63
	A1/8	-2,27		A1/8	-1,76		A1/8	-2,08		A1/8	-2,58
	A1/9	-2,37		A1/9	-1,84		A1/9	-2,18		A1/9	-2,72
	A1/10	-2,30		A1/10	-1,79		A1/10	-2,11		A1/10	-2,63
	A1/11	-2,26		A1/11	-1,76		A1/11	-2,07		A1/11	-2,58
	A1/12	-2,36		A1/12	-1,83		A1/12	-2,17		A1/12	-2,71
	A1/13	-2,30		A1/13	-1,79		A1/13	-2,10		A1/13	-2,63
	A1/14	-2,25		A1/14	-1,75		A1/14	-2,06		A1/14	-2,58
X+	A1/18	-1,56	X+	A1/18	-1,21	X+	A1/15	-1,42	X+	A1/21	-1,71
X-	A1/25	-1,57	X-	A1/25	-1,22	X-	A1/24	-1,42	X-	A1/30	-1,79
Y+	A1/41	-1,61	Y+	A1/41	-1,24	Y+	A1/40	-1,45	Y+	A1/40	-1,76
Y-	A1/43	-1,49	Y-	A1/43	-1,17	Y-	A1/46	-1,38	Y-	A1/46	-1,76
350	A1/1	-2,95	351	A1/1	-2,18	352	A1/1	-2,25	353	A1/1	-1,60
	A1/2	-2,86		A1/2	-2,11		A1/2	-2,18		A1/2	-1,55
	A1/3	-2,94		A1/3	-2,17		A1/3	-2,24		A1/3	-1,60
	A1/4	-2,85		A1/4	-2,11		A1/4	-2,18		A1/4	-1,55
	A1/5	-2,78		A1/5	-2,06		A1/5	-2,12		A1/5	-1,52
	A1/6	-2,94		A1/6	-2,18		A1/6	-2,24		A1/6	-1,61
	A1/7	-2,85		A1/7	-2,11		A1/7	-2,18		A1/7	-1,56
	A1/8	-2,79		A1/8	-2,07		A1/8	-2,12		A1/8	-1,53
	A1/9	-2,95		A1/9	-2,18		A1/9	-2,25		A1/9	-1,60
	A1/10	-2,86		A1/10	-2,11		A1/10	-2,18		A1/10	-1,55
	A1/11	-2,80		A1/11	-2,07		A1/11	-2,13		A1/11	-1,52
	A1/12	-2,95		A1/12	-2,18		A1/12	-2,25		A1/12	-1,60
	A1/13	-2,86		A1/13	-2,11		A1/13	-2,18		A1/13	-1,55
	A1/14	-2,79		A1/14	-2,06		A1/14	-2,13		A1/14	-1,51

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	X+ A1/21	-1,80		X+ A1/15	-1,38		X+ A1/21	-1,38		X+ A1/18	-1,04
	X- A1/30	-1,95		X- A1/24	-1,41		X- A1/30	-1,47		X- A1/25	-1,04
	Y+ A1/40	-1,89		Y+ A1/40	-1,40		Y+ A1/40	-1,42		Y+ A1/41	-1,07
	Y- A1/46	-1,91		Y- A1/46	-1,40		Y- A1/46	-1,45		Y- A1/43	-0,99
354	A1/1	-1,58	355	A1/1	-1,76	356	A1/1	-1,99	357	A1/1	-2,18
	A1/2	-1,52		A1/2	-1,70		A1/2	-1,94		A1/2	-2,14
	A1/3	-1,58		A1/3	-1,76		A1/3	-1,99		A1/3	-2,18
	A1/4	-1,52		A1/4	-1,70		A1/4	-1,94		A1/4	-2,14
	A1/5	-1,50		A1/5	-1,68		A1/5	-1,91		A1/5	-2,09
	A1/6	-1,58		A1/6	-1,76		A1/6	-1,99		A1/6	-2,19
	A1/7	-1,53		A1/7	-1,71		A1/7	-1,94		A1/7	-2,14
	A1/8	-1,51		A1/8	-1,69		A1/8	-1,91		A1/8	-2,11
	A1/9	-1,58		A1/9	-1,76		A1/9	-1,99		A1/9	-2,19
	A1/10	-1,52		A1/10	-1,70		A1/10	-1,94		A1/10	-2,14
	A1/11	-1,50		A1/11	-1,68		A1/11	-1,91		A1/11	-2,11
	A1/12	-1,57		A1/12	-1,76		A1/12	-1,99		A1/12	-2,18
	A1/13	-1,52		A1/13	-1,70		A1/13	-1,94		A1/13	-2,13
	A1/14	-1,49		A1/14	-1,68		A1/14	-1,90		A1/14	-2,09
	X+ A1/18	-1,04		X+ A1/18	-1,16		X+ A1/15	-1,31		X+ A1/15	-1,43
	X- A1/25	-1,04		X- A1/25	-1,17		X- A1/24	-1,35		X- A1/24	-1,51
	Y+ A1/34	-1,07		Y+ A1/41	-1,19		Y+ A1/40	-1,35		Y+ A1/40	-1,51
	Y- A1/36	-0,98		Y- A1/43	-1,14		Y- A1/46	-1,31		Y- A1/46	-1,43
358	A1/1	-2,11	359	A1/1	-2,39	360	A1/1	-2,71	361	A1/1	-2,52
	A1/2	-2,04		A1/2	-2,30		A1/2	-2,62		A1/2	-2,44
	A1/3	-2,11		A1/3	-2,38		A1/3	-2,71		A1/3	-2,52
	A1/4	-2,04		A1/4	-2,30		A1/4	-2,62		A1/4	-2,44
	A1/5	-2,00		A1/5	-2,26		A1/5	-2,56		A1/5	-2,38
	A1/6	-2,12		A1/6	-2,39		A1/6	-2,72		A1/6	-2,53
	A1/7	-2,05		A1/7	-2,31		A1/7	-2,63		A1/7	-2,45
	A1/8	-2,02		A1/8	-2,27		A1/8	-2,57		A1/8	-2,40
	A1/9	-2,11		A1/9	-2,39		A1/9	-2,72		A1/9	-2,52
	A1/10	-2,04		A1/10	-2,31		A1/10	-2,63		A1/10	-2,44
	A1/11	-2,01		A1/11	-2,27		A1/11	-2,57		A1/11	-2,39
	A1/12	-2,10		A1/12	-2,38		A1/12	-2,71		A1/12	-2,51
	A1/13	-2,03		A1/13	-2,30		A1/13	-2,62		A1/13	-2,43
	A1/14	-1,99		A1/14	-2,26		A1/14	-2,56		A1/14	-2,37
	X+ A1/18	-1,37		X+ A1/15	-1,52		X+ A1/15	-1,68		X+ A1/18	-1,60
	X- A1/25	-1,40		X- A1/24	-1,58		X- A1/24	-1,79		X- A1/25	-1,64
	Y+ A1/41	-1,42		Y+ A1/40	-1,58		Y+ A1/40	-1,77		Y+ A1/41	-1,67
	Y- A1/43	-1,32		Y- A1/46	-1,52		Y- A1/46	-1,71		Y- A1/43	-1,56
362	A1/1	-1,92	363	A1/1	-2,43	364	A1/1	-2,73	365	A1/1	-2,44
	A1/2	-1,85		A1/2	-2,34		A1/2	-2,65		A1/2	-2,35
	A1/3	-1,91		A1/3	-2,43		A1/3	-2,73		A1/3	-2,43
	A1/4	-1,85		A1/4	-2,34		A1/4	-2,64		A1/4	-2,35
	A1/5	-1,82		A1/5	-2,31		A1/5	-2,57		A1/5	-2,30
	A1/6	-1,92		A1/6	-2,43		A1/6	-2,74		A1/6	-2,44
	A1/7	-1,85		A1/7	-2,35		A1/7	-2,65		A1/7	-2,35
	A1/8	-1,83		A1/8	-2,32		A1/8	-2,59		A1/8	-2,31
	A1/9	-1,92		A1/9	-2,43		A1/9	-2,74		A1/9	-2,44
	A1/10	-1,85		A1/10	-2,35		A1/10	-2,65		A1/10	-2,36
	A1/11	-1,83		A1/11	-2,32		A1/11	-2,60		A1/11	-2,32
	A1/12	-1,91		A1/12	-2,42		A1/12	-2,73		A1/12	-2,43
	A1/13	-1,85		A1/13	-2,34		A1/13	-2,64		A1/13	-2,35
	A1/14	-1,82		A1/14	-2,31		A1/14	-2,58		A1/14	-2,31
	X+ A1/18	-1,26		X+ A1/15	-1,58		X+ A1/15	-1,66		X+ A1/15	-1,53
	X- A1/25	-1,28		X- A1/24	-1,62		X- A1/24	-1,82		X- A1/24	-1,62
	Y+ A1/41	-1,29		Y+ A1/40	-1,62		Y+ A1/40	-1,78		Y+ A1/40	-1,60
	Y- A1/43	-1,24		Y- A1/46	-1,57		Y- A1/46	-1,74		Y- A1/46	-1,57
366	A1/1	-1,82	367	A1/1	-1,99	368	A1/1	-2,46	369	A1/1	-1,98
	A1/2	-1,76		A1/2	-1,93		A1/2	-2,38		A1/2	-1,92
	A1/3	-1,81		A1/3	-1,99		A1/3	-2,46		A1/3	-1,98
	A1/4	-1,76		A1/4	-1,92		A1/4	-2,38		A1/4	-1,92
	A1/5	-1,71		A1/5	-1,89		A1/5	-2,35		A1/5	-1,89
	A1/6	-1,82		A1/6	-2,00		A1/6	-2,47		A1/6	-1,98
	A1/7	-1,76		A1/7	-1,93		A1/7	-2,38		A1/7	-1,92
	A1/8	-1,72		A1/8	-1,89		A1/8	-2,35		A1/8	-1,89
	A1/9	-1,82		A1/9	-2,00		A1/9	-2,47		A1/9	-1,98
	A1/10	-1,76		A1/10	-1,93		A1/10	-2,38		A1/10	-1,92
	A1/11	-1,72		A1/11	-1,90		A1/11	-2,35		A1/11	-1,89
	A1/12	-1,81		A1/12	-1,99		A1/12	-2,46		A1/12	-1,98
	A1/13	-1,76		A1/13	-1,93		A1/13	-2,38		A1/13	-1,92
	A1/14	-1,71		A1/14	-1,89		A1/14	-2,35		A1/14	-1,89
	X+ A1/15	-1,11		X+ A1/15	-1,26		X+ A1/15	-1,60		X+ A1/21	-1,29
	X- A1/24	-1,19		X- A1/24	-1,31		X- A1/24	-1,63		X- A1/30	-1,31
	Y+ A1/40	-1,17		Y+ A1/40	-1,30		Y+ A1/40	-1,63		Y+ A1/40	-1,29
	Y- A1/46	-1,15		Y- A1/46	-1,28		Y- A1/46	-1,61		Y- A1/46	-1,31
370	A1/1	-2,89	371	A1/1	-2,77	372	A1/1	-2,36	373	A1/1	-3,19

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/2	-2,80		A1/2	-2,69		A1/2	-2,29		A1/2	-3,12
	A1/3	-2,88		A1/3	-2,77		A1/3	-2,36		A1/3	-3,19
	A1/4	-2,80		A1/4	-2,69		A1/4	-2,29		A1/4	-3,12
	A1/5	-2,76		A1/5	-2,65		A1/5	-2,26		A1/5	-3,06
	A1/6	-2,89		A1/6	-2,77		A1/6	-2,36		A1/6	-3,20
	A1/7	-2,80		A1/7	-2,69		A1/7	-2,30		A1/7	-3,13
	A1/8	-2,76		A1/8	-2,66		A1/8	-2,26		A1/8	-3,08
	A1/9	-2,89		A1/9	-2,77		A1/9	-2,36		A1/9	-3,20
	A1/10	-2,80		A1/10	-2,69		A1/10	-2,30		A1/10	-3,13
	A1/11	-2,76		A1/11	-2,65		A1/11	-2,26		A1/11	-3,07
	A1/12	-2,88		A1/12	-2,77		A1/12	-2,36		A1/12	-3,19
	A1/13	-2,80		A1/13	-2,68		A1/13	-2,29		A1/13	-3,11
	A1/14	-2,76		A1/14	-2,65		A1/14	-2,25		A1/14	-3,06
X+	A1/18	-1,91	X+	A1/15	-1,82	X+	A1/15	-1,55	X+	A1/15	-2,09
X-	A1/25	-1,92	X-	A1/24	-1,86	X-	A1/24	-1,60	X-	A1/24	-2,19
Y+	A1/41	-1,92	Y+	A1/40	-1,86	Y+	A1/40	-1,60	Y+	A1/40	-2,18
Y-	A1/43	-1,90	Y-	A1/46	-1,82	Y-	A1/46	-1,55	Y-	A1/46	-2,10
374	A1/1	-3,17	375	A1/1	-3,28	376	A1/1	-2,49	377	A1/1	-2,92
	A1/2	-3,09		A1/2	-3,20		A1/2	-2,43		A1/2	-2,86
	A1/3	-3,17		A1/3	-3,28		A1/3	-2,49		A1/3	-2,92
	A1/4	-3,09		A1/4	-3,20		A1/4	-2,43		A1/4	-2,86
	A1/5	-3,04		A1/5	-3,15		A1/5	-2,39		A1/5	-2,81
	A1/6	-3,17		A1/6	-3,28		A1/6	-2,49		A1/6	-2,92
	A1/7	-3,09		A1/7	-3,20		A1/7	-2,43		A1/7	-2,86
	A1/8	-3,05		A1/8	-3,15		A1/8	-2,39		A1/8	-2,81
	A1/9	-3,17		A1/9	-3,28		A1/9	-2,49		A1/9	-2,92
	A1/10	-3,09		A1/10	-3,20		A1/10	-2,43		A1/10	-2,86
	A1/11	-3,04		A1/11	-3,15		A1/11	-2,39		A1/11	-2,80
	A1/12	-3,16		A1/12	-3,27		A1/12	-2,49		A1/12	-2,92
	A1/13	-3,09		A1/13	-3,20		A1/13	-2,43		A1/13	-2,86
	A1/14	-3,03		A1/14	-3,14		A1/14	-2,39		A1/14	-2,80
X+	A1/15	-2,09	X+	A1/18	-2,18	X+	A1/18	-1,65	X+	A1/18	-1,96
X-	A1/24	-2,14	X-	A1/25	-2,18	X-	A1/25	-1,64	X-	A1/25	-1,93
Y+	A1/40	-2,15	Y+	A1/34	-2,20	Y+	A1/34	-1,65	Y+	A1/34	-1,97
Y-	A1/46	-2,08	Y-	A1/36	-2,15	Y-	A1/36	-1,65	Y-	A1/36	-1,91
378	A1/1	-3,40	379	A1/1	-2,32	380	A1/1	-2,17	381	A1/1	-2,78
	A1/2	-3,32		A1/2	-2,27		A1/2	-2,11		A1/2	-2,70
	A1/3	-3,41		A1/3	-2,33		A1/3	-2,17		A1/3	-2,79
	A1/4	-3,33		A1/4	-2,28		A1/4	-2,11		A1/4	-2,70
	A1/5	-3,27		A1/5	-2,23		A1/5	-2,08		A1/5	-2,67
	A1/6	-3,38		A1/6	-2,31		A1/6	-2,17		A1/6	-2,78
	A1/7	-3,30		A1/7	-2,27		A1/7	-2,11		A1/7	-2,69
	A1/8	-3,23		A1/8	-2,21		A1/8	-2,07		A1/8	-2,65
	A1/9	-3,39		A1/9	-2,31		A1/9	-2,16		A1/9	-2,78
	A1/10	-3,31		A1/10	-2,27		A1/10	-2,11		A1/10	-2,69
	A1/11	-3,24		A1/11	-2,22		A1/11	-2,07		A1/11	-2,65
	A1/12	-3,41		A1/12	-2,33		A1/12	-2,17		A1/12	-2,79
	A1/13	-3,33		A1/13	-2,28		A1/13	-2,11		A1/13	-2,70
	A1/14	-3,28		A1/14	-2,23		A1/14	-2,08		A1/14	-2,67
X+	A1/21	-2,38	X+	A1/21	-1,61	X+	A1/21	-1,48	X+	A1/21	-1,91
X-	A1/30	-2,20	X-	A1/30	-1,50	X-	A1/30	-1,41	X-	A1/30	-1,80
Y+	A1/31	-2,17	Y+	A1/31	-1,51	Y+	A1/31	-1,43	Y+	A1/31	-1,82
Y-	A1/37	-2,39	Y-	A1/37	-1,60	Y-	A1/37	-1,47	Y-	A1/37	-1,90
382	A1/1	-3,39	383	A1/1	-2,64	384	A1/1	-2,37	385	A1/1	-2,30
	A1/2	-3,32		A1/2	-2,55		A1/2	-2,29		A1/2	-2,21
	A1/3	-3,40		A1/3	-2,64		A1/3	-2,37		A1/3	-2,30
	A1/4	-3,32		A1/4	-2,56		A1/4	-2,29		A1/4	-2,21
	A1/5	-3,27		A1/5	-2,53		A1/5	-2,27		A1/5	-2,19
	A1/6	-3,37		A1/6	-2,63		A1/6	-2,37		A1/6	-2,30
	A1/7	-3,29		A1/7	-2,55		A1/7	-2,29		A1/7	-2,21
	A1/8	-3,22		A1/8	-2,51		A1/8	-2,26		A1/8	-2,19
	A1/9	-3,39		A1/9	-2,63		A1/9	-2,37		A1/9	-2,29
	A1/10	-3,31		A1/10	-2,55		A1/10	-2,28		A1/10	-2,21
	A1/11	-3,24		A1/11	-2,52		A1/11	-2,26		A1/11	-2,18
	A1/12	-3,42		A1/12	-2,64		A1/12	-2,37		A1/12	-2,30
	A1/13	-3,34		A1/13	-2,56		A1/13	-2,29		A1/13	-2,21
	A1/14	-3,29		A1/14	-2,53		A1/14	-2,27		A1/14	-2,19
X+	A1/21	-2,40	X+	A1/21	-1,80	X+	A1/21	-1,61	X+	A1/21	-1,55
X-	A1/30	-2,21	X-	A1/30	-1,72	X-	A1/30	-1,53	X-	A1/30	-1,48
Y+	A1/31	-2,11	Y+	A1/31	-1,72	Y+	A1/31	-1,56	Y+	A1/31	-1,52
Y-	A1/37	-2,45	Y-	A1/37	-1,81	Y-	A1/37	-1,59	Y-	A1/37	-1,53
386	A1/1	-1,84	387	A1/1	-2,13	388	A1/1	-2,39	389	A1/1	-2,08
	A1/2	-1,78		A1/2	-2,07		A1/2	-2,31		A1/2	-2,02
	A1/3	-1,84		A1/3	-2,14		A1/3	-2,40		A1/3	-2,08
	A1/4	-1,78		A1/4	-2,07		A1/4	-2,32		A1/4	-2,02
	A1/5	-1,76		A1/5	-2,04		A1/5	-2,29		A1/5	-1,99
	A1/6	-1,84		A1/6	-2,13		A1/6	-2,39		A1/6	-2,07
	A1/7	-1,78		A1/7	-2,06		A1/7	-2,31		A1/7	-2,01

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/8	-1,75		A1/8	-2,03		A1/8	-2,28		A1/8	-1,97
	A1/9	-1,84		A1/9	-2,13		A1/9	-2,39		A1/9	-2,07
	A1/10	-1,78		A1/10	-2,06		A1/10	-2,30		A1/10	-2,01
	A1/11	-1,75		A1/11	-2,03		A1/11	-2,27		A1/11	-1,97
	A1/12	-1,84		A1/12	-2,14		A1/12	-2,40		A1/12	-2,08
	A1/13	-1,78		A1/13	-2,07		A1/13	-2,31		A1/13	-2,02
	A1/14	-1,76		A1/14	-2,04		A1/14	-2,29		A1/14	-1,99
X+	A1/21	-1,25	X+	A1/21	-1,45	X+	A1/21	-1,64	X+	A1/21	-1,43
X-	A1/30	-1,20	X-	A1/30	-1,38	X-	A1/30	-1,52	X-	A1/30	-1,32
Y+	A1/31	-1,21	Y+	A1/31	-1,37	Y+	A1/31	-1,57	Y+	A1/31	-1,33
Y-	A1/37	-1,24	Y-	A1/37	-1,46	Y-	A1/37	-1,62	Y-	A1/37	-1,42
390	A1/1	-2,25	391	A1/1	-2,32	392	A1/1	-2,14	393	A1/1	-2,71
	A1/2	-2,18		A1/2	-2,23		A1/2	-2,07		A1/2	-2,62
	A1/3	-2,26		A1/3	-2,32		A1/3	-2,14		A1/3	-2,71
	A1/4	-2,19		A1/4	-2,24		A1/4	-2,07		A1/4	-2,63
	A1/5	-2,16		A1/5	-2,21		A1/5	-2,04		A1/5	-2,59
	A1/6	-2,25		A1/6	-2,32		A1/6	-2,14		A1/6	-2,70
	A1/7	-2,18		A1/7	-2,23		A1/7	-2,07		A1/7	-2,62
	A1/8	-2,14		A1/8	-2,21		A1/8	-2,03		A1/8	-2,58
	A1/9	-2,24		A1/9	-2,31		A1/9	-2,13		A1/9	-2,70
	A1/10	-2,17		A1/10	-2,23		A1/10	-2,06		A1/10	-2,62
	A1/11	-2,13		A1/11	-2,20		A1/11	-2,02		A1/11	-2,58
	A1/12	-2,25		A1/12	-2,32		A1/12	-2,14		A1/12	-2,71
	A1/13	-2,19		A1/13	-2,23		A1/13	-2,07		A1/13	-2,63
	A1/14	-2,15		A1/14	-2,21		A1/14	-2,03		A1/14	-2,59
X+	A1/21	-1,58	X+	A1/21	-1,57	X+	A1/21	-1,46	X+	A1/21	-1,84
X-	A1/30	-1,39	X-	A1/30	-1,47	X-	A1/30	-1,33	X-	A1/30	-1,77
Y+	A1/31	-1,48	Y+	A1/31	-1,53	Y+	A1/31	-1,41	Y+	A1/31	-1,77
Y-	A1/37	-1,53	Y-	A1/37	-1,54	Y-	A1/37	-1,42	Y-	A1/37	-1,83
394	A1/1	-3,46	395	A1/1	-3,25	396	A1/1	-2,34	397	A1/1	-1,99
	A1/2	-3,38		A1/2	-3,18		A1/2	-2,28		A1/2	-1,92
	A1/3	-3,47		A1/3	-3,25		A1/3	-2,35		A1/3	-1,99
	A1/4	-3,39		A1/4	-3,18		A1/4	-2,28		A1/4	-1,93
	A1/5	-3,33		A1/5	-3,12		A1/5	-2,25		A1/5	-1,90
	A1/6	-3,44		A1/6	-3,22		A1/6	-2,35		A1/6	-1,99
	A1/7	-3,36		A1/7	-3,15		A1/7	-2,28		A1/7	-1,93
	A1/8	-3,28		A1/8	-3,08		A1/8	-2,25		A1/8	-1,90
	A1/9	-3,46		A1/9	-3,24		A1/9	-2,34		A1/9	-1,99
	A1/10	-3,38		A1/10	-3,17		A1/10	-2,28		A1/10	-1,92
	A1/11	-3,31		A1/11	-3,11		A1/11	-2,24		A1/11	-1,90
	A1/12	-3,49		A1/12	-3,27		A1/12	-2,34		A1/12	-1,99
	A1/13	-3,41		A1/13	-3,20		A1/13	-2,28		A1/13	-1,92
	A1/14	-3,36		A1/14	-3,15		A1/14	-2,24		A1/14	-1,89
X+	A1/21	-2,41	X+	A1/21	-2,24	X+	A1/15	-1,58	X+	A1/15	-1,33
X-	A1/30	-2,30	X-	A1/30	-2,16	X-	A1/24	-1,54	X-	A1/24	-1,30
Y+	A1/31	-2,11	Y+	A1/31	-1,98	Y+	A1/31	-1,58	Y+	A1/31	-1,33
Y-	A1/37	-2,52	Y-	A1/37	-2,34	Y-	A1/37	-1,54	Y-	A1/37	-1,29
398	A1/1	-2,33	399	A1/1	-2,35	400	A1/1	-2,73	401	A1/1	-2,01
	A1/2	-2,24		A1/2	-2,27		A1/2	-2,64		A1/2	-1,94
	A1/3	-2,33		A1/3	-2,35		A1/3	-2,73		A1/3	-2,02
	A1/4	-2,24		A1/4	-2,27		A1/4	-2,64		A1/4	-1,95
	A1/5	-2,22		A1/5	-2,24		A1/5	-2,59		A1/5	-1,91
	A1/6	-2,33		A1/6	-2,35		A1/6	-2,73		A1/6	-2,01
	A1/7	-2,24		A1/7	-2,27		A1/7	-2,64		A1/7	-1,94
	A1/8	-2,22		A1/8	-2,23		A1/8	-2,58		A1/8	-1,90
	A1/9	-2,32		A1/9	-2,35		A1/9	-2,72		A1/9	-2,01
	A1/10	-2,24		A1/10	-2,26		A1/10	-2,63		A1/10	-1,94
	A1/11	-2,21		A1/11	-2,23		A1/11	-2,58		A1/11	-1,91
	A1/12	-2,33		A1/12	-2,35		A1/12	-2,73		A1/12	-2,02
	A1/13	-2,24		A1/13	-2,27		A1/13	-2,64		A1/13	-1,95
	A1/14	-2,21		A1/14	-2,23		A1/14	-2,59		A1/14	-1,92
X+	A1/15	-1,56	X+	A1/21	-1,56	X+	A1/21	-1,79	X+	A1/20	-1,32
X-	A1/24	-1,51	X-	A1/30	-1,50	X-	A1/30	-1,71	X-	A1/27	-1,29
Y+	A1/31	-1,55	Y+	A1/31	-1,52	Y+	A1/31	-1,76	Y+	A1/34	-1,27
Y-	A1/37	-1,52	Y-	A1/37	-1,54	Y-	A1/37	-1,77	Y-	A1/36	-1,33
402	A1/1	-1,67	403	A1/1	-2,45	404	A1/1	-3,03	405	A1/1	-3,05
	A1/2	-1,62		A1/2	-2,39		A1/2	-2,95		A1/2	-2,96
	A1/3	-1,67		A1/3	-2,46		A1/3	-3,04		A1/3	-3,06
	A1/4	-1,62		A1/4	-2,40		A1/4	-2,96		A1/4	-2,97
	A1/5	-1,58		A1/5	-2,36		A1/5	-2,91		A1/5	-2,93
	A1/6	-1,67		A1/6	-2,45		A1/6	-3,04		A1/6	-3,05
	A1/7	-1,61		A1/7	-2,39		A1/7	-2,95		A1/7	-2,96
	A1/8	-1,58		A1/8	-2,35		A1/8	-2,90		A1/8	-2,91
	A1/9	-1,67		A1/9	-2,45		A1/9	-3,02		A1/9	-3,04
	A1/10	-1,62		A1/10	-2,39		A1/10	-2,94		A1/10	-2,95
	A1/11	-1,58		A1/11	-2,34		A1/11	-2,89		A1/11	-2,89
	A1/12	-1,67		A1/12	-2,45		A1/12	-3,03		A1/12	-3,05
	A1/13	-1,62		A1/13	-2,39		A1/13	-2,95		A1/13	-2,96

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/14	-1,59		A1/14	-2,35		A1/14	-2,89		A1/14	-2,91
X+	A1/20	-1,08	X+	A1/15	-1,67	X+	A1/15	-2,09	X+	A1/15	-2,11
X-	A1/27	-1,06	X-	A1/24	-1,57	X-	A1/24	-1,92	X-	A1/24	-1,89
Y+	A1/34	-1,04	Y+	A1/31	-1,63	Y+	A1/31	-2,04	Y+	A1/31	-2,04
Y-	A1/36	-1,09	Y-	A1/37	-1,63	Y-	A1/37	-2,00	Y-	A1/37	-2,04
406	A1/1	-2,59	407	A1/1	-3,14	408	A1/1	-2,85	409	A1/1	-2,53
	A1/2	-2,53		A1/2	-3,05		A1/2	-2,77		A1/2	-2,46
	A1/3	-2,60		A1/3	-3,15		A1/3	-2,86		A1/3	-2,53
	A1/4	-2,53		A1/4	-3,06		A1/4	-2,77		A1/4	-2,47
	A1/5	-2,49		A1/5	-3,01		A1/5	-2,73		A1/5	-2,43
	A1/6	-2,59		A1/6	-3,15		A1/6	-2,86		A1/6	-2,53
	A1/7	-2,53		A1/7	-3,05		A1/7	-2,77		A1/7	-2,46
	A1/8	-2,48		A1/8	-3,00		A1/8	-2,73		A1/8	-2,42
	A1/9	-2,59		A1/9	-3,13		A1/9	-2,84		A1/9	-2,52
	A1/10	-2,52		A1/10	-3,04		A1/10	-2,76		A1/10	-2,45
	A1/11	-2,47		A1/11	-2,98		A1/11	-2,71		A1/11	-2,40
	A1/12	-2,59		A1/12	-3,14		A1/12	-2,84		A1/12	-2,52
	A1/13	-2,53		A1/13	-3,04		A1/13	-2,76		A1/13	-2,45
	A1/14	-2,48		A1/14	-2,99		A1/14	-2,71		A1/14	-2,41
X+	A1/21	-1,77	X+	A1/15	-2,16	X+	A1/15	-1,95	X+	A1/15	-1,76
X-	A1/30	-1,65	X-	A1/24	-1,97	X-	A1/24	-1,82	X-	A1/24	-1,58
Y+	A1/31	-1,72	Y+	A1/31	-2,12	Y+	A1/31	-1,94	Y+	A1/31	-1,72
Y-	A1/37	-1,73	Y-	A1/37	-2,05	Y-	A1/37	-1,84	Y-	A1/37	-1,65
410	A1/1	-2,41	411	A1/1	-2,02	412	A1/1	-1,72	413	A1/1	-1,98
	A1/2	-2,34		A1/2	-1,97		A1/2	-1,67		A1/2	-1,93
	A1/3	-2,41		A1/3	-2,02		A1/3	-1,72		A1/3	-1,99
	A1/4	-2,34		A1/4	-1,97		A1/4	-1,68		A1/4	-1,94
	A1/5	-2,31		A1/5	-1,94		A1/5	-1,65		A1/5	-1,91
	A1/6	-2,41		A1/6	-2,02		A1/6	-1,72		A1/6	-1,99
	A1/7	-2,35		A1/7	-1,97		A1/7	-1,68		A1/7	-1,93
	A1/8	-2,31		A1/8	-1,93		A1/8	-1,65		A1/8	-1,91
	A1/9	-2,40		A1/9	-2,01		A1/9	-1,71		A1/9	-1,98
	A1/10	-2,33		A1/10	-1,96		A1/10	-1,67		A1/10	-1,92
	A1/11	-2,29		A1/11	-1,92		A1/11	-1,63		A1/11	-1,88
	A1/12	-2,40		A1/12	-2,01		A1/12	-1,71		A1/12	-1,98
	A1/13	-2,33		A1/13	-1,96		A1/13	-1,67		A1/13	-1,92
	A1/14	-2,29		A1/14	-1,92		A1/14	-1,63		A1/14	-1,89
X+	A1/15	-1,65	X+	A1/15	-1,38	X+	A1/15	-1,18	X+	A1/15	-1,39
X-	A1/24	-1,55	X-	A1/24	-1,28	X-	A1/24	-1,09	X-	A1/24	-1,24
Y+	A1/31	-1,66	Y+	A1/31	-1,35	Y+	A1/31	-1,17	Y+	A1/31	-1,37
Y-	A1/37	-1,55	Y-	A1/37	-1,33	Y-	A1/37	-1,10	Y-	A1/37	-1,28
414	A1/1	-2,65	415	A1/1	-1,99	416	A1/1	-3,20	417	A1/1	-2,94
	A1/2	-2,57		A1/2	-1,94		A1/2	-3,10		A1/2	-2,85
	A1/3	-2,65		A1/3	-2,00		A1/3	-3,20		A1/3	-2,94
	A1/4	-2,57		A1/4	-1,94		A1/4	-3,11		A1/4	-2,85
	A1/5	-2,54		A1/5	-1,91		A1/5	-3,05		A1/5	-2,81
	A1/6	-2,66		A1/6	-2,00		A1/6	-3,21		A1/6	-2,95
	A1/7	-2,57		A1/7	-1,94		A1/7	-3,12		A1/7	-2,87
	A1/8	-2,54		A1/8	-1,91		A1/8	-3,06		A1/8	-2,82
	A1/9	-2,64		A1/9	-1,99		A1/9	-3,19		A1/9	-2,93
	A1/10	-2,56		A1/10	-1,93		A1/10	-3,10		A1/10	-2,85
	A1/11	-2,52		A1/11	-1,90		A1/11	-3,03		A1/11	-2,80
	A1/12	-2,64		A1/12	-1,99		A1/12	-3,19		A1/12	-2,92
	A1/13	-2,56		A1/13	-1,93		A1/13	-3,09		A1/13	-2,84
	A1/14	-2,52		A1/14	-1,89		A1/14	-3,02		A1/14	-2,78
X+	A1/15	-1,81	X+	A1/15	-1,35	X+	A1/15	-2,15	X+	A1/15	-1,98
X-	A1/24	-1,70	X-	A1/24	-1,29	X-	A1/24	-2,05	X-	A1/24	-1,92
Y+	A1/31	-1,81	Y+	A1/31	-1,37	Y+	A1/31	-2,18	Y+	A1/31	-2,03
Y-	A1/37	-1,70	Y-	A1/37	-1,25	Y-	A1/37	-2,00	Y-	A1/37	-1,83
418	A1/1	-2,62	419	A1/1	-2,88	420	A1/1	-2,54	421	A1/1	-2,58
	A1/2	-2,55		A1/2	-2,80		A1/2	-2,48		A1/2	-2,52
	A1/3	-2,62		A1/3	-2,88		A1/3	-2,54		A1/3	-2,58
	A1/4	-2,55		A1/4	-2,80		A1/4	-2,48		A1/4	-2,52
	A1/5	-2,50		A1/5	-2,74		A1/5	-2,43		A1/5	-2,47
	A1/6	-2,63		A1/6	-2,90		A1/6	-2,55		A1/6	-2,59
	A1/7	-2,56		A1/7	-2,82		A1/7	-2,49		A1/7	-2,53
	A1/8	-2,52		A1/8	-2,77		A1/8	-2,45		A1/8	-2,49
	A1/9	-2,61		A1/9	-2,88		A1/9	-2,54		A1/9	-2,58
	A1/10	-2,55		A1/10	-2,80		A1/10	-2,48		A1/10	-2,52
	A1/11	-2,49		A1/11	-2,73		A1/11	-2,44		A1/11	-2,47
	A1/12	-2,60		A1/12	-2,86		A1/12	-2,53		A1/12	-2,56
	A1/13	-2,53		A1/13	-2,78		A1/13	-2,47		A1/13	-2,50
	A1/14	-2,47		A1/14	-2,70		A1/14	-2,42		A1/14	-2,45
X+	A1/15	-1,76	X+	A1/15	-1,92	X+	A1/15	-1,70	X+	A1/15	-1,73
X-	A1/24	-1,74	X-	A1/24	-1,87	X-	A1/24	-1,71	X-	A1/24	-1,74
Y+	A1/31	-1,84	Y+	A1/31	-2,01	Y+	A1/40	-1,76	Y+	A1/40	-1,81
Y-	A1/37	-1,58	Y-	A1/37	-1,71	Y-	A1/46	-1,60	Y-	A1/46	-1,61

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
422	A1/1	-1,93	423	A1/1	-2,11	424	A1/1	-2,98	425	A1/1	-2,63
	A1/2	-1,87		A1/2	-2,05		A1/2	-2,90		A1/2	-2,55
	A1/3	-1,93		A1/3	-2,11		A1/3	-2,98		A1/3	-2,63
	A1/4	-1,88		A1/4	-2,05		A1/4	-2,90		A1/4	-2,55
	A1/5	-1,85		A1/5	-2,02		A1/5	-2,86		A1/5	-2,52
	A1/6	-1,93		A1/6	-2,12		A1/6	-2,99		A1/6	-2,64
	A1/7	-1,88		A1/7	-2,06		A1/7	-2,91		A1/7	-2,55
	A1/8	-1,85		A1/8	-2,04		A1/8	-2,87		A1/8	-2,53
	A1/9	-1,92		A1/9	-2,11		A1/9	-2,98		A1/9	-2,63
	A1/10	-1,87		A1/10	-2,06		A1/10	-2,90		A1/10	-2,54
	A1/11	-1,84		A1/11	-2,02		A1/11	-2,86		A1/11	-2,51
	A1/12	-1,92		A1/12	-2,10		A1/12	-2,98		A1/12	-2,62
	A1/13	-1,87		A1/13	-2,05		A1/13	-2,89		A1/13	-2,54
	A1/14	-1,84		A1/14	-2,01		A1/14	-2,85		A1/14	-2,51
	X+ A1/15	-1,32		X+ A1/15	-1,41		X+ A1/15	-2,00		X+ A1/15	-1,78
	X- A1/24	-1,25		X- A1/24	-1,43		X- A1/24	-2,01		X- A1/24	-1,72
	Y+ A1/31	-1,33		Y+ A1/40	-1,46		Y+ A1/40	-2,04		Y+ A1/31	-1,79
	Y- A1/37	-1,24		Y- A1/46	-1,35		Y- A1/46	-1,94		Y- A1/37	-1,71
426	A1/1	-3,57	427	A1/1	-2,63	428	A1/1	-2,03	429	A1/1	-2,64
	A1/2	-3,49		A1/2	-2,57		A1/2	-1,98		A1/2	-2,56
	A1/3	-3,57		A1/3	-2,63		A1/3	-2,04		A1/3	-2,64
	A1/4	-3,49		A1/4	-2,58		A1/4	-1,98		A1/4	-2,56
	A1/5	-3,43		A1/5	-2,53		A1/5	-1,95		A1/5	-2,53
	A1/6	-3,53		A1/6	-2,61		A1/6	-2,04		A1/6	-2,64
	A1/7	-3,46		A1/7	-2,56		A1/7	-1,98		A1/7	-2,56
	A1/8	-3,38		A1/8	-2,49		A1/8	-1,95		A1/8	-2,52
	A1/9	-3,56		A1/9	-2,62		A1/9	-2,03		A1/9	-2,64
	A1/10	-3,49		A1/10	-2,57		A1/10	-1,98		A1/10	-2,56
	A1/11	-3,43		A1/11	-2,52		A1/11	-1,95		A1/11	-2,53
	A1/12	-3,60		A1/12	-2,64		A1/12	-2,03		A1/12	-2,64
	A1/13	-3,52		A1/13	-2,59		A1/13	-1,97		A1/13	-2,56
	A1/14	-3,48		A1/14	-2,55		A1/14	-1,94		A1/14	-2,53
	X+ A1/20	-2,49		X+ A1/20	-1,81		X+ A1/15	-1,37		X+ A1/21	-1,77
	X- A1/27	-2,44		X- A1/27	-1,76		X- A1/24	-1,35		X- A1/30	-1,75
	Y+ A1/34	-2,16		Y+ A1/34	-1,62		Y+ A1/31	-1,38		Y+ A1/31	-1,74
	Y- A1/36	-2,64		Y- A1/36	-1,89		Y- A1/37	-1,33		Y- A1/37	-1,77
430	A1/1	-2,51	431	A1/1	-3,50	432	A1/1	-2,20	433	A1/1	-1,71
	A1/2	-2,43		A1/2	-3,42		A1/2	-2,11		A1/2	-1,65
	A1/3	-2,51		A1/3	-3,50		A1/3	-2,20		A1/3	-1,71
	A1/4	-2,43		A1/4	-3,42		A1/4	-2,11		A1/4	-1,65
	A1/5	-2,41		A1/5	-3,38		A1/5	-2,09		A1/5	-1,63
	A1/6	-2,50		A1/6	-3,46		A1/6	-2,20		A1/6	-1,71
	A1/7	-2,42		A1/7	-3,38		A1/7	-2,12		A1/7	-1,65
	A1/8	-2,39		A1/8	-3,31		A1/8	-2,10		A1/8	-1,63
	A1/9	-2,51		A1/9	-3,50		A1/9	-2,20		A1/9	-1,71
	A1/10	-2,43		A1/10	-3,42		A1/10	-2,11		A1/10	-1,65
	A1/11	-2,41		A1/11	-3,37		A1/11	-2,09		A1/11	-1,62
	A1/12	-2,52		A1/12	-3,54		A1/12	-2,19		A1/12	-1,70
	A1/13	-2,43		A1/13	-3,46		A1/13	-2,11		A1/13	-1,64
	A1/14	-2,42		A1/14	-3,44		A1/14	-2,08		A1/14	-1,62
	X+ A1/20	-1,70		X+ A1/20	-2,47		X+ A1/15	-1,46		X+ A1/15	-1,13
	X- A1/27	-1,70		X- A1/27	-2,45		X- A1/24	-1,45		X- A1/24	-1,12
	Y+ A1/41	-1,62		Y+ A1/34	-2,09		Y+ A1/31	-1,48		Y+ A1/31	-1,14
	Y- A1/43	-1,74		Y- A1/36	-2,67		Y- A1/37	-1,40		Y- A1/37	-1,10
434	A1/1	-1,71	435	A1/1	-2,18	436	A1/1	-1,52	437	A1/1	-2,22
	A1/2	-1,65		A1/2	-2,09		A1/2	-1,47		A1/2	-2,14
	A1/3	-1,72		A1/3	-2,18		A1/3	-1,52		A1/3	-2,22
	A1/4	-1,66		A1/4	-2,09		A1/4	-1,47		A1/4	-2,14
	A1/5	-1,63		A1/5	-2,07		A1/5	-1,44		A1/5	-2,10
	A1/6	-1,71		A1/6	-2,18		A1/6	-1,52		A1/6	-2,22
	A1/7	-1,65		A1/7	-2,10		A1/7	-1,47		A1/7	-2,14
	A1/8	-1,62		A1/8	-2,07		A1/8	-1,43		A1/8	-2,10
	A1/9	-1,71		A1/9	-2,18		A1/9	-1,52		A1/9	-2,22
	A1/10	-1,65		A1/10	-2,09		A1/10	-1,47		A1/10	-2,14
	A1/11	-1,62		A1/11	-2,06		A1/11	-1,44		A1/11	-2,10
	A1/12	-1,72		A1/12	-2,18		A1/12	-1,53		A1/12	-2,22
	A1/13	-1,66		A1/13	-2,09		A1/13	-1,48		A1/13	-2,14
	A1/14	-1,63		A1/14	-2,06		A1/14	-1,44		A1/14	-2,10
	X+ A1/20	-1,12		X+ A1/15	-1,42		X+ A1/20	-0,98		X+ A1/15	-1,44
	X- A1/27	-1,09		X- A1/24	-1,40		X- A1/27	-0,95		X- A1/24	-1,40
	Y+ A1/34	-1,07		Y+ A1/31	-1,42		Y+ A1/34	-0,94		Y+ A1/31	-1,43
	Y- A1/36	-1,13		Y- A1/37	-1,40		Y- A1/36	-0,99		Y- A1/37	-1,42
438	A1/1	-2,08	439	A1/1	-2,10	440	A1/1	-2,67	441	A1/1	-2,17
	A1/2	-2,00		A1/2	-2,02		A1/2	-2,59		A1/2	-2,09
	A1/3	-2,08		A1/3	-2,10		A1/3	-2,68		A1/3	-2,17
	A1/4	-2,00		A1/4	-2,02		A1/4	-2,59		A1/4	-2,09
	A1/5	-1,98		A1/5	-2,00		A1/5	-2,57		A1/5	-2,08
	A1/6	-2,09		A1/6	-2,11		A1/6	-2,66		A1/6	-2,18

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/7	-2,00		A1/7	-2,02		A1/7	-2,57		A1/7	-2,09
	A1/8	-1,99		A1/8	-2,01		A1/8	-2,54		A1/8	-2,08
	A1/9	-2,08		A1/9	-2,10		A1/9	-2,67		A1/9	-2,17
	A1/10	-2,00		A1/10	-2,02		A1/10	-2,59		A1/10	-2,09
	A1/11	-1,99		A1/11	-2,00		A1/11	-2,57		A1/11	-2,08
	A1/12	-2,08		A1/12	-2,10		A1/12	-2,69		A1/12	-2,17
	A1/13	-1,99		A1/13	-2,01		A1/13	-2,61		A1/13	-2,08
	A1/14	-1,98		A1/14	-1,99		A1/14	-2,59		A1/14	-2,07
X+	A1/15	-1,38	X+	A1/15	-1,39	X+	A1/20	-1,85	X+	A1/15	-1,45
X-	A1/24	-1,39	X-	A1/24	-1,39	X-	A1/27	-1,83	X-	A1/24	-1,45
Y+	A1/40	-1,41	Y+	A1/40	-1,42	Y+	A1/34	-1,69	Y+	A1/40	-1,47
Y-	A1/46	-1,34	Y-	A1/46	-1,33	Y-	A1/36	-1,92	Y-	A1/46	-1,42
442	A1/1	-2,11	443	A1/1	-2,25	444	A1/1	-3,76	445	A1/1	-3,28
	A1/2	-2,03		A1/2	-2,16		A1/2	-3,68		A1/2	-3,19
	A1/3	-2,11		A1/3	-2,25		A1/3	-3,76		A1/3	-3,28
	A1/4	-2,03		A1/4	-2,16		A1/4	-3,69		A1/4	-3,20
	A1/5	-2,00		A1/5	-2,14		A1/5	-3,64		A1/5	-3,17
	A1/6	-2,11		A1/6	-2,25		A1/6	-3,71		A1/6	-3,25
	A1/7	-2,04		A1/7	-2,17		A1/7	-3,63		A1/7	-3,17
	A1/8	-2,01		A1/8	-2,16		A1/8	-3,54		A1/8	-3,12
	A1/9	-2,11		A1/9	-2,25		A1/9	-3,76		A1/9	-3,28
	A1/10	-2,03		A1/10	-2,16		A1/10	-3,68		A1/10	-3,19
	A1/11	-2,00		A1/11	-2,14		A1/11	-3,63		A1/11	-3,15
	A1/12	-2,11		A1/12	-2,24		A1/12	-3,82		A1/12	-3,31
	A1/13	-2,03		A1/13	-2,15		A1/13	-3,74		A1/13	-3,22
	A1/14	-2,00		A1/14	-2,13		A1/14	-3,72		A1/14	-3,20
X+	A1/15	-1,38	X+	A1/15	-1,50	X+	A1/20	-2,71	X+	A1/20	-2,33
X-	A1/24	-1,37	X-	A1/24	-1,51	X-	A1/27	-2,67	X-	A1/27	-2,24
Y+	A1/31	-1,40	Y+	A1/40	-1,55	Y+	A1/34	-2,19	Y+	A1/34	-2,04
Y-	A1/37	-1,34	Y-	A1/46	-1,43	Y-	A1/36	-2,98	Y-	A1/36	-2,44
446	A1/1	-4,80	447	A1/1	-2,57	448	A1/1	-2,46	449	A1/1	-2,73
	A1/2	-4,71		A1/2	-2,48		A1/2	-2,39		A1/2	-2,64
	A1/3	-4,80		A1/3	-2,57		A1/3	-2,46		A1/3	-2,73
	A1/4	-4,72		A1/4	-2,48		A1/4	-2,39		A1/4	-2,64
	A1/5	-4,65		A1/5	-2,46		A1/5	-2,35		A1/5	-2,61
	A1/6	-4,71		A1/6	-2,57		A1/6	-2,47		A1/6	-2,74
	A1/7	-4,63		A1/7	-2,48		A1/7	-2,39		A1/7	-2,65
	A1/8	-4,50		A1/8	-2,46		A1/8	-2,36		A1/8	-2,63
	A1/9	-4,79		A1/9	-2,57		A1/9	-2,46		A1/9	-2,73
	A1/10	-4,71		A1/10	-2,47		A1/10	-2,38		A1/10	-2,64
	A1/11	-4,63		A1/11	-2,46		A1/11	-2,35		A1/11	-2,61
	A1/12	-4,88		A1/12	-2,57		A1/12	-2,45		A1/12	-2,72
	A1/13	-4,80		A1/13	-2,48		A1/13	-2,38		A1/13	-2,63
	A1/14	-4,78		A1/14	-2,46		A1/14	-2,34		A1/14	-2,60
X+	A1/20	-3,57	X+	A1/15	-1,74	X+	A1/15	-1,64	X+	A1/15	-1,85
X-	A1/27	-3,39	X-	A1/24	-1,70	X-	A1/24	-1,64	X-	A1/24	-1,83
Y+	A1/34	-2,72	Y+	A1/31	-1,73	Y+	A1/31	-1,68	Y+	A1/31	-1,89
Y-	A1/36	-3,94	Y-	A1/37	-1,72	Y-	A1/37	-1,58	Y-	A1/37	-1,76
450	A1/1	-3,15	451	A1/1	-3,10	452	A1/1	-2,84	453	A1/1	-2,49
	A1/2	-3,07		A1/2	-3,02		A1/2	-2,76		A1/2	-2,42
	A1/3	-3,15		A1/3	-3,10		A1/3	-2,85		A1/3	-2,49
	A1/4	-3,07		A1/4	-3,02		A1/4	-2,76		A1/4	-2,42
	A1/5	-3,02		A1/5	-2,97		A1/5	-2,71		A1/5	-2,37
	A1/6	-3,16		A1/6	-3,12		A1/6	-2,86		A1/6	-2,51
	A1/7	-3,08		A1/7	-3,04		A1/7	-2,77		A1/7	-2,44
	A1/8	-3,04		A1/8	-3,00		A1/8	-2,73		A1/8	-2,39
	A1/9	-3,14		A1/9	-3,10		A1/9	-2,84		A1/9	-2,49
	A1/10	-3,07		A1/10	-3,02		A1/10	-2,76		A1/10	-2,42
	A1/11	-3,02		A1/11	-2,96		A1/11	-2,70		A1/11	-2,36
	A1/12	-3,14		A1/12	-3,09		A1/12	-2,83		A1/12	-2,47
	A1/13	-3,06		A1/13	-3,00		A1/13	-2,74		A1/13	-2,40
	A1/14	-3,01		A1/14	-2,94		A1/14	-2,68		A1/14	-2,33
X+	A1/15	-2,14	X+	A1/15	-2,10	X+	A1/15	-1,89	X+	A1/15	-1,66
X-	A1/24	-2,11	X-	A1/24	-2,06	X-	A1/24	-1,85	X-	A1/24	-1,62
Y+	A1/31	-2,18	Y+	A1/31	-2,18	Y+	A1/31	-1,95	Y+	A1/31	-1,75
Y-	A1/37	-2,04	Y-	A1/37	-1,93	Y-	A1/37	-1,74	Y-	A1/37	-1,46
454	A1/1	-2,18	455	A1/1	-3,07	456	A1/1	-3,06	457	A1/1	-1,88
	A1/2	-2,12		A1/2	-2,99		A1/2	-2,96		A1/2	-1,84
	A1/3	-2,18		A1/3	-3,08		A1/3	-3,06		A1/3	-1,88
	A1/4	-2,13		A1/4	-3,00		A1/4	-2,96		A1/4	-1,84
	A1/5	-2,08		A1/5	-2,95		A1/5	-2,92		A1/5	-1,81
	A1/6	-2,19		A1/6	-3,09		A1/6	-3,07		A1/6	-1,89
	A1/7	-2,14		A1/7	-3,01		A1/7	-2,97		A1/7	-1,85
	A1/8	-2,10		A1/8	-2,98		A1/8	-2,93		A1/8	-1,82
	A1/9	-2,18		A1/9	-3,07		A1/9	-3,06		A1/9	-1,88
	A1/10	-2,12		A1/10	-2,99		A1/10	-2,96		A1/10	-1,84
	A1/11	-2,08		A1/11	-2,95		A1/11	-2,91		A1/11	-1,80
	A1/12	-2,16		A1/12	-3,06		A1/12	-3,05		A1/12	-1,87

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/13	-2,11		A1/13	-2,98		A1/13	-2,95		A1/13	-1,83
	A1/14	-2,06		A1/14	-2,92		A1/14	-2,90		A1/14	-1,79
X+	A1/15	-1,47	X+	A1/15	-2,11	X+	A1/15	-2,04	X+	A1/15	-1,28
X-	A1/24	-1,45	X-	A1/24	-2,06	X-	A1/24	-2,01	X-	A1/24	-1,25
Y+	A1/31	-1,54	Y+	A1/31	-2,18	Y+	A1/31	-2,08	Y+	A1/31	-1,32
Y-	A1/37	-1,32	Y-	A1/37	-1,95	Y-	A1/37	-1,94	Y-	A1/37	-1,18
458	A1/1	-3,18	459	A1/1	-3,25	460	A1/1	-3,50	461	A1/1	-3,36
	A1/2	-3,11		A1/2	-3,18		A1/2	-3,41		A1/2	-3,28
	A1/3	-3,18		A1/3	-3,25		A1/3	-3,51		A1/3	-3,36
	A1/4	-3,12		A1/4	-3,19		A1/4	-3,41		A1/4	-3,28
	A1/5	-3,07		A1/5	-3,14		A1/5	-3,37		A1/5	-3,24
	A1/6	-3,20		A1/6	-3,27		A1/6	-3,52		A1/6	-3,38
	A1/7	-3,13		A1/7	-3,21		A1/7	-3,42		A1/7	-3,30
	A1/8	-3,09		A1/8	-3,17		A1/8	-3,38		A1/8	-3,27
	A1/9	-3,18		A1/9	-3,24		A1/9	-3,50		A1/9	-3,35
	A1/10	-3,11		A1/10	-3,18		A1/10	-3,41		A1/10	-3,27
	A1/11	-3,05		A1/11	-3,13		A1/11	-3,36		A1/11	-3,22
	A1/12	-3,16		A1/12	-3,23		A1/12	-3,49		A1/12	-3,34
	A1/13	-3,10		A1/13	-3,16		A1/13	-3,40		A1/13	-3,26
	A1/14	-3,03		A1/14	-3,10		A1/14	-3,34		A1/14	-3,20
X+	A1/15	-2,21	X+	A1/15	-2,31	X+	A1/15	-2,39	X+	A1/15	-2,38
X-	A1/24	-2,13	X-	A1/24	-2,22	X-	A1/24	-2,33	X-	A1/24	-2,26
Y+	A1/31	-2,28	Y+	A1/31	-2,39	Y+	A1/31	-2,44	Y+	A1/31	-2,45
Y-	A1/37	-2,02	Y-	A1/37	-2,06	Y-	A1/37	-2,26	Y-	A1/37	-2,13
462	A1/1	-4,13	463	A1/1	-4,09	464	A1/1	-3,54	465	A1/1	-4,46
	A1/2	-4,04		A1/2	-4,01		A1/2	-3,48		A1/2	-4,39
	A1/3	-4,13		A1/3	-4,10		A1/3	-3,55		A1/3	-4,48
	A1/4	-4,05		A1/4	-4,02		A1/4	-3,49		A1/4	-4,42
	A1/5	-3,99		A1/5	-3,97		A1/5	-3,44		A1/5	-4,37
	A1/6	-4,15		A1/6	-4,13		A1/6	-3,58		A1/6	-4,53
	A1/7	-4,06		A1/7	-4,05		A1/7	-3,52		A1/7	-4,46
	A1/8	-4,01		A1/8	-4,01		A1/8	-3,49		A1/8	-4,44
	A1/9	-4,12		A1/9	-4,07		A1/9	-3,53		A1/9	-4,44
	A1/10	-4,03		A1/10	-3,99		A1/10	-3,47		A1/10	-4,37
	A1/11	-3,96		A1/11	-3,93		A1/11	-3,42		A1/11	-4,29
	A1/12	-4,11		A1/12	-4,05		A1/12	-3,50		A1/12	-4,39
	A1/13	-4,02		A1/13	-3,97		A1/13	-3,44		A1/13	-4,33
	A1/14	-3,94		A1/14	-3,89		A1/14	-3,37		A1/14	-4,22
X+	A1/15	-2,90	X+	A1/15	-3,02	X+	A1/15	-2,60	X+	A1/15	-3,49
X-	A1/24	-2,75	X-	A1/24	-2,73	X-	A1/24	-2,44	X-	A1/24	-3,02
Y+	A1/31	-2,95	Y+	A1/31	-3,12	Y+	A1/31	-2,74	Y+	A1/31	-3,67
Y-	A1/37	-2,67	Y-	A1/37	-2,57	Y-	A1/37	-2,20	Y-	A1/37	-2,70
466	A1/1	-1,84	467	A1/1	-2,47	468	A1/1	-1,96	469	A1/1	-2,48
	A1/2	-1,78		A1/2	-2,39		A1/2	-1,90		A1/2	-2,39
	A1/3	-1,84		A1/3	-2,47		A1/3	-1,96		A1/3	-2,48
	A1/4	-1,78		A1/4	-2,39		A1/4	-1,90		A1/4	-2,39
	A1/5	-1,75		A1/5	-2,36		A1/5	-1,87		A1/5	-2,36
	A1/6	-1,84		A1/6	-2,48		A1/6	-1,96		A1/6	-2,48
	A1/7	-1,78		A1/7	-2,39		A1/7	-1,90		A1/7	-2,39
	A1/8	-1,76		A1/8	-2,36		A1/8	-1,87		A1/8	-2,35
	A1/9	-1,84		A1/9	-2,47		A1/9	-1,96		A1/9	-2,47
	A1/10	-1,78		A1/10	-2,38		A1/10	-1,90		A1/10	-2,39
	A1/11	-1,75		A1/11	-2,35		A1/11	-1,86		A1/11	-2,35
	A1/12	-1,83		A1/12	-2,47		A1/12	-1,96		A1/12	-2,48
	A1/13	-1,78		A1/13	-2,38		A1/13	-1,90		A1/13	-2,39
	A1/14	-1,74		A1/14	-2,35		A1/14	-1,86		A1/14	-2,35
X+	A1/15	-1,22	X+	A1/15	-1,65	X+	A1/15	-1,27	X+	A1/18	-1,63
X-	A1/24	-1,19	X-	A1/24	-1,60	X-	A1/24	-1,26	X-	A1/25	-1,59
Y+	A1/31	-1,23	Y+	A1/31	-1,66	Y+	A1/31	-1,27	Y+	A1/34	-1,62
Y-	A1/37	-1,17	Y-	A1/37	-1,59	Y-	A1/37	-1,26	Y-	A1/36	-1,61
470	A1/1	-2,48	471	A1/1	-2,71	472	A1/1	-2,50	473	A1/1	-2,71
	A1/2	-2,40		A1/2	-2,62		A1/2	-2,41		A1/2	-2,62
	A1/3	-2,49		A1/3	-2,71		A1/3	-2,50		A1/3	-2,71
	A1/4	-2,40		A1/4	-2,62		A1/4	-2,41		A1/4	-2,62
	A1/5	-2,38		A1/5	-2,58		A1/5	-2,38		A1/5	-2,58
	A1/6	-2,49		A1/6	-2,71		A1/6	-2,50		A1/6	-2,70
	A1/7	-2,40		A1/7	-2,62		A1/7	-2,41		A1/7	-2,62
	A1/8	-2,38		A1/8	-2,57		A1/8	-2,38		A1/8	-2,58
	A1/9	-2,48		A1/9	-2,71		A1/9	-2,49		A1/9	-2,71
	A1/10	-2,40		A1/10	-2,62		A1/10	-2,41		A1/10	-2,62
	A1/11	-2,37		A1/11	-2,56		A1/11	-2,38		A1/11	-2,58
	A1/12	-2,48		A1/12	-2,71		A1/12	-2,50		A1/12	-2,71
	A1/13	-2,40		A1/13	-2,62		A1/13	-2,41		A1/13	-2,62
	A1/14	-2,37		A1/14	-2,57		A1/14	-2,38		A1/14	-2,58
X+	A1/15	-1,66	X+	A1/20	-1,79	X+	A1/18	-1,64	X+	A1/20	-1,78
X-	A1/24	-1,63	X-	A1/27	-1,71	X-	A1/25	-1,64	X-	A1/27	-1,76
Y+	A1/31	-1,67	Y+	A1/34	-1,75	Y+	A1/34	-1,64	Y+	A1/34	-1,76
Y-	A1/37	-1,62	Y-	A1/36	-1,76	Y-	A1/36	-1,64	Y-	A1/36	-1,78

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
474	A1/1	-1,66	475	A1/1	-2,49	476	A1/1	-2,33	477	A1/1	-2,05
	A1/2	-1,61		A1/2	-2,41		A1/2	-2,25		A1/2	-1,98
	A1/3	-1,66		A1/3	-2,50		A1/3	-2,33		A1/3	-2,05
	A1/4	-1,61		A1/4	-2,41		A1/4	-2,25		A1/4	-1,98
	A1/5	-1,58		A1/5	-2,37		A1/5	-2,22		A1/5	-1,94
	A1/6	-1,66		A1/6	-2,49		A1/6	-2,33		A1/6	-2,05
	A1/7	-1,61		A1/7	-2,41		A1/7	-2,25		A1/7	-1,98
	A1/8	-1,58		A1/8	-2,37		A1/8	-2,22		A1/8	-1,94
	A1/9	-1,66		A1/9	-2,49		A1/9	-2,33		A1/9	-2,05
	A1/10	-1,61		A1/10	-2,41		A1/10	-2,25		A1/10	-1,98
	A1/11	-1,57		A1/11	-2,36		A1/11	-2,21		A1/11	-1,94
	A1/12	-1,66		A1/12	-2,49		A1/12	-2,33		A1/12	-2,05
	A1/13	-1,61		A1/13	-2,41		A1/13	-2,25		A1/13	-1,98
	A1/14	-1,57		A1/14	-2,36		A1/14	-2,22		A1/14	-1,94
X+	A1/18	-1,07	X+	A1/18	-1,65	X+	A1/20	-1,53	X+	A1/18	-1,32
X-	A1/25	-1,05	X-	A1/25	-1,57	X-	A1/27	-1,51	X-	A1/25	-1,32
Y+	A1/34	-1,07	Y+	A1/34	-1,62	Y+	A1/34	-1,52	Y+	A1/34	-1,33
Y-	A1/36	-1,05	Y-	A1/36	-1,61	Y-	A1/36	-1,52	Y-	A1/36	-1,32
478	A1/1	-2,04	479	A1/1	-2,91	480	A1/1	-2,97	481	A1/1	-3,32
	A1/2	-1,98		A1/2	-2,83		A1/2	-2,89		A1/2	-3,25
	A1/3	-2,04		A1/3	-2,91		A1/3	-2,97		A1/3	-3,32
	A1/4	-1,98		A1/4	-2,83		A1/4	-2,88		A1/4	-3,25
	A1/5	-1,94		A1/5	-2,80		A1/5	-2,84		A1/5	-3,20
	A1/6	-2,04		A1/6	-2,92		A1/6	-2,97		A1/6	-3,32
	A1/7	-1,98		A1/7	-2,83		A1/7	-2,88		A1/7	-3,25
	A1/8	-1,93		A1/8	-2,80		A1/8	-2,84		A1/8	-3,20
	A1/9	-2,04		A1/9	-2,91		A1/9	-2,97		A1/9	-3,32
	A1/10	-1,98		A1/10	-2,83		A1/10	-2,89		A1/10	-3,25
	A1/11	-1,93		A1/11	-2,80		A1/11	-2,85		A1/11	-3,20
	A1/12	-2,05		A1/12	-2,91		A1/12	-2,97		A1/12	-3,31
	A1/13	-1,98		A1/13	-2,83		A1/13	-2,89		A1/13	-3,25
	A1/14	-1,94		A1/14	-2,79		A1/14	-2,85		A1/14	-3,19
X+	A1/20	-1,32	X+	A1/15	-1,95	X+	A1/20	-1,97	X+	A1/15	-2,23
X-	A1/27	-1,29	X-	A1/24	-1,95	X-	A1/27	-1,99	X-	A1/24	-2,24
Y+	A1/34	-1,29	Y+	A1/40	-1,96	Y+	A1/41	-1,96	Y+	A1/40	-2,24
Y-	A1/36	-1,32	Y-	A1/46	-1,93	Y-	A1/43	-1,99	Y-	A1/46	-2,22
482	A1/1	-3,21	483	A1/1	-2,13	484	A1/1	-3,47	485	A1/1	-3,82
	A1/2	-3,15		A1/2	-2,08		A1/2	-3,40		A1/2	-3,74
	A1/3	-3,21		A1/3	-2,13		A1/3	-3,47		A1/3	-3,81
	A1/4	-3,15		A1/4	-2,08		A1/4	-3,40		A1/4	-3,74
	A1/5	-3,09		A1/5	-2,04		A1/5	-3,33		A1/5	-3,66
	A1/6	-3,22		A1/6	-2,14		A1/6	-3,46		A1/6	-3,81
	A1/7	-3,16		A1/7	-2,09		A1/7	-3,39		A1/7	-3,73
	A1/8	-3,11		A1/8	-2,06		A1/8	-3,33		A1/8	-3,65
	A1/9	-3,21		A1/9	-2,13		A1/9	-3,47		A1/9	-3,82
	A1/10	-3,15		A1/10	-2,08		A1/10	-3,40		A1/10	-3,75
	A1/11	-3,10		A1/11	-2,05		A1/11	-3,34		A1/11	-3,67
	A1/12	-3,20		A1/12	-2,12		A1/12	-3,47		A1/12	-3,83
	A1/13	-3,14		A1/13	-2,07		A1/13	-3,40		A1/13	-3,75
	A1/14	-3,08		A1/14	-2,03		A1/14	-3,35		A1/14	-3,68
X+	A1/15	-2,17	X+	A1/15	-1,43	X+	A1/20	-2,32	X+	A1/20	-2,53
X-	A1/24	-2,19	X-	A1/24	-1,46	X-	A1/27	-2,34	X-	A1/27	-2,58
Y+	A1/40	-2,23	Y+	A1/40	-1,50	Y+	A1/41	-2,28	Y+	A1/41	-2,46
Y-	A1/46	-2,10	Y-	A1/46	-1,36	Y-	A1/43	-2,37	Y-	A1/43	-2,61
486	A1/1	-3,18	487	A1/1	-2,48	488	A1/1	-2,35	489	A1/1	-2,38
	A1/2	-3,09		A1/2	-2,40		A1/2	-2,27		A1/2	-2,30
	A1/3	-3,17		A1/3	-2,48		A1/3	-2,35		A1/3	-2,38
	A1/4	-3,09		A1/4	-2,40		A1/4	-2,27		A1/4	-2,30
	A1/5	-3,04		A1/5	-2,36		A1/5	-2,24		A1/5	-2,28
	A1/6	-3,17		A1/6	-2,48		A1/6	-2,35		A1/6	-2,38
	A1/7	-3,09		A1/7	-2,39		A1/7	-2,27		A1/7	-2,30
	A1/8	-3,04		A1/8	-2,36		A1/8	-2,24		A1/8	-2,27
	A1/9	-3,18		A1/9	-2,48		A1/9	-2,35		A1/9	-2,38
	A1/10	-3,10		A1/10	-2,40		A1/10	-2,27		A1/10	-2,30
	A1/11	-3,05		A1/11	-2,36		A1/11	-2,24		A1/11	-2,27
	A1/12	-3,18		A1/12	-2,48		A1/12	-2,35		A1/12	-2,38
	A1/13	-3,10		A1/13	-2,40		A1/13	-2,27		A1/13	-2,30
	A1/14	-3,05		A1/14	-2,36		A1/14	-2,25		A1/14	-2,28
X+	A1/21	-2,07	X+	A1/20	-1,63	X+	A1/20	-1,55	X+	A1/20	-1,58
X-	A1/30	-2,15	X-	A1/27	-1,61	X-	A1/27	-1,55	X-	A1/27	-1,57
Y+	A1/40	-2,08	Y+	A1/34	-1,61	Y+	A1/34	-1,54	Y+	A1/34	-1,57
Y-	A1/46	-2,15	Y-	A1/36	-1,63	Y-	A1/36	-1,55	Y-	A1/36	-1,58
490	A1/1	-1,84	491	A1/1	-2,78	492	A1/1	-2,27	493	A1/1	-2,38
	A1/2	-1,78		A1/2	-2,70		A1/2	-2,21		A1/2	-2,29
	A1/3	-1,84		A1/3	-2,78		A1/3	-2,27		A1/3	-2,38
	A1/4	-1,78		A1/4	-2,70		A1/4	-2,21		A1/4	-2,29
	A1/5	-1,76		A1/5	-2,67		A1/5	-2,17		A1/5	-2,27

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/6	-1,84		A1/6	-2,78		A1/6	-2,27		A1/6	-2,38
	A1/7	-1,78		A1/7	-2,70		A1/7	-2,21		A1/7	-2,29
	A1/8	-1,75		A1/8	-2,66		A1/8	-2,17		A1/8	-2,27
	A1/9	-1,84		A1/9	-2,78		A1/9	-2,26		A1/9	-2,38
	A1/10	-1,78		A1/10	-2,70		A1/10	-2,21		A1/10	-2,29
	A1/11	-1,76		A1/11	-2,66		A1/11	-2,17		A1/11	-2,27
	A1/12	-1,84		A1/12	-2,78		A1/12	-2,27		A1/12	-2,38
	A1/13	-1,78		A1/13	-2,70		A1/13	-2,21		A1/13	-2,29
	A1/14	-1,76		A1/14	-2,66		A1/14	-2,17		A1/14	-2,27
X+	A1/20	-1,21	X+	A1/18	-1,86	X+	A1/20	-1,51	X+	A1/20	-1,58
X-	A1/27	-1,21	X-	A1/25	-1,84	X-	A1/27	-1,49	X-	A1/27	-1,57
Y+	A1/34	-1,20	Y+	A1/34	-1,85	Y+	A1/34	-1,50	Y+	A1/34	-1,57
Y-	A1/36	-1,22	Y-	A1/36	-1,84	Y-	A1/36	-1,51	Y-	A1/36	-1,58
494	A1/1	-2,37	495	A1/1	-3,15	496	A1/1	-2,64	497	A1/1	-2,56
	A1/2	-2,32		A1/2	-3,07		A1/2	-2,56		A1/2	-2,48
	A1/3	-2,37		A1/3	-3,15		A1/3	-2,64		A1/3	-2,56
	A1/4	-2,32		A1/4	-3,07		A1/4	-2,56		A1/4	-2,48
	A1/5	-2,28		A1/5	-3,03		A1/5	-2,53		A1/5	-2,45
	A1/6	-2,37		A1/6	-3,15		A1/6	-2,64		A1/6	-2,56
	A1/7	-2,32		A1/7	-3,08		A1/7	-2,56		A1/7	-2,48
	A1/8	-2,28		A1/8	-3,03		A1/8	-2,53		A1/8	-2,45
	A1/9	-2,37		A1/9	-3,15		A1/9	-2,64		A1/9	-2,56
	A1/10	-2,32		A1/10	-3,07		A1/10	-2,56		A1/10	-2,48
	A1/11	-2,27		A1/11	-3,02		A1/11	-2,53		A1/11	-2,45
	A1/12	-2,37		A1/12	-3,15		A1/12	-2,64		A1/12	-2,57
	A1/13	-2,32		A1/13	-3,07		A1/13	-2,56		A1/13	-2,48
	A1/14	-2,27		A1/14	-3,02		A1/14	-2,53		A1/14	-2,45
X+	A1/18	-1,59	X+	A1/18	-2,12	X+	A1/18	-1,76	X+	A1/20	-1,69
X-	A1/25	-1,56	X-	A1/25	-2,08	X-	A1/25	-1,75	X-	A1/27	-1,71
Y+	A1/34	-1,60	Y+	A1/34	-2,13	Y+	A1/34	-1,77	Y+	A1/41	-1,68
Y-	A1/36	-1,55	Y-	A1/36	-2,07	Y-	A1/36	-1,75	Y-	A1/43	-1,71
498	A1/1	-2,53	499	A1/1	-2,90	500	A1/1	-2,82	501	A1/1	-2,78
	A1/2	-2,45		A1/2	-2,82		A1/2	-2,74		A1/2	-2,70
	A1/3	-2,53		A1/3	-2,90		A1/3	-2,82		A1/3	-2,77
	A1/4	-2,45		A1/4	-2,82		A1/4	-2,74		A1/4	-2,69
	A1/5	-2,42		A1/5	-2,78		A1/5	-2,70		A1/5	-2,65
	A1/6	-2,53		A1/6	-2,90		A1/6	-2,82		A1/6	-2,77
	A1/7	-2,44		A1/7	-2,82		A1/7	-2,74		A1/7	-2,69
	A1/8	-2,42		A1/8	-2,78		A1/8	-2,71		A1/8	-2,65
	A1/9	-2,53		A1/9	-2,90		A1/9	-2,82		A1/9	-2,78
	A1/10	-2,45		A1/10	-2,82		A1/10	-2,74		A1/10	-2,70
	A1/11	-2,42		A1/11	-2,78		A1/11	-2,70		A1/11	-2,66
	A1/12	-2,53		A1/12	-2,89		A1/12	-2,82		A1/12	-2,78
	A1/13	-2,45		A1/13	-2,81		A1/13	-2,74		A1/13	-2,70
	A1/14	-2,42		A1/14	-2,77		A1/14	-2,70		A1/14	-2,66
X+	A1/20	-1,68	X+	A1/15	-1,94	X+	A1/15	-1,88	X+	A1/21	-1,80
X-	A1/27	-1,69	X-	A1/24	-1,93	X-	A1/24	-1,88	X-	A1/30	-1,88
Y+	A1/41	-1,67	Y+	A1/31	-1,96	Y+	A1/40	-1,89	Y+	A1/40	-1,82
Y-	A1/43	-1,69	Y-	A1/37	-1,90	Y-	A1/46	-1,87	Y-	A1/46	-1,86
502	A1/1	-2,52	503	A1/1	-3,16	504	A1/1	-2,11	505	A1/1	-2,55
	A1/2	-2,45		A1/2	-3,09		A1/2	-2,05		A1/2	-2,49
	A1/3	-2,52		A1/3	-3,16		A1/3	-2,11		A1/3	-2,55
	A1/4	-2,45		A1/4	-3,09		A1/4	-2,05		A1/4	-2,49
	A1/5	-2,41		A1/5	-3,03		A1/5	-2,02		A1/5	-2,45
	A1/6	-2,51		A1/6	-3,16		A1/6	-2,11		A1/6	-2,55
	A1/7	-2,44		A1/7	-3,09		A1/7	-2,04		A1/7	-2,49
	A1/8	-2,41		A1/8	-3,03		A1/8	-2,02		A1/8	-2,45
	A1/9	-2,52		A1/9	-3,17		A1/9	-2,11		A1/9	-2,55
	A1/10	-2,45		A1/10	-3,09		A1/10	-2,05		A1/10	-2,49
	A1/11	-2,41		A1/11	-3,03		A1/11	-2,02		A1/11	-2,45
	A1/12	-2,52		A1/12	-3,17		A1/12	-2,11		A1/12	-2,55
	A1/13	-2,45		A1/13	-3,09		A1/13	-2,05		A1/13	-2,49
	A1/14	-2,41		A1/14	-3,04		A1/14	-2,03		A1/14	-2,45
X+	A1/20	-1,66	X+	A1/20	-2,07	X+	A1/20	-1,41	X+	A1/21	-1,70
X-	A1/27	-1,68	X-	A1/27	-2,12	X-	A1/27	-1,42	X-	A1/30	-1,71
Y+	A1/41	-1,66	Y+	A1/41	-2,07	Y+	A1/41	-1,39	Y+	A1/40	-1,71
Y-	A1/43	-1,69	Y-	A1/43	-2,12	Y-	A1/43	-1,43	Y-	A1/46	-1,71
506	A1/1	-3,44	507	A1/1	-3,16	508	A1/1	-2,23	509	A1/1	-3,18
	A1/2	-3,37		A1/2	-3,08		A1/2	-2,15		A1/2	-3,08
	A1/3	-3,44		A1/3	-3,16		A1/3	-2,23		A1/3	-3,18
	A1/4	-3,37		A1/4	-3,08		A1/4	-2,15		A1/4	-3,08
	A1/5	-3,30		A1/5	-3,04		A1/5	-2,13		A1/5	-3,04
	A1/6	-3,44		A1/6	-3,17		A1/6	-2,23		A1/6	-3,18
	A1/7	-3,37		A1/7	-3,09		A1/7	-2,14		A1/7	-3,08
	A1/8	-3,32		A1/8	-3,05		A1/8	-2,13		A1/8	-3,04
	A1/9	-3,44		A1/9	-3,16		A1/9	-2,23		A1/9	-3,18
	A1/10	-3,37		A1/10	-3,08		A1/10	-2,15		A1/10	-3,08
	A1/11	-3,30		A1/11	-3,04		A1/11	-2,13		A1/11	-3,04

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/12	-3,43		A1/12	-3,16		A1/12	-2,23		A1/12	-3,18
	A1/13	-3,36		A1/13	-3,08		A1/13	-2,15		A1/13	-3,08
	A1/14	-3,29		A1/14	-3,03		A1/14	-2,13		A1/14	-3,05
X+	A1/15	-2,30	X+	A1/15	-2,12	X+	A1/20	-1,48	X+	A1/20	-2,12
X-	A1/24	-2,31	X-	A1/24	-2,12	X-	A1/27	-1,48	X-	A1/27	-2,11
Y+	A1/40	-2,35	Y+	A1/40	-2,15	Y+	A1/34	-1,47	Y+	A1/34	-2,09
Y-	A1/46	-2,24	Y-	A1/46	-2,07	Y-	A1/36	-1,49	Y-	A1/36	-2,13
510	A1/1	-2,56	511	A1/1	-2,13	512	A1/1	-2,46	513	A1/1	-1,94
	A1/2	-2,47		A1/2	-2,04		A1/2	-2,37		A1/2	-1,85
	A1/3	-2,56		A1/3	-2,13		A1/3	-2,46		A1/3	-1,94
	A1/4	-2,47		A1/4	-2,04		A1/4	-2,38		A1/4	-1,85
	A1/5	-2,45		A1/5	-2,03		A1/5	-2,35		A1/5	-1,84
	A1/6	-2,56		A1/6	-2,13		A1/6	-2,46		A1/6	-1,94
	A1/7	-2,47		A1/7	-2,04		A1/7	-2,37		A1/7	-1,85
	A1/8	-2,45		A1/8	-2,03		A1/8	-2,34		A1/8	-1,84
	A1/9	-2,56		A1/9	-2,13		A1/9	-2,46		A1/9	-1,94
	A1/10	-2,47		A1/10	-2,04		A1/10	-2,37		A1/10	-1,85
	A1/11	-2,45		A1/11	-2,03		A1/11	-2,35		A1/11	-1,84
	A1/12	-2,56		A1/12	-2,13		A1/12	-2,46		A1/12	-1,94
	A1/13	-2,47		A1/13	-2,04		A1/13	-2,38		A1/13	-1,85
	A1/14	-2,45		A1/14	-2,03		A1/14	-2,35		A1/14	-1,84
X+	A1/20	-1,71	X+	A1/21	-1,40	X+	A1/20	-1,64	X+	A1/21	-1,27
X-	A1/27	-1,72	X-	A1/30	-1,42	X-	A1/27	-1,61	X-	A1/30	-1,28
Y+	A1/41	-1,69	Y+	A1/40	-1,41	Y+	A1/34	-1,61	Y+	A1/40	-1,27
Y-	A1/43	-1,73	Y-	A1/46	-1,42	Y-	A1/36	-1,64	Y-	A1/46	-1,28
514	A1/1	-1,86	515	A1/1	-1,80	516	A1/1	-1,66	517	A1/1	-1,65
	A1/2	-1,77		A1/2	-1,71		A1/2	-1,57		A1/2	-1,55
	A1/3	-1,86		A1/3	-1,80		A1/3	-1,66		A1/3	-1,64
	A1/4	-1,77		A1/4	-1,71		A1/4	-1,57		A1/4	-1,55
	A1/5	-1,77		A1/5	-1,71		A1/5	-1,57		A1/5	-1,56
	A1/6	-1,86		A1/6	-1,80		A1/6	-1,66		A1/6	-1,65
	A1/7	-1,77		A1/7	-1,71		A1/7	-1,57		A1/7	-1,55
	A1/8	-1,77		A1/8	-1,71		A1/8	-1,57		A1/8	-1,56
	A1/9	-1,87		A1/9	-1,80		A1/9	-1,66		A1/9	-1,65
	A1/10	-1,78		A1/10	-1,71		A1/10	-1,58		A1/10	-1,56
	A1/11	-1,78		A1/11	-1,72		A1/11	-1,58		A1/11	-1,57
	A1/12	-1,86		A1/12	-1,80		A1/12	-1,66		A1/12	-1,65
	A1/13	-1,77		A1/13	-1,71		A1/13	-1,57		A1/13	-1,55
	A1/14	-1,77		A1/14	-1,71		A1/14	-1,58		A1/14	-1,56
X+	A1/21	-1,22	X+	A1/21	-1,17	X+	A1/21	-1,07	X+	A1/21	-1,06
X-	A1/30	-1,25	X-	A1/30	-1,21	X-	A1/30	-1,12	X-	A1/30	-1,12
Y+	A1/40	-1,23	Y+	A1/40	-1,19	Y+	A1/40	-1,10	Y+	A1/40	-1,09
Y-	A1/46	-1,24	Y-	A1/46	-1,20	Y-	A1/46	-1,11	Y-	A1/46	-1,10
518	A1/1	-3,77	519	A1/1	-2,23	520	A1/1	-2,97	521	A1/1	-1,69
	A1/2	-3,67		A1/2	-2,14		A1/2	-2,88		A1/2	-1,61
	A1/3	-3,77		A1/3	-2,23		A1/3	-2,97		A1/3	-1,69
	A1/4	-3,67		A1/4	-2,14		A1/4	-2,88		A1/4	-1,60
	A1/5	-3,61		A1/5	-2,13		A1/5	-2,85		A1/5	-1,60
	A1/6	-3,76		A1/6	-2,23		A1/6	-2,97		A1/6	-1,69
	A1/7	-3,66		A1/7	-2,14		A1/7	-2,88		A1/7	-1,60
	A1/8	-3,60		A1/8	-2,13		A1/8	-2,85		A1/8	-1,60
	A1/9	-3,76		A1/9	-2,23		A1/9	-2,97		A1/9	-1,69
	A1/10	-3,67		A1/10	-2,14		A1/10	-2,88		A1/10	-1,61
	A1/11	-3,60		A1/11	-2,13		A1/11	-2,85		A1/11	-1,61
	A1/12	-3,77		A1/12	-2,23		A1/12	-2,97		A1/12	-1,70
	A1/13	-3,67		A1/13	-2,14		A1/13	-2,88		A1/13	-1,61
	A1/14	-3,61		A1/14	-2,13		A1/14	-2,85		A1/14	-1,62
X+	A1/20	-2,53	X+	A1/15	-1,47	X+	A1/15	-1,98	X+	A1/20	-1,11
X-	A1/27	-2,46	X-	A1/24	-1,49	X-	A1/24	-1,99	X-	A1/27	-1,15
Y+	A1/34	-2,46	Y+	A1/40	-1,49	Y+	A1/40	-1,99	Y+	A1/41	-1,09
Y-	A1/36	-2,53	Y-	A1/46	-1,48	Y-	A1/46	-1,98	Y-	A1/43	-1,16
522	A1/1	-1,65	523	A1/1	-2,14	524	A1/1	-1,99	525	A1/1	-3,17
	A1/2	-1,56		A1/2	-2,06		A1/2	-1,90		A1/2	-3,10
	A1/3	-1,65		A1/3	-2,14		A1/3	-1,99		A1/3	-3,19
	A1/4	-1,56		A1/4	-2,06		A1/4	-1,90		A1/4	-3,11
	A1/5	-1,56		A1/5	-2,05		A1/5	-1,90		A1/5	-3,08
	A1/6	-1,65		A1/6	-2,12		A1/6	-1,98		A1/6	-3,14
	A1/7	-1,56		A1/7	-2,04		A1/7	-1,89		A1/7	-3,06
	A1/8	-1,56		A1/8	-2,02		A1/8	-1,89		A1/8	-3,00
	A1/9	-1,66		A1/9	-2,14		A1/9	-1,99		A1/9	-3,16
	A1/10	-1,56		A1/10	-2,05		A1/10	-1,90		A1/10	-3,08
	A1/11	-1,57		A1/11	-2,04		A1/11	-1,90		A1/11	-3,04
	A1/12	-1,65		A1/12	-2,16		A1/12	-2,00		A1/12	-3,21
	A1/13	-1,56		A1/13	-2,07		A1/13	-1,91		A1/13	-3,13
	A1/14	-1,57		A1/14	-2,07		A1/14	-1,91		A1/14	-3,12
X+	A1/21	-1,06	X+	A1/20	-1,50	X+	A1/20	-1,34	X+	A1/20	-2,41
X-	A1/30	-1,13	X-	A1/27	-1,46	X-	A1/27	-1,35	X-	A1/27	-2,13
Y+	A1/40	-1,09	Y+	A1/34	-1,34	Y+	A1/41	-1,28	Y+	A1/34	-1,98

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	Y- A1/46	-1,12		Y- A1/36	-1,56		Y- A1/43	-1,38		Y- A1/36	-2,50
526	A1/1	-2,78	527	A1/1	-1,88	528	A1/1	-1,60	529	A1/1	-1,60
	A1/2	-2,70		A1/2	-1,79		A1/2	-1,51		A1/2	-1,51
	A1/3	-2,79		A1/3	-1,88		A1/3	-1,60		A1/3	-1,60
	A1/4	-2,71		A1/4	-1,79		A1/4	-1,51		A1/4	-1,51
	A1/5	-2,69		A1/5	-1,79		A1/5	-1,51		A1/5	-1,51
	A1/6	-2,76		A1/6	-1,88		A1/6	-1,60		A1/6	-1,60
	A1/7	-2,68		A1/7	-1,79		A1/7	-1,51		A1/7	-1,51
	A1/8	-2,65		A1/8	-1,80		A1/8	-1,52		A1/8	-1,52
	A1/9	-2,77		A1/9	-1,88		A1/9	-1,60		A1/9	-1,61
	A1/10	-2,69		A1/10	-1,80		A1/10	-1,51		A1/10	-1,51
	A1/11	-2,67		A1/11	-1,80		A1/11	-1,52		A1/11	-1,52
	A1/12	-2,80		A1/12	-1,88		A1/12	-1,60		A1/12	-1,60
	A1/13	-2,72		A1/13	-1,79		A1/13	-1,51		A1/13	-1,51
	A1/14	-2,71		A1/14	-1,80		A1/14	-1,52		A1/14	-1,52
	X+ A1/20	-2,03		X+ A1/21	-1,24		X+ A1/21	-1,02		X+ A1/21	-1,02
	X- A1/27	-1,85		X- A1/30	-1,27		X- A1/30	-1,10		X- A1/30	-1,09
	Y+ A1/34	-1,82		Y+ A1/40	-1,26		Y+ A1/40	-1,07		Y+ A1/40	-1,07
	Y- A1/36	-2,05		Y- A1/46	-1,26		Y- A1/46	-1,07		Y- A1/46	-1,07
530	A1/1	-3,00	531	A1/1	-3,57	532	A1/1	-2,54	533	A1/1	-4,42
	A1/2	-2,94		A1/2	-3,51		A1/2	-2,46		A1/2	-4,36
	A1/3	-3,02		A1/3	-3,60		A1/3	-2,54		A1/3	-4,45
	A1/4	-2,96		A1/4	-3,53		A1/4	-2,46		A1/4	-4,39
	A1/5	-2,94		A1/5	-3,50		A1/5	-2,45		A1/5	-4,34
	A1/6	-3,00		A1/6	-3,55		A1/6	-2,54		A1/6	-4,36
	A1/7	-2,94		A1/7	-3,49		A1/7	-2,46		A1/7	-4,29
	A1/8	-2,91		A1/8	-3,43		A1/8	-2,44		A1/8	-4,19
	A1/9	-2,99		A1/9	-3,55		A1/9	-2,53		A1/9	-4,39
	A1/10	-2,93		A1/10	-3,49		A1/10	-2,45		A1/10	-4,33
	A1/11	-2,89		A1/11	-3,43		A1/11	-2,43		A1/11	-4,24
	A1/12	-3,00		A1/12	-3,60		A1/12	-2,54		A1/12	-4,49
	A1/13	-2,94		A1/13	-3,53		A1/13	-2,46		A1/13	-4,42
	A1/14	-2,92		A1/14	-3,51		A1/14	-2,44		A1/14	-4,40
	X+ A1/18	-2,25		X+ A1/20	-2,77		X+ A1/18	-1,79		X+ A1/20	-3,58
	X- A1/25	-1,92		X- A1/27	-2,32		X- A1/25	-1,66		X- A1/27	-2,91
	Y+ A1/34	-2,15		Y+ A1/34	-2,41		Y+ A1/34	-1,75		Y+ A1/34	-2,77
	Y- A1/36	-2,13		Y- A1/36	-2,72		Y- A1/36	-1,74		Y- A1/36	-3,67
534	A1/1	-3,63	535	A1/1	-2,32	536	A1/1	-1,62	537	A1/1	-1,84
	A1/2	-3,54		A1/2	-2,24		A1/2	-1,53		A1/2	-1,75
	A1/3	-3,63		A1/3	-2,32		A1/3	-1,62		A1/3	-1,84
	A1/4	-3,53		A1/4	-2,24		A1/4	-1,53		A1/4	-1,75
	A1/5	-3,48		A1/5	-2,21		A1/5	-1,53		A1/5	-1,75
	A1/6	-3,63		A1/6	-2,32		A1/6	-1,62		A1/6	-1,84
	A1/7	-3,54		A1/7	-2,24		A1/7	-1,53		A1/7	-1,75
	A1/8	-3,49		A1/8	-2,22		A1/8	-1,54		A1/8	-1,75
	A1/9	-3,63		A1/9	-2,32		A1/9	-1,63		A1/9	-1,84
	A1/10	-3,54		A1/10	-2,24		A1/10	-1,54		A1/10	-1,75
	A1/11	-3,48		A1/11	-2,22		A1/11	-1,55		A1/11	-1,75
	A1/12	-3,62		A1/12	-2,31		A1/12	-1,62		A1/12	-1,84
	A1/13	-3,53		A1/13	-2,23		A1/13	-1,53		A1/13	-1,75
	A1/14	-3,47		A1/14	-2,21		A1/14	-1,54		A1/14	-1,75
	X+ A1/15	-2,42		X+ A1/15	-1,53		X+ A1/21	-1,04		X+ A1/21	-1,19
	X- A1/24	-2,44		X- A1/24	-1,56		X- A1/30	-1,11		X- A1/30	-1,24
	Y+ A1/40	-2,47		Y+ A1/40	-1,56		Y+ A1/40	-1,08		Y+ A1/40	-1,22
	Y- A1/46	-2,37		Y- A1/46	-1,53		Y- A1/46	-1,09		Y- A1/46	-1,23
538	A1/1	-1,80	539	A1/1	-1,57	540	A1/1	-1,65	541	A1/1	-1,64
	A1/2	-1,71		A1/2	-1,49		A1/2	-1,55		A1/2	-1,55
	A1/3	-1,80		A1/3	-1,57		A1/3	-1,64		A1/3	-1,63
	A1/4	-1,71		A1/4	-1,48		A1/4	-1,55		A1/4	-1,55
	A1/5	-1,71		A1/5	-1,49		A1/5	-1,56		A1/5	-1,55
	A1/6	-1,80		A1/6	-1,57		A1/6	-1,65		A1/6	-1,64
	A1/7	-1,71		A1/7	-1,49		A1/7	-1,56		A1/7	-1,56
	A1/8	-1,71		A1/8	-1,49		A1/8	-1,56		A1/8	-1,56
	A1/9	-1,80		A1/9	-1,57		A1/9	-1,65		A1/9	-1,64
	A1/10	-1,72		A1/10	-1,49		A1/10	-1,56		A1/10	-1,55
	A1/11	-1,71		A1/11	-1,50		A1/11	-1,57		A1/11	-1,56
	A1/12	-1,80		A1/12	-1,57		A1/12	-1,64		A1/12	-1,63
	A1/13	-1,71		A1/13	-1,49		A1/13	-1,55		A1/13	-1,55
	A1/14	-1,71		A1/14	-1,49		A1/14	-1,56		A1/14	-1,55
	X+ A1/15	-1,17		X+ A1/15	-1,01		X+ A1/15	-1,06		X+ A1/15	-1,07
	X- A1/24	-1,21		X- A1/24	-1,07		X- A1/24	-1,13		X- A1/24	-1,12
	Y+ A1/40	-1,20		Y+ A1/40	-1,05		Y+ A1/40	-1,11		Y+ A1/40	-1,13
	Y- A1/46	-1,19		Y- A1/46	-1,04		Y- A1/46	-1,09		Y- A1/46	-1,06
542	A1/1	-1,99	543	A1/1	-2,11	544	A1/1	-2,79	545	A1/1	-3,27
	A1/2	-1,90		A1/2	-2,03		A1/2	-2,71		A1/2	-3,21
	A1/3	-1,99		A1/3	-2,11		A1/3	-2,80		A1/3	-3,29
	A1/4	-1,90		A1/4	-2,03		A1/4	-2,72		A1/4	-3,23

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/5	-1,90		A1/5	-2,02		A1/5	-2,71		A1/5	-3,21
	A1/6	-2,00		A1/6	-2,12		A1/6	-2,81		A1/6	-3,29
	A1/7	-1,91		A1/7	-2,04		A1/7	-2,73		A1/7	-3,23
	A1/8	-1,91		A1/8	-2,04		A1/8	-2,72		A1/8	-3,21
	A1/9	-1,99		A1/9	-2,11		A1/9	-2,78		A1/9	-3,25
	A1/10	-1,90		A1/10	-2,02		A1/10	-2,70		A1/10	-3,19
	A1/11	-1,90		A1/11	-2,01		A1/11	-2,68		A1/11	-3,14
	A1/12	-1,99		A1/12	-2,09		A1/12	-2,78		A1/12	-3,25
	A1/13	-1,90		A1/13	-2,01		A1/13	-2,69		A1/13	-3,19
	A1/14	-1,89		A1/14	-1,99		A1/14	-2,66		A1/14	-3,14
X+	A1/15	-1,35	X+	A1/15	-1,48	X+	A1/15	-2,03	X+	A1/18	-2,52
X-	A1/24	-1,35	X-	A1/24	-1,42	X-	A1/24	-1,84	X-	A1/25	-2,09
Y+	A1/40	-1,39	Y+	A1/31	-1,54	Y+	A1/31	-2,05	Y+	A1/34	-2,49
Y-	A1/46	-1,28	Y-	A1/37	-1,31	Y-	A1/37	-1,80	Y-	A1/36	-2,15
546	A1/1	-4,40	547	A1/1	-3,15	548	A1/1	-2,56	549	A1/1	-1,89
	A1/2	-4,34		A1/2	-3,08		A1/2	-2,53		A1/2	-1,86
	A1/3	-4,44		A1/3	-3,17		A1/3	-2,55		A1/3	-1,89
	A1/4	-4,37		A1/4	-3,09		A1/4	-2,51		A1/4	-1,85
	A1/5	-4,33		A1/5	-3,07		A1/5	-2,46		A1/5	-1,82
	A1/6	-4,47		A1/6	-3,19		A1/6	-2,59		A1/6	-1,91
	A1/7	-4,40		A1/7	-3,11		A1/7	-2,56		A1/7	-1,87
	A1/8	-4,38		A1/8	-3,10		A1/8	-2,54		A1/8	-1,85
	A1/9	-4,37		A1/9	-3,14		A1/9	-2,58		A1/9	-1,90
	A1/10	-4,30		A1/10	-3,06		A1/10	-2,54		A1/10	-1,86
	A1/11	-4,21		A1/11	-3,02		A1/11	-2,51		A1/11	-1,84
	A1/12	-4,34		A1/12	-3,12		A1/12	-2,53		A1/12	-1,88
	A1/13	-4,27		A1/13	-3,04		A1/13	-2,50		A1/13	-1,84
	A1/14	-4,16		A1/14	-2,98		A1/14	-2,44		A1/14	-1,80
X+	A1/15	-3,52	X+	A1/15	-2,38	X+	A1/15	-1,67	X+	A1/15	-1,24
X-	A1/24	-2,81	X-	A1/24	-2,07	X-	A1/24	-1,98	X-	A1/24	-1,39
Y+	A1/31	-3,61	Y+	A1/31	-2,46	Y+	A1/40	-2,04	Y+	A1/40	-1,42
Y-	A1/37	-2,64	Y-	A1/37	-1,92	Y-	A1/46	-1,56	Y-	A1/46	-1,19
550	A1/1	-1,89	551	A1/1	-2,28	552	A1/1	-1,78	553	A1/1	-1,71
	A1/2	-1,85		A1/2	-2,23		A1/2	-1,74		A1/2	-1,67
	A1/3	-1,88		A1/3	-2,27		A1/3	-1,78		A1/3	-1,71
	A1/4	-1,85		A1/4	-2,23		A1/4	-1,74		A1/4	-1,67
	A1/5	-1,81		A1/5	-2,18		A1/5	-1,71		A1/5	-1,64
	A1/6	-1,90		A1/6	-2,28		A1/6	-1,78		A1/6	-1,71
	A1/7	-1,86		A1/7	-2,24		A1/7	-1,75		A1/7	-1,68
	A1/8	-1,83		A1/8	-2,20		A1/8	-1,72		A1/8	-1,65
	A1/9	-1,89		A1/9	-2,28		A1/9	-1,78		A1/9	-1,71
	A1/10	-1,86		A1/10	-2,24		A1/10	-1,75		A1/10	-1,67
	A1/11	-1,83		A1/11	-2,20		A1/11	-1,72		A1/11	-1,64
	A1/12	-1,88		A1/12	-2,27		A1/12	-1,78		A1/12	-1,71
	A1/13	-1,84		A1/13	-2,23		A1/13	-1,74		A1/13	-1,67
	A1/14	-1,81		A1/14	-2,18		A1/14	-1,71		A1/14	-1,64
X+	A1/15	-1,23	X+	A1/15	-1,49	X+	A1/15	-1,17	X+	A1/15	-1,14
X-	A1/24	-1,33	X-	A1/24	-1,58	X-	A1/24	-1,22	X-	A1/24	-1,15
Y+	A1/40	-1,34	Y+	A1/40	-1,58	Y+	A1/40	-1,22	Y+	A1/40	-1,16
Y-	A1/46	-1,22	Y-	A1/46	-1,48	Y-	A1/46	-1,17	Y-	A1/46	-1,12
554	A1/1	-1,90	555	A1/1	-1,84	556	A1/1	-3,10	557	A1/1	-1,57
	A1/2	-1,86		A1/2	-1,80		A1/2	-3,04		A1/2	-1,53
	A1/3	-1,90		A1/3	-1,84		A1/3	-3,10		A1/3	-1,57
	A1/4	-1,86		A1/4	-1,81		A1/4	-3,04		A1/4	-1,53
	A1/5	-1,82		A1/5	-1,77		A1/5	-2,98		A1/5	-1,51
	A1/6	-1,90		A1/6	-1,84		A1/6	-3,10		A1/6	-1,57
	A1/7	-1,86		A1/7	-1,81		A1/7	-3,05		A1/7	-1,54
	A1/8	-1,83		A1/8	-1,78		A1/8	-2,99		A1/8	-1,51
	A1/9	-1,89		A1/9	-1,84		A1/9	-3,09		A1/9	-1,57
	A1/10	-1,86		A1/10	-1,80		A1/10	-3,04		A1/10	-1,53
	A1/11	-1,82		A1/11	-1,77		A1/11	-2,97		A1/11	-1,51
	A1/12	-1,89		A1/12	-1,84		A1/12	-3,09		A1/12	-1,57
	A1/13	-1,86		A1/13	-1,80		A1/13	-3,04		A1/13	-1,53
	A1/14	-1,82		A1/14	-1,76		A1/14	-2,97		A1/14	-1,50
X+	A1/18	-1,27	X+	A1/18	-1,24	X+	A1/18	-2,09	X+	A1/18	-1,06
X-	A1/25	-1,26	X-	A1/25	-1,22	X-	A1/25	-2,05	X-	A1/25	-1,04
Y+	A1/34	-1,29	Y+	A1/34	-1,25	Y+	A1/34	-2,11	Y+	A1/34	-1,07
Y-	A1/36	-1,24	Y-	A1/36	-1,20	Y-	A1/36	-2,01	Y-	A1/36	-1,02
558	A1/1	-1,60	559	A1/1	-1,87	560	A1/1	-1,28	561	A1/1	-2,11
	A1/2	-1,57		A1/2	-1,84		A1/2	-1,24		A1/2	-2,06
	A1/3	-1,60		A1/3	-1,87		A1/3	-1,28		A1/3	-2,10
	A1/4	-1,57		A1/4	-1,84		A1/4	-1,24		A1/4	-2,06
	A1/5	-1,54		A1/5	-1,80		A1/5	-1,22		A1/5	-2,02
	A1/6	-1,61		A1/6	-1,88		A1/6	-1,28		A1/6	-2,11
	A1/7	-1,57		A1/7	-1,85		A1/7	-1,24		A1/7	-2,07
	A1/8	-1,55		A1/8	-1,81		A1/8	-1,23		A1/8	-2,03
	A1/9	-1,60		A1/9	-1,87		A1/9	-1,28		A1/9	-2,11
	A1/10	-1,57		A1/10	-1,84		A1/10	-1,24		A1/10	-2,07

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/11	-1,54		A1/11	-1,80		A1/11	-1,23		A1/11	-2,02
	A1/12	-1,60		A1/12	-1,87		A1/12	-1,28		A1/12	-2,10
	A1/13	-1,56		A1/13	-1,83		A1/13	-1,24		A1/13	-2,06
	A1/14	-1,53		A1/14	-1,79		A1/14	-1,22		A1/14	-2,01
X+	A1/15	-1,08	X+	A1/15	-1,26	X+	A1/15	-0,85	X+	A1/15	-1,41
X-	A1/24	-1,07	X-	A1/24	-1,26	X-	A1/24	-0,86	X-	A1/24	-1,42
Y+	A1/31	-1,10	Y+	A1/40	-1,30	Y+	A1/40	-0,87	Y+	A1/40	-1,45
Y-	A1/37	-1,04	Y-	A1/46	-1,20	Y-	A1/46	-0,83	Y-	A1/46	-1,35
562	A1/1	-0,94	563	A1/1	-0,77	564	A1/1	-0,77	565	A1/1	-0,99
	A1/2	-0,90		A1/2	-0,73		A1/2	-0,73		A1/2	-0,95
	A1/3	-0,94		A1/3	-0,77		A1/3	-0,77		A1/3	-0,99
	A1/4	-0,90		A1/4	-0,73		A1/4	-0,73		A1/4	-0,95
	A1/5	-0,89		A1/5	-0,73		A1/5	-0,73		A1/5	-0,94
	A1/6	-0,94		A1/6	-0,77		A1/6	-0,77		A1/6	-1,00
	A1/7	-0,90		A1/7	-0,73		A1/7	-0,73		A1/7	-0,96
	A1/8	-0,90		A1/8	-0,73		A1/8	-0,74		A1/8	-0,96
	A1/9	-0,94		A1/9	-0,77		A1/9	-0,77		A1/9	-0,99
	A1/10	-0,90		A1/10	-0,73		A1/10	-0,73		A1/10	-0,95
	A1/11	-0,90		A1/11	-0,73		A1/11	-0,73		A1/11	-0,94
	A1/12	-0,94		A1/12	-0,77		A1/12	-0,77		A1/12	-0,98
	A1/13	-0,90		A1/13	-0,73		A1/13	-0,73		A1/13	-0,94
	A1/14	-0,89		A1/14	-0,73		A1/14	-0,73		A1/14	-0,93
X+	A1/15	-0,62	X+	A1/15	-0,50	X+	A1/15	-0,51	X+	A1/15	-0,69
X-	A1/24	-0,63	X-	A1/24	-0,52	X-	A1/24	-0,52	X-	A1/24	-0,67
Y+	A1/40	-0,63	Y+	A1/40	-0,51	Y+	A1/40	-0,53	Y+	A1/31	-0,73
Y-	A1/46	-0,62	Y-	A1/46	-0,51	Y-	A1/46	-0,49	Y-	A1/37	-0,60
566	A1/1	-1,51	567	A1/1	-2,39	568	A1/1	-2,53	569	A1/1	-1,99
	A1/2	-1,48		A1/2	-2,36		A1/2	-2,50		A1/2	-1,95
	A1/3	-1,52		A1/3	-2,41		A1/3	-2,51		A1/3	-1,98
	A1/4	-1,48		A1/4	-2,38		A1/4	-2,47		A1/4	-1,94
	A1/5	-1,47		A1/5	-2,35		A1/5	-2,42		A1/5	-1,90
	A1/6	-1,53		A1/6	-2,43		A1/6	-2,50		A1/6	-1,97
	A1/7	-1,50		A1/7	-2,40		A1/7	-2,46		A1/7	-1,94
	A1/8	-1,49		A1/8	-2,39		A1/8	-2,40		A1/8	-1,90
	A1/9	-1,51		A1/9	-2,37		A1/9	-2,56		A1/9	-2,00
	A1/10	-1,47		A1/10	-2,34		A1/10	-2,53		A1/10	-1,97
	A1/11	-1,44		A1/11	-2,28		A1/11	-2,51		A1/11	-1,95
	A1/12	-1,49		A1/12	-2,34		A1/12	-2,57		A1/12	-2,01
	A1/13	-1,45		A1/13	-2,31		A1/13	-2,54		A1/13	-1,97
	A1/14	-1,42		A1/14	-2,24		A1/14	-2,52		A1/14	-1,96
X+	A1/15	-1,15	X+	A1/15	-1,93	X+	A1/21	-1,57	X+	A1/21	-1,25
X-	A1/24	-1,00	X-	A1/24	-1,54	X-	A1/30	-2,10	X-	A1/30	-1,54
Y+	A1/31	-1,21	Y+	A1/31	-2,03	Y+	A1/40	-1,55	Y+	A1/40	-1,26
Y-	A1/37	-0,89	Y-	A1/37	-1,36	Y-	A1/46	-2,11	Y-	A1/46	-1,54
570	A1/1	-1,95	571	A1/1	-2,04	572	A1/1	-2,48	573	A1/1	-2,09
	A1/2	-1,91		A1/2	-2,01		A1/2	-2,44		A1/2	-2,05
	A1/3	-1,94		A1/3	-2,04		A1/3	-2,48		A1/3	-2,08
	A1/4	-1,90		A1/4	-2,00		A1/4	-2,44		A1/4	-2,05
	A1/5	-1,87		A1/5	-1,96		A1/5	-2,39		A1/5	-2,00
	A1/6	-1,94		A1/6	-2,04		A1/6	-2,45		A1/6	-2,09
	A1/7	-1,90		A1/7	-2,00		A1/7	-2,41		A1/7	-2,05
	A1/8	-1,87		A1/8	-1,96		A1/8	-2,35		A1/8	-2,01
	A1/9	-1,96		A1/9	-2,05		A1/9	-2,48		A1/9	-2,10
	A1/10	-1,92		A1/10	-2,02		A1/10	-2,45		A1/10	-2,06
	A1/11	-1,90		A1/11	-1,99		A1/11	-2,41		A1/11	-2,03
	A1/12	-1,96		A1/12	-2,05		A1/12	-2,51		A1/12	-2,09
	A1/13	-1,92		A1/13	-2,01		A1/13	-2,47		A1/13	-2,06
	A1/14	-1,90		A1/14	-1,98		A1/14	-2,44		A1/14	-2,02
X+	A1/21	-1,24	X+	A1/20	-1,31	X+	A1/21	-1,71	X+	A1/20	-1,34
X-	A1/30	-1,44	X-	A1/27	-1,47	X-	A1/30	-1,79	X-	A1/27	-1,48
Y+	A1/40	-1,27	Y+	A1/41	-1,35	Y+	A1/40	-1,49	Y+	A1/41	-1,40
Y-	A1/46	-1,42	Y-	A1/43	-1,45	Y-	A1/46	-1,91	Y-	A1/43	-1,45
574	A1/1	-1,97	575	A1/1	-2,11	576	A1/1	-2,29	577	A1/1	-2,49
	A1/2	-1,93		A1/2	-2,07		A1/2	-2,25		A1/2	-2,45
	A1/3	-1,97		A1/3	-2,10		A1/3	-2,28		A1/3	-2,49
	A1/4	-1,93		A1/4	-2,07		A1/4	-2,25		A1/4	-2,45
	A1/5	-1,89		A1/5	-2,02		A1/5	-2,20		A1/5	-2,40
	A1/6	-1,97		A1/6	-2,12		A1/6	-2,27		A1/6	-2,48
	A1/7	-1,93		A1/7	-2,08		A1/7	-2,23		A1/7	-2,44
	A1/8	-1,90		A1/8	-2,05		A1/8	-2,18		A1/8	-2,38
	A1/9	-1,98		A1/9	-2,12		A1/9	-2,29		A1/9	-2,49
	A1/10	-1,94		A1/10	-2,08		A1/10	-2,25		A1/10	-2,45
	A1/11	-1,91		A1/11	-2,05		A1/11	-2,21		A1/11	-2,40
	A1/12	-1,97		A1/12	-2,10		A1/12	-2,30		A1/12	-2,50
	A1/13	-1,93		A1/13	-2,07		A1/13	-2,26		A1/13	-2,46
	A1/14	-1,90		A1/14	-2,03		A1/14	-2,23		A1/14	-2,42
X+	A1/18	-1,27	X+	A1/18	-1,37	X+	A1/21	-1,56	X+	A1/21	-1,68
X-	A1/25	-1,39	X-	A1/25	-1,51	X-	A1/30	-1,59	X-	A1/30	-1,70

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RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	Y+ A1/41	-1,36		Y+ A1/41	-1,50		Y+ A1/40	-1,43		Y+ A1/40	-1,59
	Y- A1/43	-1,33		Y- A1/43	-1,40		Y- A1/46	-1,66		Y- A1/46	-1,74
578	A1/1	-1,81	579	A1/1	-1,80	580	A1/1	-2,41	581	A1/1	-2,44
	A1/2	-1,78		A1/2	-1,76		A1/2	-2,36		A1/2	-2,39
	A1/3	-1,81		A1/3	-1,80		A1/3	-2,41		A1/3	-2,44
	A1/4	-1,78		A1/4	-1,76		A1/4	-2,36		A1/4	-2,40
	A1/5	-1,74		A1/5	-1,73		A1/5	-2,31		A1/5	-2,35
	A1/6	-1,81		A1/6	-1,80		A1/6	-2,40		A1/6	-2,43
	A1/7	-1,77		A1/7	-1,76		A1/7	-2,35		A1/7	-2,38
	A1/8	-1,74		A1/8	-1,72		A1/8	-2,30		A1/8	-2,32
	A1/9	-1,81		A1/9	-1,80		A1/9	-2,40		A1/9	-2,43
	A1/10	-1,78		A1/10	-1,76		A1/10	-2,35		A1/10	-2,38
	A1/11	-1,74		A1/11	-1,72		A1/11	-2,30		A1/11	-2,33
	A1/12	-1,82		A1/12	-1,80		A1/12	-2,41		A1/12	-2,44
	A1/13	-1,78		A1/13	-1,76		A1/13	-2,36		A1/13	-2,40
	A1/14	-1,75		A1/14	-1,73		A1/14	-2,32		A1/14	-2,35
X+	A1/21	-1,22	X+	A1/21	-1,22	X+	A1/21	-1,65	X+	A1/21	-1,69
X-	A1/30	-1,22	X-	A1/30	-1,19	X-	A1/30	-1,56	X-	A1/30	-1,57
Y+	A1/31	-1,17	Y+	A1/31	-1,17	Y+	A1/31	-1,57	Y+	A1/31	-1,57
Y-	A1/37	-1,24	Y-	A1/37	-1,23	Y-	A1/37	-1,65	Y-	A1/37	-1,69
582	A1/1	-2,08	583	A1/1	-2,07	584	A1/1	-3,16	585	A1/1	-2,08
	A1/2	-2,04		A1/2	-2,03		A1/2	-3,12		A1/2	-2,03
	A1/3	-2,09		A1/3	-2,08		A1/3	-3,17		A1/3	-2,08
	A1/4	-2,05		A1/4	-2,04		A1/4	-3,13		A1/4	-2,04
	A1/5	-2,01		A1/5	-2,00		A1/5	-3,08		A1/5	-2,01
	A1/6	-2,07		A1/6	-2,06		A1/6	-3,10		A1/6	-2,06
	A1/7	-2,03		A1/7	-2,02		A1/7	-3,06		A1/7	-2,01
	A1/8	-1,98		A1/8	-1,96		A1/8	-2,97		A1/8	-1,97
	A1/9	-2,07		A1/9	-2,07		A1/9	-3,15		A1/9	-2,07
	A1/10	-2,04		A1/10	-2,03		A1/10	-3,11		A1/10	-2,03
	A1/11	-1,99		A1/11	-1,98		A1/11	-3,05		A1/11	-2,00
	A1/12	-2,09		A1/12	-2,09		A1/12	-3,22		A1/12	-2,10
	A1/13	-2,05		A1/13	-2,05		A1/13	-3,18		A1/13	-2,05
	A1/14	-2,01		A1/14	-2,02		A1/14	-3,16		A1/14	-2,04
X+	A1/21	-1,47	X+	A1/21	-1,49	X+	A1/20	-2,42	X+	A1/20	-1,52
X-	A1/30	-1,34	X-	A1/30	-1,34	X-	A1/27	-2,20	X-	A1/27	-1,41
Y+	A1/31	-1,32	Y+	A1/31	-1,27	Y+	A1/34	-1,77	Y+	A1/34	-1,27
Y-	A1/37	-1,48	Y-	A1/37	-1,54	Y-	A1/36	-2,65	Y-	A1/36	-1,59
586	A1/1	-1,57	587	A1/1	-1,63	588	A1/1	-1,97	589	A1/1	-2,30
	A1/2	-1,52		A1/2	-1,59		A1/2	-1,92		A1/2	-2,26
	A1/3	-1,57		A1/3	-1,64		A1/3	-1,97		A1/3	-2,30
	A1/4	-1,52		A1/4	-1,59		A1/4	-1,93		A1/4	-2,26
	A1/5	-1,51		A1/5	-1,57		A1/5	-1,90		A1/5	-2,23
	A1/6	-1,56		A1/6	-1,64		A1/6	-1,97		A1/6	-2,31
	A1/7	-1,52		A1/7	-1,59		A1/7	-1,93		A1/7	-2,27
	A1/8	-1,50		A1/8	-1,58		A1/8	-1,90		A1/8	-2,23
	A1/9	-1,56		A1/9	-1,63		A1/9	-1,96		A1/9	-2,30
	A1/10	-1,52		A1/10	-1,59		A1/10	-1,92		A1/10	-2,26
	A1/11	-1,50		A1/11	-1,57		A1/11	-1,89		A1/11	-2,21
	A1/12	-1,57		A1/12	-1,63		A1/12	-1,96		A1/12	-2,29
	A1/13	-1,52		A1/13	-1,58		A1/13	-1,92		A1/13	-2,25
	A1/14	-1,51		A1/14	-1,56		A1/14	-1,88		A1/14	-2,20
X+	A1/21	-1,08	X+	A1/15	-1,13	X+	A1/15	-1,36	X+	A1/15	-1,61
X-	A1/30	-1,04	X-	A1/24	-1,09	X-	A1/24	-1,31	X-	A1/24	-1,53
Y+	A1/31	-1,05	Y+	A1/31	-1,14	Y+	A1/31	-1,38	Y+	A1/31	-1,62
Y-	A1/37	-1,08	Y-	A1/37	-1,07	Y-	A1/37	-1,28	Y-	A1/37	-1,51
590	A1/1	-2,56	591	A1/1	-2,42	592	A1/1	-2,68	593	A1/1	-2,34
	A1/2	-2,52		A1/2	-2,38		A1/2	-2,65		A1/2	-2,30
	A1/3	-2,57		A1/3	-2,44		A1/3	-2,70		A1/3	-2,34
	A1/4	-2,53		A1/4	-2,40		A1/4	-2,67		A1/4	-2,30
	A1/5	-2,48		A1/5	-2,36		A1/5	-2,64		A1/5	-2,25
	A1/6	-2,58		A1/6	-2,45		A1/6	-2,73		A1/6	-2,35
	A1/7	-2,53		A1/7	-2,41		A1/7	-2,69		A1/7	-2,31
	A1/8	-2,50		A1/8	-2,39		A1/8	-2,68		A1/8	-2,27
	A1/9	-2,56		A1/9	-2,41		A1/9	-2,66		A1/9	-2,34
	A1/10	-2,51		A1/10	-2,37		A1/10	-2,63		A1/10	-2,30
	A1/11	-2,46		A1/11	-2,33		A1/11	-2,57		A1/11	-2,25
	A1/12	-2,55		A1/12	-2,40		A1/12	-2,64		A1/12	-2,33
	A1/13	-2,51		A1/13	-2,36		A1/13	-2,60		A1/13	-2,29
	A1/14	-2,45		A1/14	-2,30		A1/14	-2,53		A1/14	-2,24
X+	A1/15	-1,84	X+	A1/15	-1,84	X+	A1/15	-2,18	X+	A1/15	-1,57
X-	A1/24	-1,69	X-	A1/24	-1,60	X-	A1/24	-1,76	X-	A1/24	-1,58
Y+	A1/31	-1,86	Y+	A1/31	-1,88	Y+	A1/31	-2,27	Y+	A1/40	-1,62
Y-	A1/37	-1,66	Y-	A1/37	-1,53	Y-	A1/37	-1,61	Y-	A1/46	-1,49
594	A1/1	-1,50	595	A1/1	-2,34	596	A1/1	-1,08	597	A1/1	-0,86
	A1/2	-1,46		A1/2	-2,29		A1/2	-1,04		A1/2	-0,82
	A1/3	-1,50		A1/3	-2,34		A1/3	-1,08		A1/3	-0,86

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLU

Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	A1/4	-1,46		A1/4	-2,29		A1/4	-1,04		A1/4	-0,82
	A1/5	-1,44		A1/5	-2,24		A1/5	-1,03		A1/5	-0,82
	A1/6	-1,50		A1/6	-2,33		A1/6	-1,08		A1/6	-0,86
	A1/7	-1,46		A1/7	-2,29		A1/7	-1,04		A1/7	-0,82
	A1/8	-1,43		A1/8	-2,23		A1/8	-1,03		A1/8	-0,82
	A1/9	-1,50		A1/9	-2,33		A1/9	-1,08		A1/9	-0,86
	A1/10	-1,46		A1/10	-2,29		A1/10	-1,04		A1/10	-0,82
	A1/11	-1,43		A1/11	-2,23		A1/11	-1,03		A1/11	-0,82
	A1/12	-1,50		A1/12	-2,34		A1/12	-1,08		A1/12	-0,86
	A1/13	-1,46		A1/13	-2,30		A1/13	-1,04		A1/13	-0,82
	A1/14	-1,44		A1/14	-2,25		A1/14	-1,03		A1/14	-0,82
X+	A1/20	-1,01	X+	A1/20	-1,58	X+	A1/20	-0,72	X+	A1/21	-0,56
X-	A1/27	-0,97	X-	A1/27	-1,52	X-	A1/27	-0,71	X-	A1/30	-0,57
Y+	A1/34	-0,98	Y+	A1/34	-1,52	Y+	A1/34	-0,71	Y+	A1/40	-0,56
Y-	A1/36	-1,01	Y-	A1/36	-1,58	Y-	A1/36	-0,72	Y-	A1/46	-0,57
598	A1/1	-0,83	599	A1/1	-1,03	600	A1/1	-1,55	601	A1/1	-2,41
	A1/2	-0,79		A1/2	-0,99		A1/2	-1,51		A1/2	-2,38
	A1/3	-0,83		A1/3	-1,03		A1/3	-1,55		A1/3	-2,43
	A1/4	-0,79		A1/4	-0,99		A1/4	-1,52		A1/4	-2,40
	A1/5	-0,79		A1/5	-0,99		A1/5	-1,50		A1/5	-2,37
	A1/6	-0,83		A1/6	-1,02		A1/6	-1,53		A1/6	-2,37
	A1/7	-0,79		A1/7	-0,98		A1/7	-1,49		A1/7	-2,33
	A1/8	-0,78		A1/8	-0,97		A1/8	-1,45		A1/8	-2,26
	A1/9	-0,83		A1/9	-1,03		A1/9	-1,54		A1/9	-2,40
	A1/10	-0,79		A1/10	-0,99		A1/10	-1,50		A1/10	-2,36
	A1/11	-0,79		A1/11	-0,98		A1/11	-1,48		A1/11	-2,31
	A1/12	-0,83		A1/12	-1,04		A1/12	-1,57		A1/12	-2,46
	A1/13	-0,79		A1/13	-1,00		A1/13	-1,53		A1/13	-2,42
	A1/14	-0,79		A1/14	-1,00		A1/14	-1,53		A1/14	-2,41
X+	A1/20	-0,55	X+	A1/20	-0,72	X+	A1/20	-1,18	X+	A1/20	-1,97
X-	A1/27	-0,56	X-	A1/27	-0,70	X-	A1/27	-1,05	X-	A1/27	-1,61
Y+	A1/41	-0,53	Y+	A1/34	-0,63	Y+	A1/34	-0,93	Y+	A1/34	-1,44
Y-	A1/43	-0,57	Y-	A1/36	-0,76	Y-	A1/36	-1,25	Y-	A1/36	-2,08

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD

Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
1	SLD/1	-1,61	3	SLD/1	-3,08	4	SLD/1	-3,56	5	SLD/1	-3,26
	SLD/2	-1,59		SLD/2	-3,02		SLD/2	-3,48		SLD/2	-3,18
	SLD/3	-1,60		SLD/3	-3,08		SLD/3	-3,56		SLD/3	-3,25
	SLD/4	-1,58		SLD/4	-3,02		SLD/4	-3,47		SLD/4	-3,17
	SLD/5	-1,54		SLD/5	-2,97		SLD/5	-3,40		SLD/5	-3,11
	SLD/6	-1,58		SLD/6	-3,07		SLD/6	-3,56		SLD/6	-3,26
	SLD/7	-1,56		SLD/7	-3,02		SLD/7	-3,47		SLD/7	-3,18
	SLD/8	-1,51		SLD/8	-2,96		SLD/8	-3,41		SLD/8	-3,11
	SLD/9	-1,62		SLD/9	-3,08		SLD/9	-3,57		SLD/9	-3,26
	SLD/10	-1,61		SLD/10	-3,03		SLD/10	-3,48		SLD/10	-3,18
	SLD/11	-1,58		SLD/11	-2,98		SLD/11	-3,41		SLD/11	-3,12
	SLD/12	-1,64		SLD/12	-3,09		SLD/12	-3,57		SLD/12	-3,26
	SLD/13	-1,62		SLD/13	-3,03		SLD/13	-3,48		SLD/13	-3,18
	SLD/14	-1,61		SLD/14	-2,99		SLD/14	-3,41		SLD/14	-3,11
X+	SLD/20	-1,02	X+	SLD/20	-2,07	X+	SLD/20	-2,30	X+	SLD/18	-2,10
X-	SLD/27	-1,35	X-	SLD/27	-2,16	X-	SLD/27	-2,38	X-	SLD/25	-2,18
Y+	SLD/41	-0,84	Y+	SLD/41	-2,03	Y+	SLD/41	-2,35	Y+	SLD/41	-2,15
Y-	SLD/43	-1,44	Y-	SLD/43	-2,18	Y-	SLD/43	-2,35	Y-	SLD/43	-2,14
7	SLD/1	-3,34	8	SLD/1	-2,69	9	SLD/1	-3,35	10	SLD/1	-2,21
	SLD/2	-3,26		SLD/2	-2,64		SLD/2	-3,25		SLD/2	-2,19
	SLD/3	-3,34		SLD/3	-2,69		SLD/3	-3,35		SLD/3	-2,22
	SLD/4	-3,26		SLD/4	-2,65		SLD/4	-3,25		SLD/4	-2,20
	SLD/5	-3,20		SLD/5	-2,59		SLD/5	-3,17		SLD/5	-2,16
	SLD/6	-3,33		SLD/6	-2,64		SLD/6	-3,36		SLD/6	-2,15
	SLD/7	-3,25		SLD/7	-2,60		SLD/7	-3,26		SLD/7	-2,13
	SLD/8	-3,18		SLD/8	-2,51		SLD/8	-3,18		SLD/8	-2,04
	SLD/9	-3,34		SLD/9	-2,68		SLD/9	-3,35		SLD/9	-2,20
	SLD/10	-3,25		SLD/10	-2,64		SLD/10	-3,25		SLD/10	-2,18
	SLD/11	-3,18		SLD/11	-2,58		SLD/11	-3,16		SLD/11	-2,13
	SLD/12	-3,35		SLD/12	-2,73		SLD/12	-3,34		SLD/12	-2,27
	SLD/13	-3,26		SLD/13	-2,69		SLD/13	-3,24		SLD/13	-2,25
	SLD/14	-3,20		SLD/14	-2,66		SLD/14	-3,15		SLD/14	-2,24
X+	SLD/21	-2,26	X+	SLD/20	-1,95	X+	SLD/15	-2,18	X+	SLD/20	-1,81
X-	SLD/30	-2,15	X-	SLD/27	-1,88	X-	SLD/24	-2,10	X-	SLD/27	-1,58
Y+	SLD/31	-2,15	Y+	SLD/34	-1,38	Y+	SLD/31	-2,21	Y+	SLD/34	-1,02
Y-	SLD/37	-2,26	Y-	SLD/36	-2,23	Y-	SLD/37	-2,05	Y-	SLD/36	-2,12
12	SLD/1	-1,69	14	SLD/1	-2,94	15	SLD/1	-2,62	16	SLD/1	-3,17
	SLD/2	-1,67		SLD/2	-2,85		SLD/2	-2,59		SLD/2	-3,07
	SLD/3	-1,66		SLD/3	-2,94		SLD/3	-2,61		SLD/3	-3,17
	SLD/4	-1,65		SLD/4	-2,86		SLD/4	-2,58		SLD/4	-3,07

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/5	-1,61		SLD/5	-2,79		SLD/5	-2,52		SLD/5	-2,99
	SLD/6	-1,65		SLD/6	-2,95		SLD/6	-2,64		SLD/6	-3,17
	SLD/7	-1,64		SLD/7	-2,86		SLD/7	-2,60		SLD/7	-3,08
	SLD/8	-1,59		SLD/8	-2,80		SLD/8	-2,56		SLD/8	-3,01
	SLD/9	-1,71		SLD/9	-2,94		SLD/9	-2,63		SLD/9	-3,17
	SLD/10	-1,69		SLD/10	-2,85		SLD/10	-2,60		SLD/10	-3,08
	SLD/11	-1,68		SLD/11	-2,78		SLD/11	-2,55		SLD/11	-3,00
	SLD/12	-1,72		SLD/12	-2,93		SLD/12	-2,61		SLD/12	-3,16
	SLD/13	-1,70		SLD/13	-2,85		SLD/13	-2,57		SLD/13	-3,07
	SLD/14	-1,70		SLD/14	-2,77		SLD/14	-2,51		SLD/14	-2,99
X+	SLD/21	-1,00	X+	SLD/15	-1,92	X+	SLD/18	-1,70	X+	SLD/18	-2,01
X-	SLD/30	-1,55	X-	SLD/24	-1,86	X-	SLD/25	-1,96	X-	SLD/25	-2,06
Y+	SLD/40	-0,94	Y+	SLD/31	-1,95	Y+	SLD/41	-1,99	Y+	SLD/41	-2,08
Y-	SLD/46	-1,58	Y-	SLD/37	-1,81	Y-	SLD/43	-1,67	Y-	SLD/43	-1,97
17	SLD/1	-2,60	18	SLD/1	-2,64	19	SLD/1	-1,52	20	SLD/1	-2,11
	SLD/2	-2,54		SLD/2	-2,59		SLD/2	-1,51		SLD/2	-2,09
	SLD/3	-2,60		SLD/3	-2,64		SLD/3	-1,54		SLD/3	-2,09
	SLD/4	-2,54		SLD/4	-2,59		SLD/4	-1,52		SLD/4	-2,06
	SLD/5	-2,49		SLD/5	-2,54		SLD/5	-1,51		SLD/5	-2,01
	SLD/6	-2,60		SLD/6	-2,65		SLD/6	-1,56		SLD/6	-2,13
	SLD/7	-2,54		SLD/7	-2,60		SLD/7	-1,54		SLD/7	-2,11
	SLD/8	-2,49		SLD/8	-2,56		SLD/8	-1,54		SLD/8	-2,08
	SLD/9	-2,60		SLD/9	-2,64		SLD/9	-1,51		SLD/9	-2,13
	SLD/10	-2,53		SLD/10	-2,59		SLD/10	-1,49		SLD/10	-2,11
	SLD/11	-2,48		SLD/11	-2,54		SLD/11	-1,45		SLD/11	-2,08
	SLD/12	-2,59		SLD/12	-2,63		SLD/12	-1,49		SLD/12	-2,08
	SLD/13	-2,53		SLD/13	-2,57		SLD/13	-1,47		SLD/13	-2,06
	SLD/14	-2,48		SLD/14	-2,52		SLD/14	-1,42		SLD/14	-2,01
X+	SLD/15	-1,75	X+	SLD/15	-1,81	X+	SLD/15	-1,38	X+	SLD/18	-1,24
X-	SLD/24	-1,68	X-	SLD/24	-1,79	X-	SLD/24	-0,98	X-	SLD/25	-1,78
Y+	SLD/31	-1,77	Y+	SLD/31	-1,89	Y+	SLD/31	-1,46	Y+	SLD/41	-1,75
Y-	SLD/37	-1,66	Y-	SLD/37	-1,65	Y-	SLD/37	-0,83	Y-	SLD/43	-1,30
21	SLD/1	-3,30	22	SLD/1	-3,41	23	SLD/1	-4,47	24	SLD/1	-3,64
	SLD/2	-3,23		SLD/2	-3,31		SLD/2	-4,34		SLD/2	-3,58
	SLD/3	-3,30		SLD/3	-3,41		SLD/3	-4,47		SLD/3	-3,64
	SLD/4	-3,23		SLD/4	-3,31		SLD/4	-4,34		SLD/4	-3,58
	SLD/5	-3,17		SLD/5	-3,22		SLD/5	-4,22		SLD/5	-3,50
	SLD/6	-3,29		SLD/6	-3,41		SLD/6	-4,47		SLD/6	-3,63
	SLD/7	-3,22		SLD/7	-3,31		SLD/7	-4,34		SLD/7	-3,57
	SLD/8	-3,15		SLD/8	-3,22		SLD/8	-4,23		SLD/8	-3,48
	SLD/9	-3,29		SLD/9	-3,41		SLD/9	-4,48		SLD/9	-3,64
	SLD/10	-3,23		SLD/10	-3,31		SLD/10	-4,35		SLD/10	-3,58
	SLD/11	-3,16		SLD/11	-3,23		SLD/11	-4,23		SLD/11	-3,49
	SLD/12	-3,30		SLD/12	-3,41		SLD/12	-4,47		SLD/12	-3,65
	SLD/13	-3,24		SLD/13	-3,31		SLD/13	-4,34		SLD/13	-3,59
	SLD/14	-3,18		SLD/14	-3,22		SLD/14	-4,23		SLD/14	-3,51
X+	SLD/21	-2,26	X+	SLD/15	-2,14	X+	SLD/21	-2,78	X+	SLD/20	-2,44
X-	SLD/30	-2,16	X-	SLD/24	-2,18	X-	SLD/30	-2,86	X-	SLD/27	-2,41
Y+	SLD/31	-2,12	Y+	SLD/40	-2,17	Y+	SLD/40	-2,83	Y+	SLD/34	-2,32
Y-	SLD/37	-2,29	Y-	SLD/46	-2,16	Y-	SLD/46	-2,83	Y-	SLD/36	-2,49
25	SLD/1	-1,81	31	SLD/1	-1,61	32	SLD/1	-1,61	65	SLD/1	-2,95
	SLD/2	-1,80		SLD/2	-1,60		SLD/2	-1,59		SLD/2	-2,91
	SLD/3	-1,80		SLD/3	-1,63		SLD/3	-1,62		SLD/3	-2,94
	SLD/4	-1,78		SLD/4	-1,62		SLD/4	-1,61		SLD/4	-2,90
	SLD/5	-1,74		SLD/5	-1,60		SLD/5	-1,59		SLD/5	-2,84
	SLD/6	-1,84		SLD/6	-1,58		SLD/6	-1,64		SLD/6	-2,90
	SLD/7	-1,83		SLD/7	-1,56		SLD/7	-1,63		SLD/7	-2,86
	SLD/8	-1,81		SLD/8	-1,51		SLD/8	-1,62		SLD/8	-2,78
	SLD/9	-1,83		SLD/9	-1,60		SLD/9	-1,59		SLD/9	-2,96
	SLD/10	-1,81		SLD/10	-1,58		SLD/10	-1,58		SLD/10	-2,92
	SLD/11	-1,79		SLD/11	-1,54		SLD/11	-1,53		SLD/11	-2,87
	SLD/12	-1,78		SLD/12	-1,65		SLD/12	-1,57		SLD/12	-2,99
	SLD/13	-1,77		SLD/13	-1,64		SLD/13	-1,56		SLD/13	-2,96
	SLD/14	-1,72		SLD/14	-1,63		SLD/14	-1,50		SLD/14	-2,93
X+	SLD/15	-1,15	X+	SLD/20	-1,46	X+	SLD/15	-1,43	X+	SLD/21	-2,02
X-	SLD/24	-1,51	X-	SLD/27	-1,05	X-	SLD/24	-0,99	X-	SLD/30	-2,29
Y+	SLD/40	-1,58	Y+	SLD/34	-0,91	Y+	SLD/31	-1,52	Y+	SLD/40	-1,60
Y-	SLD/46	-1,02	Y-	SLD/36	-1,55	Y-	SLD/37	-0,83	Y-	SLD/46	-2,51
66	SLD/1	-2,57	67	SLD/1	-2,39	68	SLD/1	-1,54	69	SLD/1	-1,42
	SLD/2	-2,53		SLD/2	-2,33		SLD/2	-1,51		SLD/2	-1,39
	SLD/3	-2,56		SLD/3	-2,39		SLD/3	-1,54		SLD/3	-1,42
	SLD/4	-2,52		SLD/4	-2,33		SLD/4	-1,50		SLD/4	-1,38
	SLD/5	-2,47		SLD/5	-2,28		SLD/5	-1,48		SLD/5	-1,36
	SLD/6	-2,54		SLD/6	-2,39		SLD/6	-1,54		SLD/6	-1,42
	SLD/7	-2,50		SLD/7	-2,34		SLD/7	-1,51		SLD/7	-1,38
	SLD/8	-2,44		SLD/8	-2,29		SLD/8	-1,48		SLD/8	-1,36
	SLD/9	-2,58		SLD/9	-2,39		SLD/9	-1,54		SLD/9	-1,42
	SLD/10	-2,54		SLD/10	-2,34		SLD/10	-1,51		SLD/10	-1,39

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/11	-2,51		SLD/11	-2,29		SLD/11	-1,48		SLD/11	-1,36
	SLD/12	-2,60		SLD/12	-2,39		SLD/12	-1,54		SLD/12	-1,42
	SLD/13	-2,56		SLD/13	-2,33		SLD/13	-1,51		SLD/13	-1,39
	SLD/14	-2,53		SLD/14	-2,29		SLD/14	-1,48		SLD/14	-1,36
X+	SLD/20	-1,68	X+	SLD/18	-1,55	X+	SLD/20	-1,00	X+	SLD/20	-0,92
X-	SLD/27	-1,98	X-	SLD/25	-1,62	X-	SLD/27	-1,04	X-	SLD/27	-0,96
Y+	SLD/41	-1,53	Y+	SLD/41	-1,61	Y+	SLD/41	-1,02	Y+	SLD/41	-0,93
Y-	SLD/43	-2,06	Y-	SLD/43	-1,57	Y-	SLD/43	-1,03	Y-	SLD/43	-0,96
70	SLD/1	-2,12	71	SLD/1	-1,62	72	SLD/1	-1,32	73	SLD/1	-1,39
	SLD/2	-2,08		SLD/2	-1,57		SLD/2	-1,27		SLD/2	-1,35
	SLD/3	-2,12		SLD/3	-1,62		SLD/3	-1,32		SLD/3	-1,39
	SLD/4	-2,08		SLD/4	-1,57		SLD/4	-1,27		SLD/4	-1,35
	SLD/5	-2,04		SLD/5	-1,55		SLD/5	-1,26		SLD/5	-1,33
	SLD/6	-2,12		SLD/6	-1,62		SLD/6	-1,32		SLD/6	-1,39
	SLD/7	-2,08		SLD/7	-1,58		SLD/7	-1,28		SLD/7	-1,35
	SLD/8	-2,04		SLD/8	-1,56		SLD/8	-1,26		SLD/8	-1,33
	SLD/9	-2,12		SLD/9	-1,62		SLD/9	-1,32		SLD/9	-1,39
	SLD/10	-2,08		SLD/10	-1,57		SLD/10	-1,27		SLD/10	-1,35
	SLD/11	-2,04		SLD/11	-1,55		SLD/11	-1,26		SLD/11	-1,33
	SLD/12	-2,13		SLD/12	-1,62		SLD/12	-1,32		SLD/12	-1,39
	SLD/13	-2,08		SLD/13	-1,57		SLD/13	-1,27		SLD/13	-1,35
	SLD/14	-2,05		SLD/14	-1,55		SLD/14	-1,26		SLD/14	-1,33
X+	SLD/21	-1,43	X+	SLD/18	-1,09	X+	SLD/18	-0,87	X+	SLD/20	-0,91
X-	SLD/30	-1,43	X-	SLD/25	-1,09	X-	SLD/25	-0,88	X-	SLD/27	-0,93
Y+	SLD/40	-1,38	Y+	SLD/41	-1,10	Y+	SLD/41	-0,88	Y+	SLD/41	-0,90
Y-	SLD/46	-1,46	Y-	SLD/43	-1,06	Y-	SLD/43	-0,87	Y-	SLD/43	-0,93
74	SLD/1	-2,25	75	SLD/1	-1,70	76	SLD/1	-1,26	77	SLD/1	-1,33
	SLD/2	-2,20		SLD/2	-1,65		SLD/2	-1,21		SLD/2	-1,29
	SLD/3	-2,26		SLD/3	-1,70		SLD/3	-1,26		SLD/3	-1,33
	SLD/4	-2,21		SLD/4	-1,65		SLD/4	-1,22		SLD/4	-1,30
	SLD/5	-2,17		SLD/5	-1,63		SLD/5	-1,20		SLD/5	-1,27
	SLD/6	-2,25		SLD/6	-1,70		SLD/6	-1,25		SLD/6	-1,33
	SLD/7	-2,20		SLD/7	-1,65		SLD/7	-1,21		SLD/7	-1,29
	SLD/8	-2,15		SLD/8	-1,62		SLD/8	-1,20		SLD/8	-1,26
	SLD/9	-2,25		SLD/9	-1,69		SLD/9	-1,25		SLD/9	-1,33
	SLD/10	-2,20		SLD/10	-1,64		SLD/10	-1,21		SLD/10	-1,29
	SLD/11	-2,15		SLD/11	-1,62		SLD/11	-1,20		SLD/11	-1,27
	SLD/12	-2,26		SLD/12	-1,70		SLD/12	-1,26		SLD/12	-1,34
	SLD/13	-2,21		SLD/13	-1,65		SLD/13	-1,22		SLD/13	-1,30
	SLD/14	-2,17		SLD/14	-1,62		SLD/14	-1,20		SLD/14	-1,28
X+	SLD/21	-1,56	X+	SLD/21	-1,16	X+	SLD/21	-0,85	X+	SLD/21	-0,90
X-	SLD/30	-1,45	X-	SLD/30	-1,10	X-	SLD/30	-0,82	X-	SLD/30	-0,87
Y+	SLD/31	-1,47	Y+	SLD/31	-1,13	Y+	SLD/31	-0,81	Y+	SLD/31	-0,83
Y-	SLD/37	-1,55	Y-	SLD/37	-1,14	Y-	SLD/37	-0,86	Y-	SLD/37	-0,92
78	SLD/1	-1,99	79	SLD/1	-1,42	80	SLD/1	-1,28	81	SLD/1	-1,42
	SLD/2	-1,95		SLD/2	-1,38		SLD/2	-1,24		SLD/2	-1,38
	SLD/3	-1,99		SLD/3	-1,42		SLD/3	-1,28		SLD/3	-1,42
	SLD/4	-1,95		SLD/4	-1,38		SLD/4	-1,24		SLD/4	-1,38
	SLD/5	-1,91		SLD/5	-1,36		SLD/5	-1,22		SLD/5	-1,35
	SLD/6	-1,98		SLD/6	-1,42		SLD/6	-1,28		SLD/6	-1,42
	SLD/7	-1,94		SLD/7	-1,38		SLD/7	-1,24		SLD/7	-1,37
	SLD/8	-1,90		SLD/8	-1,36		SLD/8	-1,22		SLD/8	-1,33
	SLD/9	-1,99		SLD/9	-1,42		SLD/9	-1,28		SLD/9	-1,42
	SLD/10	-1,94		SLD/10	-1,38		SLD/10	-1,24		SLD/10	-1,37
	SLD/11	-1,91		SLD/11	-1,36		SLD/11	-1,22		SLD/11	-1,34
	SLD/12	-1,99		SLD/12	-1,42		SLD/12	-1,28		SLD/12	-1,43
	SLD/13	-1,95		SLD/13	-1,37		SLD/13	-1,24		SLD/13	-1,38
	SLD/14	-1,92		SLD/14	-1,35		SLD/14	-1,22		SLD/14	-1,35
X+	SLD/21	-1,36	X+	SLD/15	-0,96	X+	SLD/21	-0,84	X+	SLD/20	-0,93
X-	SLD/30	-1,31	X-	SLD/24	-0,94	X-	SLD/30	-0,82	X-	SLD/27	-0,90
Y+	SLD/31	-1,28	Y+	SLD/31	-0,98	Y+	SLD/31	-0,83	Y+	SLD/34	-0,85
Y-	SLD/37	-1,38	Y-	SLD/37	-0,91	Y-	SLD/37	-0,84	Y-	SLD/36	-0,96
82	SLD/1	-3,35	83	SLD/1	-2,89	84	SLD/1	-2,70	85	SLD/1	-3,02
	SLD/2	-3,27		SLD/2	-2,81		SLD/2	-2,62		SLD/2	-2,94
	SLD/3	-3,36		SLD/3	-2,89		SLD/3	-2,70		SLD/3	-3,03
	SLD/4	-3,28		SLD/4	-2,82		SLD/4	-2,62		SLD/4	-2,94
	SLD/5	-3,23		SLD/5	-2,77		SLD/5	-2,57		SLD/5	-2,86
	SLD/6	-3,36		SLD/6	-2,90		SLD/6	-2,70		SLD/6	-3,03
	SLD/7	-3,28		SLD/7	-2,82		SLD/7	-2,63		SLD/7	-2,94
	SLD/8	-3,24		SLD/8	-2,78		SLD/8	-2,57		SLD/8	-2,88
	SLD/9	-3,34		SLD/9	-2,88		SLD/9	-2,69		SLD/9	-3,02
	SLD/10	-3,27		SLD/10	-2,80		SLD/10	-2,61		SLD/10	-2,94
	SLD/11	-3,22		SLD/11	-2,75		SLD/11	-2,55		SLD/11	-2,86
	SLD/12	-3,34		SLD/12	-2,88		SLD/12	-2,69		SLD/12	-3,02
	SLD/13	-3,26		SLD/13	-2,80		SLD/13	-2,61		SLD/13	-2,93
	SLD/14	-3,21		SLD/14	-2,74		SLD/14	-2,55		SLD/14	-2,85
X+	SLD/18	-2,35	X+	SLD/15	-2,02	X+	SLD/15	-1,82	X+	SLD/18	-1,95
X-	SLD/25	-2,22	X-	SLD/24	-1,85	X-	SLD/24	-1,69	X-	SLD/25	-1,94

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	Y+ SLD/34	-2,38		Y+ SLD/31	-2,04		Y+ SLD/31	-1,82		Y+ SLD/34	-2,01
	Y- SLD/36	-2,17		Y- SLD/37	-1,81		Y- SLD/37	-1,70		Y- SLD/36	-1,84
86	SLD/1	-2,80	87	SLD/1	-2,63	88	SLD/1	-2,38	89	SLD/1	-1,74
	SLD/2	-2,72		SLD/2	-2,56		SLD/2	-2,32		SLD/2	-1,70
	SLD/3	-2,80		SLD/3	-2,63		SLD/3	-2,38		SLD/3	-1,74
	SLD/4	-2,72		SLD/4	-2,56		SLD/4	-2,32		SLD/4	-1,70
	SLD/5	-2,65		SLD/5	-2,49		SLD/5	-2,28		SLD/5	-1,67
	SLD/6	-2,81		SLD/6	-2,64		SLD/6	-2,38		SLD/6	-1,74
	SLD/7	-2,72		SLD/7	-2,56		SLD/7	-2,32		SLD/7	-1,70
	SLD/8	-2,66		SLD/8	-2,50		SLD/8	-2,27		SLD/8	-1,67
	SLD/9	-2,80		SLD/9	-2,64		SLD/9	-2,37		SLD/9	-1,74
	SLD/10	-2,72		SLD/10	-2,56		SLD/10	-2,32		SLD/10	-1,70
	SLD/11	-2,66		SLD/11	-2,50		SLD/11	-2,27		SLD/11	-1,66
	SLD/12	-2,80		SLD/12	-2,63		SLD/12	-2,38		SLD/12	-1,74
	SLD/13	-2,72		SLD/13	-2,56		SLD/13	-2,32		SLD/13	-1,70
	SLD/14	-2,65		SLD/14	-2,49		SLD/14	-2,27		SLD/14	-1,67
X+	SLD/18	-1,78	X+	SLD/18	-1,66	X+	SLD/21	-1,60	X+	SLD/21	-1,17
X-	SLD/25	-1,81	X-	SLD/25	-1,70	X-	SLD/30	-1,53	X-	SLD/30	-1,12
Y+	SLD/41	-1,83	Y+	SLD/41	-1,70	Y+	SLD/31	-1,57	Y+	SLD/31	-1,16
Y-	SLD/43	-1,74	Y-	SLD/43	-1,66	Y-	SLD/37	-1,58	Y-	SLD/37	-1,16
90	SLD/1	-1,65	91	SLD/1	-2,05	92	SLD/1	-1,51	93	SLD/1	-1,76
	SLD/2	-1,61		SLD/2	-1,99		SLD/2	-1,47		SLD/2	-1,72
	SLD/3	-1,66		SLD/3	-2,05		SLD/3	-1,51		SLD/3	-1,76
	SLD/4	-1,62		SLD/4	-2,00		SLD/4	-1,47		SLD/4	-1,72
	SLD/5	-1,59		SLD/5	-1,95		SLD/5	-1,44		SLD/5	-1,69
	SLD/6	-1,65		SLD/6	-2,07		SLD/6	-1,52		SLD/6	-1,77
	SLD/7	-1,61		SLD/7	-2,01		SLD/7	-1,48		SLD/7	-1,73
	SLD/8	-1,58		SLD/8	-1,97		SLD/8	-1,46		SLD/8	-1,71
	SLD/9	-1,65		SLD/9	-2,05		SLD/9	-1,51		SLD/9	-1,76
	SLD/10	-1,61		SLD/10	-1,99		SLD/10	-1,47		SLD/10	-1,72
	SLD/11	-1,58		SLD/11	-1,94		SLD/11	-1,44		SLD/11	-1,69
	SLD/12	-1,65		SLD/12	-2,03		SLD/12	-1,50		SLD/12	-1,75
	SLD/13	-1,61		SLD/13	-1,98		SLD/13	-1,46		SLD/13	-1,71
	SLD/14	-1,58		SLD/14	-1,91		SLD/14	-1,42		SLD/14	-1,67
X+	SLD/15	-1,11	X+	SLD/15	-1,38	X+	SLD/15	-1,02	X+	SLD/15	-1,20
X-	SLD/24	-1,06	X-	SLD/24	-1,34	X-	SLD/24	-1,00	X-	SLD/24	-1,19
Y+	SLD/31	-1,10	Y+	SLD/31	-1,49	Y+	SLD/31	-1,09	Y+	SLD/31	-1,26
Y-	SLD/37	-1,09	Y-	SLD/37	-1,15	Y-	SLD/37	-0,88	Y-	SLD/37	-1,08
94	SLD/1	-2,63	95	SLD/1	-2,32	96	SLD/1	-2,43	97	SLD/1	-3,13
	SLD/2	-2,59		SLD/2	-2,28		SLD/2	-2,39		SLD/2	-3,09
	SLD/3	-2,62		SLD/3	-2,31		SLD/3	-2,41		SLD/3	-3,11
	SLD/4	-2,58		SLD/4	-2,27		SLD/4	-2,38		SLD/4	-3,07
	SLD/5	-2,52		SLD/5	-2,23		SLD/5	-2,33		SLD/5	-3,00
	SLD/6	-2,65		SLD/6	-2,34		SLD/6	-2,45		SLD/6	-3,15
	SLD/7	-2,61		SLD/7	-2,30		SLD/7	-2,41		SLD/7	-3,12
	SLD/8	-2,58		SLD/8	-2,28		SLD/8	-2,39		SLD/8	-3,08
	SLD/9	-2,64		SLD/9	-2,33		SLD/9	-2,44		SLD/9	-3,16
	SLD/10	-2,60		SLD/10	-2,29		SLD/10	-2,41		SLD/10	-3,12
	SLD/11	-2,56		SLD/11	-2,26		SLD/11	-2,38		SLD/11	-3,08
	SLD/12	-2,60		SLD/12	-2,30		SLD/12	-2,41		SLD/12	-3,11
	SLD/13	-2,56		SLD/13	-2,26		SLD/13	-2,38		SLD/13	-3,07
	SLD/14	-2,50		SLD/14	-2,21		SLD/14	-2,33		SLD/14	-3,00
X+	SLD/18	-1,75	X+	SLD/18	-1,53	X+	SLD/18	-1,53	X+	SLD/18	-1,88
X-	SLD/25	-2,01	X-	SLD/25	-1,79	X-	SLD/25	-1,92	X-	SLD/25	-2,55
Y+	SLD/41	-2,10	Y+	SLD/41	-1,84	Y+	SLD/41	-1,90	Y+	SLD/41	-2,48
Y-	SLD/43	-1,60	Y-	SLD/43	-1,45	Y-	SLD/43	-1,57	Y-	SLD/43	-2,02
98	SLD/1	-2,86	99	SLD/1	-2,71	100	SLD/1	-2,91	101	SLD/1	-3,66
	SLD/2	-2,77		SLD/2	-2,62		SLD/2	-2,83		SLD/2	-3,58
	SLD/3	-2,86		SLD/3	-2,71		SLD/3	-2,92		SLD/3	-3,67
	SLD/4	-2,77		SLD/4	-2,62		SLD/4	-2,83		SLD/4	-3,58
	SLD/5	-2,71		SLD/5	-2,58		SLD/5	-2,78		SLD/5	-3,52
	SLD/6	-2,87		SLD/6	-2,71		SLD/6	-2,91		SLD/6	-3,65
	SLD/7	-2,78		SLD/7	-2,62		SLD/7	-2,82		SLD/7	-3,56
	SLD/8	-2,73		SLD/8	-2,58		SLD/8	-2,77		SLD/8	-3,48
	SLD/9	-2,86		SLD/9	-2,71		SLD/9	-2,91		SLD/9	-3,66
	SLD/10	-2,78		SLD/10	-2,62		SLD/10	-2,82		SLD/10	-3,57
	SLD/11	-2,71		SLD/11	-2,57		SLD/11	-2,77		SLD/11	-3,50
	SLD/12	-2,85		SLD/12	-2,70		SLD/12	-2,92		SLD/12	-3,68
	SLD/13	-2,77		SLD/13	-2,62		SLD/13	-2,83		SLD/13	-3,59
	SLD/14	-2,70		SLD/14	-2,57		SLD/14	-2,79		SLD/14	-3,53
X+	SLD/18	-1,85	X+	SLD/18	-1,78	X+	SLD/21	-1,97	X+	SLD/21	-2,52
X-	SLD/25	-1,87	X-	SLD/25	-1,75	X-	SLD/30	-1,89	X-	SLD/30	-2,39
Y+	SLD/41	-1,92	Y+	SLD/34	-1,78	Y+	SLD/31	-1,86	Y+	SLD/31	-2,31
Y-	SLD/43	-1,76	Y-	SLD/36	-1,74	Y-	SLD/37	-1,98	Y-	SLD/37	-2,57
102	SLD/1	-1,60	103	SLD/1	-1,47	104	SLD/1	-1,39	105	SLD/1	-1,59
	SLD/2	-1,56		SLD/2	-1,42		SLD/2	-1,35		SLD/2	-1,55
	SLD/3	-1,60		SLD/3	-1,47		SLD/3	-1,39		SLD/3	-1,59

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/4	-1,56		SLD/4	-1,42		SLD/4	-1,34		SLD/4	-1,55
	SLD/5	-1,52		SLD/5	-1,40		SLD/5	-1,32		SLD/5	-1,51
	SLD/6	-1,60		SLD/6	-1,47		SLD/6	-1,38		SLD/6	-1,59
	SLD/7	-1,56		SLD/7	-1,42		SLD/7	-1,34		SLD/7	-1,54
	SLD/8	-1,53		SLD/8	-1,40		SLD/8	-1,31		SLD/8	-1,50
	SLD/9	-1,60		SLD/9	-1,47		SLD/9	-1,39		SLD/9	-1,60
	SLD/10	-1,56		SLD/10	-1,43		SLD/10	-1,35		SLD/10	-1,55
	SLD/11	-1,53		SLD/11	-1,40		SLD/11	-1,32		SLD/11	-1,51
	SLD/12	-1,60		SLD/12	-1,47		SLD/12	-1,39		SLD/12	-1,60
	SLD/13	-1,55		SLD/13	-1,42		SLD/13	-1,35		SLD/13	-1,55
	SLD/14	-1,52		SLD/14	-1,40		SLD/14	-1,32		SLD/14	-1,52
X+	SLD/18	-1,03	X+	SLD/21	-0,94	X+	SLD/21	-0,90	X+	SLD/21	-1,03
X-	SLD/25	-1,07	X-	SLD/30	-0,97	X-	SLD/30	-0,92	X-	SLD/30	-1,04
Y+	SLD/41	-1,07	Y+	SLD/40	-0,95	Y+	SLD/40	-0,86	Y+	SLD/40	-0,97
Y-	SLD/43	-1,03	Y-	SLD/46	-0,97	Y-	SLD/46	-0,94	Y-	SLD/46	-1,08
106	SLD/1	-1,49	107	SLD/1	-1,65	108	SLD/1	-1,43	109	SLD/1	-1,30
	SLD/2	-1,45		SLD/2	-1,60		SLD/2	-1,38		SLD/2	-1,26
	SLD/3	-1,49		SLD/3	-1,65		SLD/3	-1,43		SLD/3	-1,30
	SLD/4	-1,45		SLD/4	-1,60		SLD/4	-1,38		SLD/4	-1,26
	SLD/5	-1,43		SLD/5	-1,57		SLD/5	-1,35		SLD/5	-1,23
	SLD/6	-1,50		SLD/6	-1,66		SLD/6	-1,43		SLD/6	-1,29
	SLD/7	-1,46		SLD/7	-1,61		SLD/7	-1,38		SLD/7	-1,26
	SLD/8	-1,43		SLD/8	-1,58		SLD/8	-1,36		SLD/8	-1,22
	SLD/9	-1,49		SLD/9	-1,65		SLD/9	-1,43		SLD/9	-1,30
	SLD/10	-1,45		SLD/10	-1,60		SLD/10	-1,38		SLD/10	-1,26
	SLD/11	-1,42		SLD/11	-1,57		SLD/11	-1,35		SLD/11	-1,23
	SLD/12	-1,49		SLD/12	-1,65		SLD/12	-1,43		SLD/12	-1,30
	SLD/13	-1,45		SLD/13	-1,60		SLD/13	-1,38		SLD/13	-1,26
	SLD/14	-1,41		SLD/14	-1,57		SLD/14	-1,35		SLD/14	-1,23
X+	SLD/15	-1,01	X+	SLD/15	-1,10	X+	SLD/15	-0,92	X+	SLD/21	-0,82
X-	SLD/24	-0,97	X-	SLD/24	-1,08	X-	SLD/24	-0,92	X-	SLD/30	-0,83
Y+	SLD/31	-1,04	Y+	SLD/31	-1,12	Y+	SLD/40	-0,92	Y+	SLD/40	-0,81
Y-	SLD/37	-0,92	Y-	SLD/37	-1,03	Y-	SLD/46	-0,91	Y-	SLD/46	-0,84
110	SLD/1	-1,58	111	SLD/1	-1,70	112	SLD/1	-1,81	113	SLD/1	-2,13
	SLD/2	-1,56		SLD/2	-1,67		SLD/2	-1,78		SLD/2	-2,10
	SLD/3	-1,58		SLD/3	-1,70		SLD/3	-1,81		SLD/3	-2,13
	SLD/4	-1,56		SLD/4	-1,67		SLD/4	-1,78		SLD/4	-2,10
	SLD/5	-1,53		SLD/5	-1,64		SLD/5	-1,75		SLD/5	-2,05
	SLD/6	-1,59		SLD/6	-1,70		SLD/6	-1,81		SLD/6	-2,12
	SLD/7	-1,56		SLD/7	-1,67		SLD/7	-1,78		SLD/7	-2,09
	SLD/8	-1,54		SLD/8	-1,64		SLD/8	-1,74		SLD/8	-2,04
	SLD/9	-1,58		SLD/9	-1,70		SLD/9	-1,81		SLD/9	-2,13
	SLD/10	-1,56		SLD/10	-1,67		SLD/10	-1,78		SLD/10	-2,10
	SLD/11	-1,53		SLD/11	-1,64		SLD/11	-1,75		SLD/11	-2,05
	SLD/12	-1,58		SLD/12	-1,69		SLD/12	-1,81		SLD/12	-2,14
	SLD/13	-1,55		SLD/13	-1,67		SLD/13	-1,79		SLD/13	-2,10
	SLD/14	-1,52		SLD/14	-1,64		SLD/14	-1,75		SLD/14	-2,06
X+	SLD/15	-1,09	X+	SLD/15	-1,15	X+	SLD/20	-1,22	X+	SLD/20	-1,44
X-	SLD/24	-1,09	X-	SLD/24	-1,15	X-	SLD/27	-1,23	X-	SLD/27	-1,44
Y+	SLD/31	-1,13	Y+	SLD/40	-1,16	Y+	SLD/41	-1,18	Y+	SLD/41	-1,34
Y-	SLD/37	-1,01	Y-	SLD/46	-1,13	Y-	SLD/43	-1,25	Y-	SLD/43	-1,49
114	SLD/1	-2,19	115	SLD/1	-2,82	116	SLD/1	-2,34	117	SLD/1	-2,85
	SLD/2	-2,15		SLD/2	-2,77		SLD/2	-2,30		SLD/2	-2,81
	SLD/3	-2,19		SLD/3	-2,82		SLD/3	-2,33		SLD/3	-2,83
	SLD/4	-2,16		SLD/4	-2,77		SLD/4	-2,30		SLD/4	-2,80
	SLD/5	-2,12		SLD/5	-2,73		SLD/5	-2,26		SLD/5	-2,74
	SLD/6	-2,19		SLD/6	-2,81		SLD/6	-2,34		SLD/6	-2,86
	SLD/7	-2,15		SLD/7	-2,77		SLD/7	-2,30		SLD/7	-2,83
	SLD/8	-2,11		SLD/8	-2,72		SLD/8	-2,27		SLD/8	-2,80
	SLD/9	-2,19		SLD/9	-2,82		SLD/9	-2,34		SLD/9	-2,86
	SLD/10	-2,15		SLD/10	-2,78		SLD/10	-2,31		SLD/10	-2,83
	SLD/11	-2,11		SLD/11	-2,74		SLD/11	-2,28		SLD/11	-2,80
	SLD/12	-2,20		SLD/12	-2,83		SLD/12	-2,34		SLD/12	-2,83
	SLD/13	-2,16		SLD/13	-2,78		SLD/13	-2,31		SLD/13	-2,80
	SLD/14	-2,12		SLD/14	-2,75		SLD/14	-2,28		SLD/14	-2,74
X+	SLD/21	-1,51	X+	SLD/21	-1,94	X+	SLD/21	-1,54	X+	SLD/15	-1,81
X-	SLD/30	-1,46	X-	SLD/30	-1,98	X-	SLD/30	-1,73	X-	SLD/24	-2,23
Y+	SLD/31	-1,44	Y+	SLD/40	-1,87	Y+	SLD/40	-1,63	Y+	SLD/40	-2,19
Y-	SLD/37	-1,52	Y-	SLD/46	-2,02	Y-	SLD/46	-1,68	Y-	SLD/46	-1,90
118	SLD/1	-1,58	119	SLD/1	-1,22	120	SLD/1	-1,67	121	SLD/1	-2,19
	SLD/2	-1,53		SLD/2	-1,18		SLD/2	-1,62		SLD/2	-2,15
	SLD/3	-1,58		SLD/3	-1,22		SLD/3	-1,67		SLD/3	-2,19
	SLD/4	-1,53		SLD/4	-1,18		SLD/4	-1,62		SLD/4	-2,15
	SLD/5	-1,50		SLD/5	-1,16		SLD/5	-1,59		SLD/5	-2,10
	SLD/6	-1,59		SLD/6	-1,23		SLD/6	-1,67		SLD/6	-2,20
	SLD/7	-1,54		SLD/7	-1,18		SLD/7	-1,62		SLD/7	-2,16
	SLD/8	-1,51		SLD/8	-1,17		SLD/8	-1,60		SLD/8	-2,12
	SLD/9	-1,58		SLD/9	-1,22		SLD/9	-1,67		SLD/9	-2,20

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/10	-1,53		SLD/10	-1,18		SLD/10	-1,62		SLD/10	-2,15
	SLD/11	-1,50		SLD/11	-1,16		SLD/11	-1,60		SLD/11	-2,12
	SLD/12	-1,58		SLD/12	-1,22		SLD/12	-1,67		SLD/12	-2,19
	SLD/13	-1,53		SLD/13	-1,18		SLD/13	-1,62		SLD/13	-2,15
	SLD/14	-1,49		SLD/14	-1,16		SLD/14	-1,59		SLD/14	-2,10
X+	SLD/18	-1,03	X+	SLD/18	-0,81	X+	SLD/15	-1,10	X+	SLD/15	-1,43
X-	SLD/25	-1,04	X-	SLD/25	-0,81	X-	SLD/24	-1,13	X-	SLD/24	-1,52
Y+	SLD/41	-1,08	Y+	SLD/41	-0,84	Y+	SLD/40	-1,13	Y+	SLD/40	-1,52
Y-	SLD/43	-0,95	Y-	SLD/43	-0,76	Y-	SLD/46	-1,09	Y-	SLD/46	-1,44
122	SLD/1	-1,39	123	SLD/1	-1,24	124	SLD/1	-1,48	125	SLD/1	-2,00
	SLD/2	-1,35		SLD/2	-1,20		SLD/2	-1,44		SLD/2	-1,96
	SLD/3	-1,39		SLD/3	-1,24		SLD/3	-1,48		SLD/3	-2,00
	SLD/4	-1,34		SLD/4	-1,20		SLD/4	-1,44		SLD/4	-1,96
	SLD/5	-1,31		SLD/5	-1,18		SLD/5	-1,42		SLD/5	-1,92
	SLD/6	-1,39		SLD/6	-1,24		SLD/6	-1,48		SLD/6	-2,00
	SLD/7	-1,35		SLD/7	-1,20		SLD/7	-1,44		SLD/7	-1,96
	SLD/8	-1,32		SLD/8	-1,18		SLD/8	-1,42		SLD/8	-1,93
	SLD/9	-1,39		SLD/9	-1,24		SLD/9	-1,48		SLD/9	-2,00
	SLD/10	-1,35		SLD/10	-1,20		SLD/10	-1,44		SLD/10	-1,96
	SLD/11	-1,32		SLD/11	-1,18		SLD/11	-1,42		SLD/11	-1,92
	SLD/12	-1,39		SLD/12	-1,24		SLD/12	-1,49		SLD/12	-2,00
	SLD/13	-1,34		SLD/13	-1,20		SLD/13	-1,44		SLD/13	-1,96
	SLD/14	-1,31		SLD/14	-1,18		SLD/14	-1,42		SLD/14	-1,92
X+	SLD/15	-0,88	X+	SLD/15	-0,80	X+	SLD/20	-0,99	X+	SLD/18	-1,35
X-	SLD/24	-0,90	X-	SLD/24	-0,81	X-	SLD/27	-0,98	X-	SLD/25	-1,32
Y+	SLD/40	-0,90	Y+	SLD/40	-0,80	Y+	SLD/34	-0,97	Y+	SLD/34	-1,35
Y-	SLD/46	-0,87	Y-	SLD/46	-0,80	Y-	SLD/36	-0,99	Y-	SLD/36	-1,31
126	SLD/1	-3,84	127	SLD/1	-2,95	128	SLD/1	-4,00	129	SLD/1	-4,38
	SLD/2	-3,75		SLD/2	-2,87		SLD/2	-3,89		SLD/2	-4,30
	SLD/3	-3,84		SLD/3	-2,95		SLD/3	-4,00		SLD/3	-4,38
	SLD/4	-3,75		SLD/4	-2,87		SLD/4	-3,89		SLD/4	-4,30
	SLD/5	-3,68		SLD/5	-2,83		SLD/5	-3,85		SLD/5	-4,21
	SLD/6	-3,83		SLD/6	-2,95		SLD/6	-4,00		SLD/6	-4,39
	SLD/7	-3,75		SLD/7	-2,86		SLD/7	-3,89		SLD/7	-4,31
	SLD/8	-3,67		SLD/8	-2,83		SLD/8	-3,84		SLD/8	-4,23
	SLD/9	-3,84		SLD/9	-2,95		SLD/9	-4,00		SLD/9	-4,38
	SLD/10	-3,75		SLD/10	-2,87		SLD/10	-3,89		SLD/10	-4,30
	SLD/11	-3,68		SLD/11	-2,83		SLD/11	-3,85		SLD/11	-4,22
	SLD/12	-3,84		SLD/12	-2,96		SLD/12	-4,01		SLD/12	-4,37
	SLD/13	-3,75		SLD/13	-2,87		SLD/13	-3,90		SLD/13	-4,29
	SLD/14	-3,68		SLD/14	-2,84		SLD/14	-3,86		SLD/14	-4,20
X+	SLD/20	-2,54	X+	SLD/20	-1,98	X+	SLD/20	-2,69	X+	SLD/15	-2,94
X-	SLD/27	-2,54	X-	SLD/27	-1,98	X-	SLD/27	-2,71	X-	SLD/24	-2,96
Y+	SLD/41	-2,51	Y+	SLD/41	-1,93	Y+	SLD/41	-2,63	Y+	SLD/40	-3,01
Y-	SLD/43	-2,55	Y-	SLD/43	-2,01	Y-	SLD/43	-2,75	Y-	SLD/46	-2,84
130	SLD/1	-2,40	131	SLD/1	-1,90	132	SLD/1	-2,48	133	SLD/1	-2,38
	SLD/2	-2,37		SLD/2	-1,88		SLD/2	-2,45		SLD/2	-2,35
	SLD/3	-2,42		SLD/3	-1,91		SLD/3	-2,50		SLD/3	-2,40
	SLD/4	-2,39		SLD/4	-1,89		SLD/4	-2,47		SLD/4	-2,38
	SLD/5	-2,37		SLD/5	-1,87		SLD/5	-2,45		SLD/5	-2,35
	SLD/6	-2,37		SLD/6	-1,89		SLD/6	-2,49		SLD/6	-2,41
	SLD/7	-2,34		SLD/7	-1,87		SLD/7	-2,46		SLD/7	-2,38
	SLD/8	-2,28		SLD/8	-1,84		SLD/8	-2,44		SLD/8	-2,36
	SLD/9	-2,38		SLD/9	-1,89		SLD/9	-2,47		SLD/9	-2,36
	SLD/10	-2,35		SLD/10	-1,86		SLD/10	-2,44		SLD/10	-2,33
	SLD/11	-2,30		SLD/11	-1,83		SLD/11	-2,39		SLD/11	-2,28
	SLD/12	-2,42		SLD/12	-1,91		SLD/12	-2,48		SLD/12	-2,35
	SLD/13	-2,40		SLD/13	-1,88		SLD/13	-2,44		SLD/13	-2,33
	SLD/14	-2,38		SLD/14	-1,86		SLD/14	-2,41		SLD/14	-2,27
X+	SLD/20	-2,04	X+	SLD/20	-1,53	X+	SLD/18	-2,00	X+	SLD/18	-2,00
X-	SLD/27	-1,52	X-	SLD/27	-1,19	X-	SLD/25	-1,55	X-	SLD/25	-1,46
Y+	SLD/34	-1,53	Y+	SLD/34	-1,34	Y+	SLD/34	-1,91	Y+	SLD/34	-2,01
Y-	SLD/36	-2,04	Y-	SLD/36	-1,45	Y-	SLD/36	-1,71	Y-	SLD/36	-1,45
134	SLD/1	-2,28	135	SLD/1	-2,18	136	SLD/1	-2,43	137	SLD/1	-2,37
	SLD/2	-2,25		SLD/2	-2,15		SLD/2	-2,39		SLD/2	-2,33
	SLD/3	-2,29		SLD/3	-2,18		SLD/3	-2,43		SLD/3	-2,37
	SLD/4	-2,25		SLD/4	-2,15		SLD/4	-2,39		SLD/4	-2,33
	SLD/5	-2,21		SLD/5	-2,10		SLD/5	-2,34		SLD/5	-2,29
	SLD/6	-2,26		SLD/6	-2,15		SLD/6	-2,38		SLD/6	-2,33
	SLD/7	-2,22		SLD/7	-2,11		SLD/7	-2,35		SLD/7	-2,29
	SLD/8	-2,15		SLD/8	-2,04		SLD/8	-2,27		SLD/8	-2,23
	SLD/9	-2,28		SLD/9	-2,18		SLD/9	-2,42		SLD/9	-2,37
	SLD/10	-2,24		SLD/10	-2,14		SLD/10	-2,38		SLD/10	-2,33
	SLD/11	-2,18		SLD/11	-2,09		SLD/11	-2,33		SLD/11	-2,29
	SLD/12	-2,31		SLD/12	-2,22		SLD/12	-2,47		SLD/12	-2,41
	SLD/13	-2,28		SLD/13	-2,18		SLD/13	-2,43		SLD/13	-2,37
	SLD/14	-2,24		SLD/14	-2,15		SLD/14	-2,40		SLD/14	-2,36
X+	SLD/21	-1,69	X+	SLD/20	-1,58	X+	SLD/20	-1,78	X+	SLD/20	-1,75

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	X- SLD/30	-1,51		X- SLD/27	-1,51		X- SLD/27	-1,71		X- SLD/27	-1,71
	Y+ SLD/31	-1,27		Y+ SLD/34	-1,13		Y+ SLD/34	-1,26		Y+ SLD/34	-1,26
	Y- SLD/37	-1,82		Y- SLD/36	-1,79		Y- SLD/36	-2,03		Y- SLD/36	-2,00
138	SLD/1	-2,58	139	SLD/1	-3,25	140	SLD/1	-2,16	141	SLD/1	-2,96
	SLD/2	-2,54		SLD/2	-3,22		SLD/2	-2,13		SLD/2	-2,92
	SLD/3	-2,58		SLD/3	-3,26		SLD/3	-2,15		SLD/3	-2,95
	SLD/4	-2,54		SLD/4	-3,22		SLD/4	-2,12		SLD/4	-2,91
	SLD/5	-2,50		SLD/5	-3,16		SLD/5	-2,08		SLD/5	-2,86
	SLD/6	-2,53		SLD/6	-3,18		SLD/6	-2,15		SLD/6	-2,94
	SLD/7	-2,49		SLD/7	-3,14		SLD/7	-2,12		SLD/7	-2,89
	SLD/8	-2,41		SLD/8	-3,03		SLD/8	-2,08		SLD/8	-2,84
	SLD/9	-2,57		SLD/9	-3,25		SLD/9	-2,17		SLD/9	-2,98
	SLD/10	-2,54		SLD/10	-3,21		SLD/10	-2,14		SLD/10	-2,93
	SLD/11	-2,50		SLD/11	-3,15		SLD/11	-2,11		SLD/11	-2,91
	SLD/12	-2,62		SLD/12	-3,33		SLD/12	-2,17		SLD/12	-2,99
	SLD/13	-2,59		SLD/13	-3,29		SLD/13	-2,13		SLD/13	-2,94
	SLD/14	-2,58		SLD/14	-3,28		SLD/14	-2,11		SLD/14	-2,93
X+	SLD/20	-1,94	X+	SLD/20	-2,55	X+	SLD/20	-1,40	X+	SLD/21	-1,96
X-	SLD/27	-1,91	X-	SLD/27	-2,41	X-	SLD/27	-1,64	X-	SLD/30	-2,31
Y+	SLD/34	-1,34	Y+	SLD/34	-1,58	Y+	SLD/41	-1,45	Y+	SLD/40	-1,88
Y-	SLD/36	-2,25	Y-	SLD/36	-3,00	Y-	SLD/43	-1,61	Y-	SLD/46	-2,36
142	SLD/1	-2,71	143	SLD/1	-3,89	144	SLD/1	-3,01	145	SLD/1	-2,69
	SLD/2	-2,67		SLD/2	-3,82		SLD/2	-2,93		SLD/2	-2,61
	SLD/3	-2,69		SLD/3	-3,88		SLD/3	-3,01		SLD/3	-2,69
	SLD/4	-2,65		SLD/4	-3,80		SLD/4	-2,93		SLD/4	-2,61
	SLD/5	-2,61		SLD/5	-3,73		SLD/5	-2,88		SLD/5	-2,56
	SLD/6	-2,67		SLD/6	-3,88		SLD/6	-3,01		SLD/6	-2,70
	SLD/7	-2,63		SLD/7	-3,81		SLD/7	-2,93		SLD/7	-2,61
	SLD/8	-2,57		SLD/8	-3,73		SLD/8	-2,88		SLD/8	-2,57
	SLD/9	-2,72		SLD/9	-3,90		SLD/9	-3,02		SLD/9	-2,70
	SLD/10	-2,69		SLD/10	-3,83		SLD/10	-2,94		SLD/10	-2,61
	SLD/11	-2,67		SLD/11	-3,77		SLD/11	-2,89		SLD/11	-2,57
	SLD/12	-2,75		SLD/12	-3,90		SLD/12	-3,01		SLD/12	-2,69
	SLD/13	-2,71		SLD/13	-3,82		SLD/13	-2,93		SLD/13	-2,61
	SLD/14	-2,70		SLD/14	-3,76		SLD/14	-2,89		SLD/14	-2,56
X+	SLD/21	-1,77	X+	SLD/20	-2,49	X+	SLD/20	-1,95	X+	SLD/18	-1,72
X-	SLD/30	-2,26	X-	SLD/27	-2,77	X-	SLD/27	-2,04	X-	SLD/25	-1,80
Y+	SLD/40	-1,59	Y+	SLD/41	-2,56	Y+	SLD/41	-1,99	Y+	SLD/41	-1,80
Y-	SLD/46	-2,36	Y-	SLD/43	-2,73	Y-	SLD/43	-2,02	Y-	SLD/43	-1,72
146	SLD/1	-2,79	147	SLD/1	-3,51	148	SLD/1	-3,03	149	SLD/1	-3,00
	SLD/2	-2,71		SLD/2	-3,42		SLD/2	-2,95		SLD/2	-2,92
	SLD/3	-2,79		SLD/3	-3,50		SLD/3	-3,03		SLD/3	-3,01
	SLD/4	-2,70		SLD/4	-3,41		SLD/4	-2,95		SLD/4	-2,93
	SLD/5	-2,64		SLD/5	-3,34		SLD/5	-2,89		SLD/5	-2,86
	SLD/6	-2,80		SLD/6	-3,51		SLD/6	-3,04		SLD/6	-3,01
	SLD/7	-2,71		SLD/7	-3,42		SLD/7	-2,95		SLD/7	-2,92
	SLD/8	-2,66		SLD/8	-3,35		SLD/8	-2,89		SLD/8	-2,86
	SLD/9	-2,79		SLD/9	-3,52		SLD/9	-3,03		SLD/9	-3,00
	SLD/10	-2,71		SLD/10	-3,42		SLD/10	-2,95		SLD/10	-2,91
	SLD/11	-2,65		SLD/11	-3,36		SLD/11	-2,88		SLD/11	-2,84
	SLD/12	-2,78		SLD/12	-3,51		SLD/12	-3,03		SLD/12	-3,00
	SLD/13	-2,70		SLD/13	-3,42		SLD/13	-2,94		SLD/13	-2,91
	SLD/14	-2,63		SLD/14	-3,35		SLD/14	-2,88		SLD/14	-2,84
X+	SLD/18	-1,76	X+	SLD/18	-2,22	X+	SLD/18	-1,99	X+	SLD/15	-2,03
X-	SLD/25	-1,85	X-	SLD/25	-2,39	X-	SLD/25	-1,97	X-	SLD/24	-1,86
Y+	SLD/41	-1,86	Y+	SLD/41	-2,35	Y+	SLD/34	-2,01	Y+	SLD/31	-2,02
Y-	SLD/43	-1,73	Y-	SLD/43	-2,30	Y-	SLD/36	-1,92	Y-	SLD/37	-1,89
150	SLD/1	-3,22	151	SLD/1	-3,28	152	SLD/1	-3,72	153	SLD/1	-3,23
	SLD/2	-3,14		SLD/2	-3,20		SLD/2	-3,63		SLD/2	-3,14
	SLD/3	-3,22		SLD/3	-3,27		SLD/3	-3,71		SLD/3	-3,24
	SLD/4	-3,14		SLD/4	-3,19		SLD/4	-3,62		SLD/4	-3,15
	SLD/5	-3,08		SLD/5	-3,13		SLD/5	-3,55		SLD/5	-3,10
	SLD/6	-3,21		SLD/6	-3,27		SLD/6	-3,71		SLD/6	-3,22
	SLD/7	-3,13		SLD/7	-3,19		SLD/7	-3,62		SLD/7	-3,14
	SLD/8	-3,07		SLD/8	-3,13		SLD/8	-3,55		SLD/8	-3,07
	SLD/9	-3,21		SLD/9	-3,28		SLD/9	-3,72		SLD/9	-3,21
	SLD/10	-3,14		SLD/10	-3,20		SLD/10	-3,63		SLD/10	-3,13
	SLD/11	-3,08		SLD/11	-3,14		SLD/11	-3,57		SLD/11	-3,05
	SLD/12	-3,22		SLD/12	-3,28		SLD/12	-3,72		SLD/12	-3,23
	SLD/13	-3,14		SLD/13	-3,20		SLD/13	-3,63		SLD/13	-3,14
	SLD/14	-3,08		SLD/14	-3,14		SLD/14	-3,57		SLD/14	-3,09
X+	SLD/21	-2,13	X+	SLD/20	-2,13	X+	SLD/20	-2,39	X+	SLD/21	-2,31
X-	SLD/30	-2,11	X-	SLD/27	-2,22	X-	SLD/27	-2,54	X-	SLD/30	-1,95
Y+	SLD/31	-2,10	Y+	SLD/41	-2,14	Y+	SLD/41	-2,41	Y+	SLD/31	-2,13
Y-	SLD/37	-2,14	Y-	SLD/43	-2,21	Y-	SLD/43	-2,53	Y-	SLD/37	-2,22
154	SLD/1	-3,22	155	SLD/1	-2,61	156	SLD/1	-2,53	157	SLD/1	-3,14
	SLD/2	-3,13		SLD/2	-2,53		SLD/2	-2,46		SLD/2	-3,04

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/3	-3,23		SLD/3	-2,62		SLD/3	-2,53		SLD/3	-3,14
	SLD/4	-3,14		SLD/4	-2,54		SLD/4	-2,46		SLD/4	-3,04
	SLD/5	-3,09		SLD/5	-2,49		SLD/5	-2,40		SLD/5	-2,98
	SLD/6	-3,22		SLD/6	-2,61		SLD/6	-2,54		SLD/6	-3,15
	SLD/7	-3,13		SLD/7	-2,54		SLD/7	-2,46		SLD/7	-3,05
	SLD/8	-3,07		SLD/8	-2,49		SLD/8	-2,41		SLD/8	-2,98
	SLD/9	-3,21		SLD/9	-2,60		SLD/9	-2,53		SLD/9	-3,14
	SLD/10	-3,11		SLD/10	-2,53		SLD/10	-2,45		SLD/10	-3,04
	SLD/11	-3,05		SLD/11	-2,47		SLD/11	-2,39		SLD/11	-2,96
	SLD/12	-3,22		SLD/12	-2,61		SLD/12	-2,52		SLD/12	-3,13
	SLD/13	-3,13		SLD/13	-2,53		SLD/13	-2,45		SLD/13	-3,03
	SLD/14	-3,07		SLD/14	-2,48		SLD/14	-2,39		SLD/14	-2,95
X+	SLD/21	-2,28	X+	SLD/15	-1,77	X+	SLD/15	-1,65	X+	SLD/15	-2,07
X-	SLD/30	-1,94	X-	SLD/24	-1,63	X-	SLD/24	-1,61	X-	SLD/24	-1,96
Y+	SLD/31	-2,15	Y+	SLD/31	-1,74	Y+	SLD/31	-1,67	Y+	SLD/31	-2,08
Y-	SLD/37	-2,17	Y-	SLD/37	-1,68	Y-	SLD/37	-1,57	Y-	SLD/37	-1,94
158	SLD/1	-2,59	159	SLD/1	-2,91	160	SLD/1	-4,26	161	SLD/1	-3,81
	SLD/2	-2,51		SLD/2	-2,82		SLD/2	-4,18		SLD/2	-3,73
	SLD/3	-2,60		SLD/3	-2,91		SLD/3	-4,26		SLD/3	-3,80
	SLD/4	-2,51		SLD/4	-2,82		SLD/4	-4,18		SLD/4	-3,72
	SLD/5	-2,46		SLD/5	-2,78		SLD/5	-4,11		SLD/5	-3,65
	SLD/6	-2,60		SLD/6	-2,91		SLD/6	-4,27		SLD/6	-3,82
	SLD/7	-2,51		SLD/7	-2,83		SLD/7	-4,19		SLD/7	-3,75
	SLD/8	-2,47		SLD/8	-2,79		SLD/8	-4,12		SLD/8	-3,70
	SLD/9	-2,59		SLD/9	-2,91		SLD/9	-4,25		SLD/9	-3,81
	SLD/10	-2,51		SLD/10	-2,82		SLD/10	-4,17		SLD/10	-3,74
	SLD/11	-2,46		SLD/11	-2,78		SLD/11	-4,09		SLD/11	-3,68
	SLD/12	-2,59		SLD/12	-2,90		SLD/12	-4,25		SLD/12	-3,79
	SLD/13	-2,50		SLD/13	-2,81		SLD/13	-4,17		SLD/13	-3,71
	SLD/14	-2,45		SLD/14	-2,77		SLD/14	-4,08		SLD/14	-3,64
X+	SLD/15	-1,71	X+	SLD/15	-1,94	X+	SLD/15	-2,95	X+	SLD/18	-2,54
X-	SLD/24	-1,68	X-	SLD/24	-1,94	X-	SLD/24	-2,84	X-	SLD/25	-2,73
Y+	SLD/31	-1,73	Y+	SLD/40	-1,99	Y+	SLD/31	-3,00	Y+	SLD/41	-2,79
Y-	SLD/37	-1,63	Y-	SLD/46	-1,86	Y-	SLD/37	-2,76	Y-	SLD/43	-2,43
162	SLD/1	-2,51	163	SLD/1	-1,61	164	SLD/1	-1,39	165	SLD/1	-1,57
	SLD/2	-2,45		SLD/2	-1,56		SLD/2	-1,35		SLD/2	-1,53
	SLD/3	-2,51		SLD/3	-1,60		SLD/3	-1,39		SLD/3	-1,57
	SLD/4	-2,44		SLD/4	-1,55		SLD/4	-1,35		SLD/4	-1,53
	SLD/5	-2,41		SLD/5	-1,52		SLD/5	-1,31		SLD/5	-1,50
	SLD/6	-2,52		SLD/6	-1,61		SLD/6	-1,39		SLD/6	-1,57
	SLD/7	-2,45		SLD/7	-1,56		SLD/7	-1,35		SLD/7	-1,53
	SLD/8	-2,42		SLD/8	-1,53		SLD/8	-1,32		SLD/8	-1,50
	SLD/9	-2,52		SLD/9	-1,61		SLD/9	-1,40		SLD/9	-1,58
	SLD/10	-2,45		SLD/10	-1,56		SLD/10	-1,35		SLD/10	-1,54
	SLD/11	-2,42		SLD/11	-1,53		SLD/11	-1,33		SLD/11	-1,51
	SLD/12	-2,51		SLD/12	-1,60		SLD/12	-1,39		SLD/12	-1,57
	SLD/13	-2,44		SLD/13	-1,55		SLD/13	-1,35		SLD/13	-1,53
	SLD/14	-2,40		SLD/14	-1,52		SLD/14	-1,31		SLD/14	-1,50
X+	SLD/18	-1,67	X+	SLD/18	-1,02	X+	SLD/18	-0,86	X+	SLD/18	-0,98
X-	SLD/25	-1,75	X-	SLD/25	-1,10	X-	SLD/25	-0,95	X-	SLD/25	-1,07
Y+	SLD/41	-1,78	Y+	SLD/41	-1,10	Y+	SLD/41	-0,93	Y+	SLD/41	-1,05
Y-	SLD/43	-1,61	Y-	SLD/43	-1,03	Y-	SLD/43	-0,88	Y-	SLD/43	-1,04
166	SLD/1	-1,57	167	SLD/1	-1,68	168	SLD/1	-1,78	169	SLD/1	-1,79
	SLD/2	-1,53		SLD/2	-1,63		SLD/2	-1,74		SLD/2	-1,74
	SLD/3	-1,57		SLD/3	-1,68		SLD/3	-1,78		SLD/3	-1,78
	SLD/4	-1,53		SLD/4	-1,63		SLD/4	-1,74		SLD/4	-1,74
	SLD/5	-1,49		SLD/5	-1,59		SLD/5	-1,70		SLD/5	-1,71
	SLD/6	-1,57		SLD/6	-1,68		SLD/6	-1,78		SLD/6	-1,79
	SLD/7	-1,53		SLD/7	-1,63		SLD/7	-1,74		SLD/7	-1,74
	SLD/8	-1,50		SLD/8	-1,59		SLD/8	-1,70		SLD/8	-1,71
	SLD/9	-1,57		SLD/9	-1,67		SLD/9	-1,78		SLD/9	-1,79
	SLD/10	-1,53		SLD/10	-1,63		SLD/10	-1,74		SLD/10	-1,74
	SLD/11	-1,50		SLD/11	-1,59		SLD/11	-1,70		SLD/11	-1,71
	SLD/12	-1,57		SLD/12	-1,67		SLD/12	-1,78		SLD/12	-1,78
	SLD/13	-1,53		SLD/13	-1,63		SLD/13	-1,74		SLD/13	-1,74
	SLD/14	-1,49		SLD/14	-1,58		SLD/14	-1,70		SLD/14	-1,71
X+	SLD/18	-1,01	X+	SLD/18	-1,09	X+	SLD/15	-1,18	X+	SLD/18	-1,16
X-	SLD/25	-1,04	X-	SLD/25	-1,06	X-	SLD/24	-1,17	X-	SLD/25	-1,20
Y+	SLD/41	-1,03	Y+	SLD/34	-1,10	Y+	SLD/31	-1,18	Y+	SLD/41	-1,20
Y-	SLD/43	-1,01	Y-	SLD/36	-1,05	Y-	SLD/37	-1,17	Y-	SLD/43	-1,17
170	SLD/1	-1,65	171	SLD/1	-1,59	172	SLD/1	-1,48	173	SLD/1	-1,53
	SLD/2	-1,61		SLD/2	-1,55		SLD/2	-1,44		SLD/2	-1,49
	SLD/3	-1,64		SLD/3	-1,60		SLD/3	-1,48		SLD/3	-1,53
	SLD/4	-1,61		SLD/4	-1,56		SLD/4	-1,44		SLD/4	-1,49
	SLD/5	-1,57		SLD/5	-1,53		SLD/5	-1,42		SLD/5	-1,46
	SLD/6	-1,65		SLD/6	-1,60		SLD/6	-1,48		SLD/6	-1,53
	SLD/7	-1,61		SLD/7	-1,55		SLD/7	-1,44		SLD/7	-1,49
	SLD/8	-1,58		SLD/8	-1,53		SLD/8	-1,42		SLD/8	-1,47

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD

Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/9	-1,65		SLD/9	-1,59		SLD/9	-1,47		SLD/9	-1,53
	SLD/10	-1,61		SLD/10	-1,54		SLD/10	-1,43		SLD/10	-1,49
	SLD/11	-1,58		SLD/11	-1,51		SLD/11	-1,40		SLD/11	-1,46
	SLD/12	-1,64		SLD/12	-1,59		SLD/12	-1,47		SLD/12	-1,52
	SLD/13	-1,61		SLD/13	-1,55		SLD/13	-1,43		SLD/13	-1,48
	SLD/14	-1,57		SLD/14	-1,52		SLD/14	-1,40		SLD/14	-1,45
X+	SLD/18	-1,06	X+	SLD/15	-1,14	X+	SLD/15	-1,04	X+	SLD/15	-1,03
X-	SLD/25	-1,12	X-	SLD/24	-0,97	X-	SLD/24	-0,93	X-	SLD/24	-1,02
Y+	SLD/41	-1,12	Y+	SLD/31	-1,11	Y+	SLD/31	-1,03	Y+	SLD/31	-1,07
Y-	SLD/43	-1,07	Y-	SLD/37	-1,03	Y-	SLD/37	-0,95	Y-	SLD/37	-0,96
174	SLD/1	-1,66	175	SLD/1	-1,51	176	SLD/1	-1,57	177	SLD/1	-1,71
	SLD/2	-1,63		SLD/2	-1,48		SLD/2	-1,54		SLD/2	-1,69
	SLD/3	-1,66		SLD/3	-1,51		SLD/3	-1,57		SLD/3	-1,71
	SLD/4	-1,62		SLD/4	-1,49		SLD/4	-1,54		SLD/4	-1,69
	SLD/5	-1,59		SLD/5	-1,46		SLD/5	-1,52		SLD/5	-1,67
	SLD/6	-1,67		SLD/6	-1,52		SLD/6	-1,58		SLD/6	-1,73
	SLD/7	-1,63		SLD/7	-1,49		SLD/7	-1,55		SLD/7	-1,71
	SLD/8	-1,61		SLD/8	-1,47		SLD/8	-1,54		SLD/8	-1,70
	SLD/9	-1,67		SLD/9	-1,51		SLD/9	-1,56		SLD/9	-1,71
	SLD/10	-1,63		SLD/10	-1,48		SLD/10	-1,54		SLD/10	-1,68
	SLD/11	-1,60		SLD/11	-1,45		SLD/11	-1,51		SLD/11	-1,65
	SLD/12	-1,66		SLD/12	-1,50		SLD/12	-1,55		SLD/12	-1,69
	SLD/13	-1,62		SLD/13	-1,48		SLD/13	-1,53		SLD/13	-1,66
	SLD/14	-1,59		SLD/14	-1,44		SLD/14	-1,50		SLD/14	-1,63
X+	SLD/15	-1,10	X+	SLD/15	-1,08	X+	SLD/15	-1,14	X+	SLD/15	-1,30
X-	SLD/24	-1,15	X-	SLD/24	-1,01	X-	SLD/24	-1,07	X-	SLD/24	-1,20
Y+	SLD/40	-1,18	Y+	SLD/31	-1,11	Y+	SLD/31	-1,20	Y+	SLD/31	-1,40
Y-	SLD/46	-1,05	Y-	SLD/37	-0,96	Y-	SLD/37	-0,98	Y-	SLD/37	-1,02
178	SLD/1	-2,26	179	SLD/1	-3,33	180	SLD/1	-3,61	181	SLD/1	-2,57
	SLD/2	-2,23		SLD/2	-3,29		SLD/2	-3,56		SLD/2	-2,52
	SLD/3	-2,27		SLD/3	-3,31		SLD/3	-3,61		SLD/3	-2,56
	SLD/4	-2,24		SLD/4	-3,27		SLD/4	-3,55		SLD/4	-2,52
	SLD/5	-2,22		SLD/5	-3,21		SLD/5	-3,49		SLD/5	-2,47
	SLD/6	-2,30		SLD/6	-3,35		SLD/6	-3,62		SLD/6	-2,56
	SLD/7	-2,27		SLD/7	-3,31		SLD/7	-3,57		SLD/7	-2,52
	SLD/8	-2,26		SLD/8	-3,27		SLD/8	-3,52		SLD/8	-2,47
	SLD/9	-2,24		SLD/9	-3,35		SLD/9	-3,62		SLD/9	-2,57
	SLD/10	-2,22		SLD/10	-3,30		SLD/10	-3,57		SLD/10	-2,52
	SLD/11	-2,18		SLD/11	-3,26		SLD/11	-3,52		SLD/11	-2,48
	SLD/12	-2,22		SLD/12	-3,30		SLD/12	-3,60		SLD/12	-2,57
	SLD/13	-2,19		SLD/13	-3,26		SLD/13	-3,55		SLD/13	-2,52
	SLD/14	-2,13		SLD/14	-3,19		SLD/14	-3,49		SLD/14	-2,48
X+	SLD/15	-1,85	X+	SLD/18	-2,17	X+	SLD/18	-2,42	X+	SLD/21	-1,70
X-	SLD/24	-1,56	X-	SLD/25	-2,57	X-	SLD/25	-2,59	X-	SLD/30	-1,77
Y+	SLD/31	-2,01	Y+	SLD/41	-2,61	Y+	SLD/41	-2,61	Y+	SLD/40	-1,71
Y-	SLD/37	-1,27	Y-	SLD/43	-2,11	Y-	SLD/43	-2,40	Y-	SLD/46	-1,76
182	SLD/1	-3,61	183	SLD/1	-3,11	184	SLD/1	-3,02	185	SLD/1	-2,86
	SLD/2	-3,52		SLD/2	-3,03		SLD/2	-2,93		SLD/2	-2,78
	SLD/3	-3,62		SLD/3	-3,12		SLD/3	-3,02		SLD/3	-2,86
	SLD/4	-3,53		SLD/4	-3,03		SLD/4	-2,93		SLD/4	-2,77
	SLD/5	-3,47		SLD/5	-2,98		SLD/5	-2,86		SLD/5	-2,70
	SLD/6	-3,59		SLD/6	-3,11		SLD/6	-3,02		SLD/6	-2,86
	SLD/7	-3,51		SLD/7	-3,02		SLD/7	-2,93		SLD/7	-2,78
	SLD/8	-3,43		SLD/8	-2,96		SLD/8	-2,86		SLD/8	-2,71
	SLD/9	-3,59		SLD/9	-3,11		SLD/9	-3,02		SLD/9	-2,87
	SLD/10	-3,51		SLD/10	-3,02		SLD/10	-2,93		SLD/10	-2,78
	SLD/11	-3,43		SLD/11	-2,95		SLD/11	-2,86		SLD/11	-2,71
	SLD/12	-3,62		SLD/12	-3,12		SLD/12	-3,02		SLD/12	-2,86
	SLD/13	-3,53		SLD/13	-3,03		SLD/13	-2,93		SLD/13	-2,78
	SLD/14	-3,47		SLD/14	-2,98		SLD/14	-2,87		SLD/14	-2,70
X+	SLD/20	-2,54	X+	SLD/20	-2,13	X+	SLD/21	-1,95	X+	SLD/15	-1,78
X-	SLD/27	-2,25	X-	SLD/27	-1,95	X-	SLD/30	-1,92	X-	SLD/24	-1,86
Y+	SLD/34	-2,31	Y+	SLD/34	-1,99	Y+	SLD/31	-1,92	Y+	SLD/40	-1,84
Y-	SLD/36	-2,51	Y-	SLD/36	-2,11	Y-	SLD/37	-1,95	Y-	SLD/46	-1,81
186	SLD/1	-3,01	187	SLD/1	-3,14	188	SLD/1	-2,86	189	SLD/1	-2,69
	SLD/2	-2,92		SLD/2	-3,05		SLD/2	-2,78		SLD/2	-2,61
	SLD/3	-3,00		SLD/3	-3,13		SLD/3	-2,87		SLD/3	-2,70
	SLD/4	-2,91		SLD/4	-3,04		SLD/4	-2,78		SLD/4	-2,61
	SLD/5	-2,83		SLD/5	-2,95		SLD/5	-2,72		SLD/5	-2,57
	SLD/6	-3,01		SLD/6	-3,14		SLD/6	-2,86		SLD/6	-2,69
	SLD/7	-2,93		SLD/7	-3,05		SLD/7	-2,78		SLD/7	-2,61
	SLD/8	-2,85		SLD/8	-2,97		SLD/8	-2,71		SLD/8	-2,56
	SLD/9	-3,02		SLD/9	-3,15		SLD/9	-2,86		SLD/9	-2,69
	SLD/10	-2,93		SLD/10	-3,06		SLD/10	-2,77		SLD/10	-2,60
	SLD/11	-2,86		SLD/11	-2,99		SLD/11	-2,70		SLD/11	-2,55
	SLD/12	-3,01		SLD/12	-3,14		SLD/12	-2,86		SLD/12	-2,69
	SLD/13	-2,92		SLD/13	-3,05		SLD/13	-2,78		SLD/13	-2,61
	SLD/14	-2,85		SLD/14	-2,97		SLD/14	-2,71		SLD/14	-2,56

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	X+ SLD/15	-1,80		X+ SLD/21	-1,83		X+ SLD/20	-1,92		X+ SLD/20	-1,80
	X- SLD/24	-2,02		X- SLD/30	-2,13		X- SLD/27	-1,73		X- SLD/27	-1,70
	Y+ SLD/40	-1,95		Y+ SLD/40	-2,03		Y+ SLD/34	-1,85		Y+ SLD/34	-1,75
	Y- SLD/46	-1,93		Y- SLD/46	-2,03		Y- SLD/36	-1,86		Y- SLD/36	-1,77
190	SLD/1	-2,92	191	SLD/1	-3,47	192	SLD/1	-4,50	193	SLD/1	-3,51
	SLD/2	-2,83		SLD/2	-3,39		SLD/2	-4,43		SLD/2	-3,44
	SLD/3	-2,91		SLD/3	-3,46		SLD/3	-4,47		SLD/3	-3,49
	SLD/4	-2,83		SLD/4	-3,39		SLD/4	-4,39		SLD/4	-3,43
	SLD/5	-2,78		SLD/5	-3,31		SLD/5	-4,31		SLD/5	-3,38
	SLD/6	-2,91		SLD/6	-3,47		SLD/6	-4,45		SLD/6	-3,48
	SLD/7	-2,83		SLD/7	-3,39		SLD/7	-4,37		SLD/7	-3,41
	SLD/8	-2,78		SLD/8	-3,32		SLD/8	-4,28		SLD/8	-3,36
	SLD/9	-2,92		SLD/9	-3,48		SLD/9	-4,53		SLD/9	-3,52
	SLD/10	-2,84		SLD/10	-3,40		SLD/10	-4,46		SLD/10	-3,46
	SLD/11	-2,79		SLD/11	-3,34		SLD/11	-4,43		SLD/11	-3,43
	SLD/12	-2,92		SLD/12	-3,48		SLD/12	-4,55		SLD/12	-3,54
	SLD/13	-2,84		SLD/13	-3,40		SLD/13	-4,48		SLD/13	-3,47
	SLD/14	-2,79		SLD/14	-3,34		SLD/14	-4,46		SLD/14	-3,45
	X+ SLD/21	-1,88		X+ SLD/21	-2,22		X+ SLD/21	-2,84		X+ SLD/21	-2,31
	X- SLD/30	-1,97		X- SLD/30	-2,40		X- SLD/30	-3,70		X- SLD/30	-2,69
	Y+ SLD/40	-1,90		Y+ SLD/40	-2,26		Y+ SLD/40	-2,72		Y+ SLD/40	-2,20
	Y- SLD/46	-1,96		Y- SLD/46	-2,38		Y- SLD/46	-3,77		Y- SLD/46	-2,76
194	SLD/1	-3,24	195	SLD/1	-3,63	196	SLD/1	-3,50	197	SLD/1	-3,17
	SLD/2	-3,16		SLD/2	-3,55		SLD/2	-3,42		SLD/2	-3,10
	SLD/3	-3,23		SLD/3	-3,61		SLD/3	-3,49		SLD/3	-3,16
	SLD/4	-3,15		SLD/4	-3,53		SLD/4	-3,42		SLD/4	-3,10
	SLD/5	-3,10		SLD/5	-3,47		SLD/5	-3,37		SLD/5	-3,05
	SLD/6	-3,22		SLD/6	-3,60		SLD/6	-3,50		SLD/6	-3,16
	SLD/7	-3,14		SLD/7	-3,53		SLD/7	-3,42		SLD/7	-3,09
	SLD/8	-3,10		SLD/8	-3,46		SLD/8	-3,37		SLD/8	-3,05
	SLD/9	-3,25		SLD/9	-3,64		SLD/9	-3,50		SLD/9	-3,18
	SLD/10	-3,17		SLD/10	-3,57		SLD/10	-3,42		SLD/10	-3,11
	SLD/11	-3,13		SLD/11	-3,53		SLD/11	-3,38		SLD/11	-3,08
	SLD/12	-3,25		SLD/12	-3,65		SLD/12	-3,50		SLD/12	-3,18
	SLD/13	-3,17		SLD/13	-3,58		SLD/13	-3,42		SLD/13	-3,12
	SLD/14	-3,14		SLD/14	-3,55		SLD/14	-3,38		SLD/14	-3,09
	X+ SLD/21	-2,09		X+ SLD/21	-2,31		X+ SLD/20	-2,33		X+ SLD/20	-2,08
	X- SLD/30	-2,35		X- SLD/30	-2,77		X- SLD/27	-2,42		X- SLD/27	-2,31
	Y+ SLD/40	-2,10		Y+ SLD/40	-2,29		Y+ SLD/41	-2,38		Y+ SLD/41	-2,09
	Y- SLD/46	-2,35		Y- SLD/46	-2,78		Y- SLD/43	-2,39		Y- SLD/43	-2,31
198	SLD/1	-2,94	199	SLD/1	-2,91	200	SLD/1	-2,51	201	SLD/1	-2,88
	SLD/2	-2,86		SLD/2	-2,83		SLD/2	-2,43		SLD/2	-2,81
	SLD/3	-2,94		SLD/3	-2,91		SLD/3	-2,51		SLD/3	-2,88
	SLD/4	-2,86		SLD/4	-2,83		SLD/4	-2,43		SLD/4	-2,80
	SLD/5	-2,82		SLD/5	-2,79		SLD/5	-2,39		SLD/5	-2,76
	SLD/6	-2,94		SLD/6	-2,92		SLD/6	-2,51		SLD/6	-2,88
	SLD/7	-2,86		SLD/7	-2,84		SLD/7	-2,43		SLD/7	-2,80
	SLD/8	-2,82		SLD/8	-2,80		SLD/8	-2,40		SLD/8	-2,76
	SLD/9	-2,95		SLD/9	-2,91		SLD/9	-2,51		SLD/9	-2,89
	SLD/10	-2,87		SLD/10	-2,83		SLD/10	-2,43		SLD/10	-2,81
	SLD/11	-2,83		SLD/11	-2,78		SLD/11	-2,39		SLD/11	-2,77
	SLD/12	-2,94		SLD/12	-2,90		SLD/12	-2,50		SLD/12	-2,89
	SLD/13	-2,86		SLD/13	-2,82		SLD/13	-2,43		SLD/13	-2,81
	SLD/14	-2,83		SLD/14	-2,77		SLD/14	-2,39		SLD/14	-2,77
	X+ SLD/21	-1,93		X+ SLD/18	-1,98		X+ SLD/18	-1,63		X+ SLD/21	-1,86
	X- SLD/30	-2,01		X- SLD/25	-1,91		X- SLD/25	-1,68		X- SLD/30	-2,00
	Y+ SLD/40	-1,96		Y+ SLD/34	-2,00		Y+ SLD/41	-1,68		Y+ SLD/40	-1,90
	Y- SLD/46	-1,99		Y- SLD/36	-1,87		Y- SLD/43	-1,62		Y- SLD/46	-1,98
202	SLD/1	-3,37	203	SLD/1	-2,57	204	SLD/1	-4,10	205	SLD/1	-4,58
	SLD/2	-3,30		SLD/2	-2,49		SLD/2	-4,02		SLD/2	-4,50
	SLD/3	-3,36		SLD/3	-2,57		SLD/3	-4,10		SLD/3	-4,57
	SLD/4	-3,29		SLD/4	-2,49		SLD/4	-4,02		SLD/4	-4,49
	SLD/5	-3,23		SLD/5	-2,44		SLD/5	-3,96		SLD/5	-4,41
	SLD/6	-3,36		SLD/6	-2,57		SLD/6	-4,07		SLD/6	-4,53
	SLD/7	-3,29		SLD/7	-2,50		SLD/7	-3,99		SLD/7	-4,46
	SLD/8	-3,23		SLD/8	-2,45		SLD/8	-3,91		SLD/8	-4,35
	SLD/9	-3,38		SLD/9	-2,57		SLD/9	-4,10		SLD/9	-4,59
	SLD/10	-3,31		SLD/10	-2,49		SLD/10	-4,03		SLD/10	-4,52
	SLD/11	-3,27		SLD/11	-2,44		SLD/11	-3,96		SLD/11	-4,45
	SLD/12	-3,38		SLD/12	-2,56		SLD/12	-4,13		SLD/12	-4,63
	SLD/13	-3,31		SLD/13	-2,48		SLD/13	-4,05		SLD/13	-4,55
	SLD/14	-3,27		SLD/14	-2,43		SLD/14	-4,01		SLD/14	-4,51
	X+ SLD/21	-2,15		X+ SLD/18	-1,69		X+ SLD/21	-2,84		X+ SLD/21	-3,09
	X- SLD/30	-2,45		X- SLD/25	-1,67		X- SLD/30	-2,91		X- SLD/30	-3,39
	Y+ SLD/40	-2,19		Y+ SLD/34	-1,72		Y+ SLD/40	-2,49		Y+ SLD/40	-2,71
	Y- SLD/46	-2,42		Y- SLD/36	-1,60		Y- SLD/46	-3,10		Y- SLD/46	-3,60
206	SLD/1	-3,65	207	SLD/1	-3,17	208	SLD/1	-3,03	209	SLD/1	-2,73

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/2	-3,58		SLD/2	-3,09		SLD/2	-2,95		SLD/2	-2,65
	SLD/3	-3,66		SLD/3	-3,18		SLD/3	-3,04		SLD/3	-2,74
	SLD/4	-3,58		SLD/4	-3,10		SLD/4	-2,96		SLD/4	-2,66
	SLD/5	-3,53		SLD/5	-3,06		SLD/5	-2,92		SLD/5	-2,63
	SLD/6	-3,64		SLD/6	-3,17		SLD/6	-3,04		SLD/6	-2,74
	SLD/7	-3,57		SLD/7	-3,09		SLD/7	-2,96		SLD/7	-2,66
	SLD/8	-3,51		SLD/8	-3,04		SLD/8	-2,92		SLD/8	-2,63
	SLD/9	-3,65		SLD/9	-3,17		SLD/9	-3,02		SLD/9	-2,73
	SLD/10	-3,57		SLD/10	-3,09		SLD/10	-2,94		SLD/10	-2,65
	SLD/11	-3,52		SLD/11	-3,05		SLD/11	-2,90		SLD/11	-2,61
	SLD/12	-3,66		SLD/12	-3,18		SLD/12	-3,02		SLD/12	-2,73
	SLD/13	-3,59		SLD/13	-3,10		SLD/13	-2,94		SLD/13	-2,65
	SLD/14	-3,54		SLD/14	-3,06		SLD/14	-2,89		SLD/14	-2,61
X+	SLD/21	-2,52	X+	SLD/21	-2,19	X+	SLD/15	-2,14	X+	SLD/15	-1,91
X-	SLD/30	-2,47	X-	SLD/30	-2,12	X-	SLD/24	-1,95	X-	SLD/24	-1,76
Y+	SLD/31	-2,39	Y+	SLD/31	-2,09	Y+	SLD/31	-2,13	Y+	SLD/31	-1,89
Y-	SLD/37	-2,57	Y-	SLD/37	-2,21	Y-	SLD/37	-1,97	Y-	SLD/37	-1,79
210	SLD/1	-3,00	211	SLD/1	-2,53	212	SLD/1	-2,74	213	SLD/1	-2,61
	SLD/2	-2,92		SLD/2	-2,45		SLD/2	-2,66		SLD/2	-2,53
	SLD/3	-3,00		SLD/3	-2,53		SLD/3	-2,75		SLD/3	-2,61
	SLD/4	-2,92		SLD/4	-2,45		SLD/4	-2,67		SLD/4	-2,53
	SLD/5	-2,88		SLD/5	-2,42		SLD/5	-2,63		SLD/5	-2,50
	SLD/6	-2,99		SLD/6	-2,53		SLD/6	-2,75		SLD/6	-2,62
	SLD/7	-2,91		SLD/7	-2,45		SLD/7	-2,67		SLD/7	-2,53
	SLD/8	-2,87		SLD/8	-2,42		SLD/8	-2,64		SLD/8	-2,50
	SLD/9	-2,99		SLD/9	-2,53		SLD/9	-2,73		SLD/9	-2,60
	SLD/10	-2,91		SLD/10	-2,44		SLD/10	-2,65		SLD/10	-2,52
	SLD/11	-2,87		SLD/11	-2,41		SLD/11	-2,61		SLD/11	-2,48
	SLD/12	-3,00		SLD/12	-2,53		SLD/12	-2,73		SLD/12	-2,60
	SLD/13	-2,92		SLD/13	-2,44		SLD/13	-2,65		SLD/13	-2,52
	SLD/14	-2,88		SLD/14	-2,41		SLD/14	-2,60		SLD/14	-2,48
X+	SLD/21	-2,04	X+	SLD/15	-1,72	X+	SLD/15	-1,93	X+	SLD/15	-1,80
X-	SLD/30	-1,99	X-	SLD/24	-1,66	X-	SLD/24	-1,74	X-	SLD/24	-1,67
Y+	SLD/31	-1,98	Y+	SLD/31	-1,72	Y+	SLD/31	-1,94	Y+	SLD/31	-1,81
Y-	SLD/37	-2,05	Y-	SLD/37	-1,66	Y-	SLD/37	-1,72	Y-	SLD/37	-1,66
214	SLD/1	-2,60	215	SLD/1	-2,52	216	SLD/1	-2,50	217	SLD/1	-2,54
	SLD/2	-2,52		SLD/2	-2,45		SLD/2	-2,41		SLD/2	-2,46
	SLD/3	-2,61		SLD/3	-2,53		SLD/3	-2,50		SLD/3	-2,54
	SLD/4	-2,53		SLD/4	-2,45		SLD/4	-2,42		SLD/4	-2,46
	SLD/5	-2,48		SLD/5	-2,41		SLD/5	-2,38		SLD/5	-2,42
	SLD/6	-2,61		SLD/6	-2,53		SLD/6	-2,50		SLD/6	-2,54
	SLD/7	-2,53		SLD/7	-2,45		SLD/7	-2,42		SLD/7	-2,47
	SLD/8	-2,48		SLD/8	-2,41		SLD/8	-2,39		SLD/8	-2,43
	SLD/9	-2,59		SLD/9	-2,52		SLD/9	-2,49		SLD/9	-2,54
	SLD/10	-2,52		SLD/10	-2,44		SLD/10	-2,41		SLD/10	-2,47
	SLD/11	-2,46		SLD/11	-2,40		SLD/11	-2,38		SLD/11	-2,42
	SLD/12	-2,59		SLD/12	-2,52		SLD/12	-2,49		SLD/12	-2,54
	SLD/13	-2,52		SLD/13	-2,44		SLD/13	-2,41		SLD/13	-2,46
	SLD/14	-2,46		SLD/14	-2,39		SLD/14	-2,37		SLD/14	-2,42
X+	SLD/15	-1,78	X+	SLD/15	-1,70	X+	SLD/18	-1,67	X+	SLD/18	-1,65
X-	SLD/24	-1,62	X-	SLD/24	-1,61	X-	SLD/25	-1,63	X-	SLD/25	-1,68
Y+	SLD/31	-1,78	Y+	SLD/31	-1,71	Y+	SLD/34	-1,68	Y+	SLD/41	-1,69
Y-	SLD/37	-1,63	Y-	SLD/37	-1,59	Y-	SLD/36	-1,61	Y-	SLD/43	-1,64
218	SLD/1	-3,16	219	SLD/1	-2,84	220	SLD/1	-2,60	221	SLD/1	-2,85
	SLD/2	-3,07		SLD/2	-2,75		SLD/2	-2,51		SLD/2	-2,76
	SLD/3	-3,15		SLD/3	-2,84		SLD/3	-2,59		SLD/3	-2,84
	SLD/4	-3,07		SLD/4	-2,75		SLD/4	-2,51		SLD/4	-2,76
	SLD/5	-3,01		SLD/5	-2,70		SLD/5	-2,47		SLD/5	-2,71
	SLD/6	-3,16		SLD/6	-2,85		SLD/6	-2,60		SLD/6	-2,85
	SLD/7	-3,07		SLD/7	-2,76		SLD/7	-2,52		SLD/7	-2,77
	SLD/8	-3,02		SLD/8	-2,71		SLD/8	-2,48		SLD/8	-2,73
	SLD/9	-3,16		SLD/9	-2,85		SLD/9	-2,60		SLD/9	-2,85
	SLD/10	-3,08		SLD/10	-2,76		SLD/10	-2,52		SLD/10	-2,77
	SLD/11	-3,03		SLD/11	-2,71		SLD/11	-2,48		SLD/11	-2,73
	SLD/12	-3,16		SLD/12	-2,84		SLD/12	-2,59		SLD/12	-2,84
	SLD/13	-3,07		SLD/13	-2,75		SLD/13	-2,51		SLD/13	-2,76
	SLD/14	-3,02		SLD/14	-2,70		SLD/14	-2,47		SLD/14	-2,72
X+	SLD/18	-2,03	X+	SLD/18	-1,81	X+	SLD/18	-1,66	X+	SLD/18	-1,84
X-	SLD/25	-2,15	X-	SLD/25	-1,90	X-	SLD/25	-1,75	X-	SLD/25	-1,95
Y+	SLD/41	-2,11	Y+	SLD/41	-1,89	Y+	SLD/41	-1,74	Y+	SLD/41	-1,94
Y-	SLD/43	-2,10	Y-	SLD/43	-1,82	Y-	SLD/43	-1,67	Y-	SLD/43	-1,86
222	SLD/1	-3,56	223	SLD/1	-3,37	224	SLD/1	-3,26	225	SLD/1	-2,47
	SLD/2	-3,48		SLD/2	-3,29		SLD/2	-3,19		SLD/2	-2,40
	SLD/3	-3,55		SLD/3	-3,37		SLD/3	-3,25		SLD/3	-2,47
	SLD/4	-3,47		SLD/4	-3,29		SLD/4	-3,18		SLD/4	-2,40
	SLD/5	-3,41		SLD/5	-3,23		SLD/5	-3,13		SLD/5	-2,36
	SLD/6	-3,56		SLD/6	-3,38		SLD/6	-3,27		SLD/6	-2,48
	SLD/7	-3,48		SLD/7	-3,30		SLD/7	-3,20		SLD/7	-2,41

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/8	-3,42		SLD/8	-3,25		SLD/8	-3,16		SLD/8	-2,38
	SLD/9	-3,57		SLD/9	-3,38		SLD/9	-3,27		SLD/9	-2,48
	SLD/10	-3,49		SLD/10	-3,30		SLD/10	-3,20		SLD/10	-2,41
	SLD/11	-3,44		SLD/11	-3,25		SLD/11	-3,15		SLD/11	-2,37
	SLD/12	-3,56		SLD/12	-3,37		SLD/12	-3,25		SLD/12	-2,47
	SLD/13	-3,48		SLD/13	-3,29		SLD/13	-3,18		SLD/13	-2,40
	SLD/14	-3,43		SLD/14	-3,24		SLD/14	-3,12		SLD/14	-2,36
X+	SLD/20	-2,28	X+	SLD/18	-2,18	X+	SLD/18	-2,14	X+	SLD/18	-1,63
X-	SLD/27	-2,49	X-	SLD/25	-2,36	X-	SLD/25	-2,32	X-	SLD/25	-1,71
Y+	SLD/41	-2,39	Y+	SLD/41	-2,33	Y+	SLD/41	-2,34	Y+	SLD/41	-1,73
Y-	SLD/43	-2,43	Y-	SLD/43	-2,25	Y-	SLD/43	-2,12	Y-	SLD/43	-1,60
226	SLD/1	-2,19	227	SLD/1	-2,68	228	SLD/1	-2,38	229	SLD/1	-2,88
	SLD/2	-2,12		SLD/2	-2,60		SLD/2	-2,30		SLD/2	-2,79
	SLD/3	-2,19		SLD/3	-2,68		SLD/3	-2,37		SLD/3	-2,88
	SLD/4	-2,12		SLD/4	-2,59		SLD/4	-2,30		SLD/4	-2,78
	SLD/5	-2,08		SLD/5	-2,54		SLD/5	-2,25		SLD/5	-2,72
	SLD/6	-2,20		SLD/6	-2,69		SLD/6	-2,38		SLD/6	-2,88
	SLD/7	-2,13		SLD/7	-2,60		SLD/7	-2,31		SLD/7	-2,79
	SLD/8	-2,10		SLD/8	-2,55		SLD/8	-2,26		SLD/8	-2,74
	SLD/9	-2,20		SLD/9	-2,69		SLD/9	-2,38		SLD/9	-2,88
	SLD/10	-2,13		SLD/10	-2,60		SLD/10	-2,31		SLD/10	-2,79
	SLD/11	-2,10		SLD/11	-2,55		SLD/11	-2,26		SLD/11	-2,73
	SLD/12	-2,19		SLD/12	-2,68		SLD/12	-2,37		SLD/12	-2,87
	SLD/13	-2,12		SLD/13	-2,59		SLD/13	-2,30		SLD/13	-2,78
	SLD/14	-2,08		SLD/14	-2,54		SLD/14	-2,25		SLD/14	-2,72
X+	SLD/18	-1,40	X+	SLD/18	-1,69	X+	SLD/18	-1,48	X+	SLD/18	-1,82
X-	SLD/25	-1,50	X-	SLD/25	-1,76	X-	SLD/25	-1,59	X-	SLD/25	-1,89
Y+	SLD/41	-1,49	Y+	SLD/41	-1,77	Y+	SLD/41	-1,58	Y+	SLD/41	-1,91
Y-	SLD/43	-1,40	Y-	SLD/43	-1,69	Y-	SLD/43	-1,51	Y-	SLD/43	-1,79
230	SLD/1	-2,92	231	SLD/1	-3,29	232	SLD/1	-3,14	233	SLD/1	-3,11
	SLD/2	-2,83		SLD/2	-3,20		SLD/2	-3,05		SLD/2	-3,02
	SLD/3	-2,92		SLD/3	-3,29		SLD/3	-3,13		SLD/3	-3,10
	SLD/4	-2,83		SLD/4	-3,19		SLD/4	-3,05		SLD/4	-3,02
	SLD/5	-2,77		SLD/5	-3,13		SLD/5	-2,99		SLD/5	-2,96
	SLD/6	-2,92		SLD/6	-3,29		SLD/6	-3,14		SLD/6	-3,11
	SLD/7	-2,83		SLD/7	-3,20		SLD/7	-3,05		SLD/7	-3,03
	SLD/8	-2,78		SLD/8	-3,13		SLD/8	-3,00		SLD/8	-2,97
	SLD/9	-2,92		SLD/9	-3,29		SLD/9	-3,14		SLD/9	-3,11
	SLD/10	-2,83		SLD/10	-3,20		SLD/10	-3,06		SLD/10	-3,03
	SLD/11	-2,78		SLD/11	-3,13		SLD/11	-3,00		SLD/11	-2,97
	SLD/12	-2,91		SLD/12	-3,29		SLD/12	-3,14		SLD/12	-3,11
	SLD/13	-2,83		SLD/13	-3,19		SLD/13	-3,05		SLD/13	-3,02
	SLD/14	-2,77		SLD/14	-3,12		SLD/14	-2,99		SLD/14	-2,97
X+	SLD/18	-1,87	X+	SLD/18	-2,13	X+	SLD/18	-2,01	X+	SLD/18	-1,99
X-	SLD/25	-1,91	X-	SLD/25	-2,14	X-	SLD/25	-2,11	X-	SLD/25	-2,08
Y+	SLD/41	-1,91	Y+	SLD/41	-2,16	Y+	SLD/41	-2,09	Y+	SLD/41	-2,05
Y-	SLD/43	-1,87	Y-	SLD/43	-2,10	Y-	SLD/43	-2,05	Y-	SLD/43	-2,04
234	SLD/1	-3,13	235	SLD/1	-2,82	236	SLD/1	-2,51	237	SLD/1	-2,56
	SLD/2	-3,04		SLD/2	-2,74		SLD/2	-2,44		SLD/2	-2,48
	SLD/3	-3,13		SLD/3	-2,82		SLD/3	-2,51		SLD/3	-2,56
	SLD/4	-3,04		SLD/4	-2,74		SLD/4	-2,44		SLD/4	-2,48
	SLD/5	-2,97		SLD/5	-2,67		SLD/5	-2,39		SLD/5	-2,43
	SLD/6	-3,13		SLD/6	-2,82		SLD/6	-2,51		SLD/6	-2,56
	SLD/7	-3,04		SLD/7	-2,74		SLD/7	-2,44		SLD/7	-2,49
	SLD/8	-2,97		SLD/8	-2,68		SLD/8	-2,39		SLD/8	-2,43
	SLD/9	-3,13		SLD/9	-2,82		SLD/9	-2,51		SLD/9	-2,56
	SLD/10	-3,03		SLD/10	-2,74		SLD/10	-2,44		SLD/10	-2,48
	SLD/11	-2,96		SLD/11	-2,68		SLD/11	-2,39		SLD/11	-2,42
	SLD/12	-3,12		SLD/12	-2,82		SLD/12	-2,51		SLD/12	-2,56
	SLD/13	-3,03		SLD/13	-2,74		SLD/13	-2,44		SLD/13	-2,48
	SLD/14	-2,96		SLD/14	-2,67		SLD/14	-2,38		SLD/14	-2,42
X+	SLD/18	-2,03	X+	SLD/18	-1,81	X+	SLD/18	-1,61	X+	SLD/18	-1,65
X-	SLD/25	-1,99	X-	SLD/25	-1,82	X-	SLD/25	-1,64	X-	SLD/25	-1,64
Y+	SLD/34	-2,06	Y+	SLD/41	-1,83	Y+	SLD/41	-1,65	Y+	SLD/34	-1,66
Y-	SLD/36	-1,95	Y-	SLD/43	-1,78	Y-	SLD/43	-1,61	Y-	SLD/36	-1,61
238	SLD/1	-2,63	239	SLD/1	-3,75	240	SLD/1	-2,36	241	SLD/1	-2,37
	SLD/2	-2,56		SLD/2	-3,67		SLD/2	-2,31		SLD/2	-2,31
	SLD/3	-2,63		SLD/3	-3,75		SLD/3	-2,36		SLD/3	-2,37
	SLD/4	-2,56		SLD/4	-3,67		SLD/4	-2,31		SLD/4	-2,31
	SLD/5	-2,51		SLD/5	-3,61		SLD/5	-2,27		SLD/5	-2,27
	SLD/6	-2,63		SLD/6	-3,73		SLD/6	-2,35		SLD/6	-2,37
	SLD/7	-2,56		SLD/7	-3,65		SLD/7	-2,30		SLD/7	-2,31
	SLD/8	-2,51		SLD/8	-3,58		SLD/8	-2,26		SLD/8	-2,27
	SLD/9	-2,64		SLD/9	-3,75		SLD/9	-2,36		SLD/9	-2,37
	SLD/10	-2,57		SLD/10	-3,67		SLD/10	-2,31		SLD/10	-2,31
	SLD/11	-2,52		SLD/11	-3,61		SLD/11	-2,27		SLD/11	-2,27
	SLD/12	-2,63		SLD/12	-3,76		SLD/12	-2,36		SLD/12	-2,37
	SLD/13	-2,56		SLD/13	-3,68		SLD/13	-2,31		SLD/13	-2,31

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/14	-2,51		SLD/14	-3,64		SLD/14	-2,28		SLD/14	-2,27
X+	SLD/18	-1,67	X+	SLD/21	-2,57	X+	SLD/21	-1,59	X+	SLD/21	-1,58
X-	SLD/25	-1,77	X-	SLD/30	-2,58	X-	SLD/30	-1,60	X-	SLD/30	-1,58
Y+	SLD/41	-1,74	Y+	SLD/40	-2,36	Y+	SLD/40	-1,52	Y+	SLD/31	-1,58
Y-	SLD/43	-1,73	Y-	SLD/46	-2,69	Y-	SLD/46	-1,64	Y-	SLD/37	-1,58
242	SLD/1	-1,76	243	SLD/1	-1,82	244	SLD/1	-1,65	245	SLD/1	-3,14
	SLD/2	-1,70		SLD/2	-1,76		SLD/2	-1,60		SLD/2	-3,05
	SLD/3	-1,76		SLD/3	-1,82		SLD/3	-1,65		SLD/3	-3,14
	SLD/4	-1,70		SLD/4	-1,76		SLD/4	-1,60		SLD/4	-3,05
	SLD/5	-1,68		SLD/5	-1,73		SLD/5	-1,57		SLD/5	-3,01
	SLD/6	-1,76		SLD/6	-1,82		SLD/6	-1,65		SLD/6	-3,13
	SLD/7	-1,70		SLD/7	-1,76		SLD/7	-1,60		SLD/7	-3,05
	SLD/8	-1,68		SLD/8	-1,73		SLD/8	-1,57		SLD/8	-3,00
	SLD/9	-1,76		SLD/9	-1,82		SLD/9	-1,65		SLD/9	-3,13
	SLD/10	-1,70		SLD/10	-1,76		SLD/10	-1,60		SLD/10	-3,05
	SLD/11	-1,68		SLD/11	-1,73		SLD/11	-1,58		SLD/11	-3,00
	SLD/12	-1,75		SLD/12	-1,82		SLD/12	-1,65		SLD/12	-3,14
	SLD/13	-1,70		SLD/13	-1,76		SLD/13	-1,60		SLD/13	-3,06
	SLD/14	-1,68		SLD/14	-1,73		SLD/14	-1,57		SLD/14	-3,01
X+	SLD/18	-1,18	X+	SLD/18	-1,19	X+	SLD/20	-1,06	X+	SLD/21	-2,10
X-	SLD/25	-1,17	X-	SLD/25	-1,20	X-	SLD/27	-1,11	X-	SLD/30	-2,08
Y+	SLD/34	-1,19	Y+	SLD/41	-1,20	Y+	SLD/41	-1,08	Y+	SLD/31	-2,06
Y-	SLD/36	-1,15	Y-	SLD/43	-1,20	Y-	SLD/43	-1,10	Y-	SLD/37	-2,12
246	SLD/1	-3,05	247	SLD/1	-2,15	248	SLD/1	-2,65	249	SLD/1	-2,44
	SLD/2	-2,98		SLD/2	-2,09		SLD/2	-2,56		SLD/2	-2,35
	SLD/3	-3,05		SLD/3	-2,15		SLD/3	-2,65		SLD/3	-2,43
	SLD/4	-2,98		SLD/4	-2,09		SLD/4	-2,56		SLD/4	-2,35
	SLD/5	-2,93		SLD/5	-2,07		SLD/5	-2,53		SLD/5	-2,33
	SLD/6	-3,05		SLD/6	-2,16		SLD/6	-2,65		SLD/6	-2,44
	SLD/7	-2,98		SLD/7	-2,09		SLD/7	-2,56		SLD/7	-2,35
	SLD/8	-2,93		SLD/8	-2,07		SLD/8	-2,53		SLD/8	-2,33
	SLD/9	-3,05		SLD/9	-2,15		SLD/9	-2,65		SLD/9	-2,44
	SLD/10	-2,98		SLD/10	-2,09		SLD/10	-2,56		SLD/10	-2,35
	SLD/11	-2,93		SLD/11	-2,07		SLD/11	-2,53		SLD/11	-2,33
	SLD/12	-3,06		SLD/12	-2,15		SLD/12	-2,65		SLD/12	-2,44
	SLD/13	-2,99		SLD/13	-2,09		SLD/13	-2,56		SLD/13	-2,35
	SLD/14	-2,94		SLD/14	-2,07		SLD/14	-2,53		SLD/14	-2,33
X+	SLD/21	-2,05	X+	SLD/18	-1,43	X+	SLD/21	-1,76	X+	SLD/20	-1,61
X-	SLD/30	-2,05	X-	SLD/25	-1,44	X-	SLD/30	-1,75	X-	SLD/27	-1,62
Y+	SLD/40	-1,99	Y+	SLD/41	-1,44	Y+	SLD/31	-1,76	Y+	SLD/41	-1,61
Y-	SLD/46	-2,08	Y-	SLD/43	-1,43	Y-	SLD/37	-1,76	Y-	SLD/43	-1,62
250	SLD/1	-1,85	251	SLD/1	-2,87	252	SLD/1	-2,68	253	SLD/1	-2,73
	SLD/2	-1,79		SLD/2	-2,79		SLD/2	-2,60		SLD/2	-2,66
	SLD/3	-1,85		SLD/3	-2,87		SLD/3	-2,68		SLD/3	-2,73
	SLD/4	-1,79		SLD/4	-2,79		SLD/4	-2,60		SLD/4	-2,67
	SLD/5	-1,77		SLD/5	-2,75		SLD/5	-2,57		SLD/5	-2,62
	SLD/6	-1,85		SLD/6	-2,86		SLD/6	-2,68		SLD/6	-2,72
	SLD/7	-1,79		SLD/7	-2,79		SLD/7	-2,60		SLD/7	-2,66
	SLD/8	-1,77		SLD/8	-2,74		SLD/8	-2,56		SLD/8	-2,60
	SLD/9	-1,85		SLD/9	-2,86		SLD/9	-2,68		SLD/9	-2,72
	SLD/10	-1,79		SLD/10	-2,79		SLD/10	-2,59		SLD/10	-2,66
	SLD/11	-1,77		SLD/11	-2,74		SLD/11	-2,56		SLD/11	-2,60
	SLD/12	-1,85		SLD/12	-2,87		SLD/12	-2,68		SLD/12	-2,73
	SLD/13	-1,78		SLD/13	-2,79		SLD/13	-2,60		SLD/13	-2,67
	SLD/14	-1,76		SLD/14	-2,75		SLD/14	-2,56		SLD/14	-2,62
X+	SLD/18	-1,22	X+	SLD/21	-1,94	X+	SLD/21	-1,80	X+	SLD/21	-1,88
X-	SLD/25	-1,24	X-	SLD/30	-1,88	X-	SLD/30	-1,76	X-	SLD/30	-1,76
Y+	SLD/41	-1,24	Y+	SLD/31	-1,89	Y+	SLD/31	-1,77	Y+	SLD/31	-1,78
Y-	SLD/43	-1,21	Y-	SLD/37	-1,94	Y-	SLD/37	-1,79	Y-	SLD/37	-1,87
254	SLD/1	-2,12	255	SLD/1	-2,46	256	SLD/1	-2,59	257	SLD/1	-2,12
	SLD/2	-2,06		SLD/2	-2,38		SLD/2	-2,51		SLD/2	-2,06
	SLD/3	-2,13		SLD/3	-2,46		SLD/3	-2,59		SLD/3	-2,12
	SLD/4	-2,07		SLD/4	-2,38		SLD/4	-2,51		SLD/4	-2,05
	SLD/5	-2,04		SLD/5	-2,35		SLD/5	-2,47		SLD/5	-2,03
	SLD/6	-2,12		SLD/6	-2,46		SLD/6	-2,59		SLD/6	-2,12
	SLD/7	-2,06		SLD/7	-2,38		SLD/7	-2,51		SLD/7	-2,05
	SLD/8	-2,03		SLD/8	-2,35		SLD/8	-2,47		SLD/8	-2,03
	SLD/9	-2,12		SLD/9	-2,46		SLD/9	-2,59		SLD/9	-2,12
	SLD/10	-2,06		SLD/10	-2,38		SLD/10	-2,51		SLD/10	-2,06
	SLD/11	-2,03		SLD/11	-2,35		SLD/11	-2,48		SLD/11	-2,03
	SLD/12	-2,12		SLD/12	-2,46		SLD/12	-2,59		SLD/12	-2,12
	SLD/13	-2,06		SLD/13	-2,38		SLD/13	-2,51		SLD/13	-2,06
	SLD/14	-2,03		SLD/14	-2,35		SLD/14	-2,48		SLD/14	-2,03
X+	SLD/21	-1,44	X+	SLD/21	-1,64	X+	SLD/20	-1,70	X+	SLD/20	-1,39
X-	SLD/30	-1,38	X-	SLD/30	-1,63	X-	SLD/27	-1,73	X-	SLD/27	-1,42
Y+	SLD/31	-1,41	Y+	SLD/31	-1,61	Y+	SLD/41	-1,69	Y+	SLD/41	-1,39
Y-	SLD/37	-1,43	Y-	SLD/37	-1,64	Y-	SLD/43	-1,74	Y-	SLD/43	-1,42

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
258	SLD/1	-2,61	259	SLD/1	-1,83	260	SLD/1	-2,11	261	SLD/1	-3,26
	SLD/2	-2,53		SLD/2	-1,77		SLD/2	-2,04		SLD/2	-3,17
	SLD/3	-2,61		SLD/3	-1,83		SLD/3	-2,11		SLD/3	-3,25
	SLD/4	-2,53		SLD/4	-1,77		SLD/4	-2,04		SLD/4	-3,17
	SLD/5	-2,50		SLD/5	-1,75		SLD/5	-2,02		SLD/5	-3,11
	SLD/6	-2,61		SLD/6	-1,83		SLD/6	-2,10		SLD/6	-3,25
	SLD/7	-2,53		SLD/7	-1,77		SLD/7	-2,04		SLD/7	-3,16
	SLD/8	-2,49		SLD/8	-1,74		SLD/8	-2,01		SLD/8	-3,10
	SLD/9	-2,62		SLD/9	-1,83		SLD/9	-2,11		SLD/9	-3,26
	SLD/10	-2,53		SLD/10	-1,77		SLD/10	-2,04		SLD/10	-3,17
	SLD/11	-2,50		SLD/11	-1,74		SLD/11	-2,01		SLD/11	-3,12
	SLD/12	-2,62		SLD/12	-1,83		SLD/12	-2,12		SLD/12	-3,26
	SLD/13	-2,53		SLD/13	-1,77		SLD/13	-2,05		SLD/13	-3,18
	SLD/14	-2,50		SLD/14	-1,75		SLD/14	-2,02		SLD/14	-3,13
X+	SLD/20	-1,72	X+	SLD/21	-1,23	X+	SLD/21	-1,41	X+	SLD/20	-2,12
X-	SLD/27	-1,75	X-	SLD/30	-1,20	X-	SLD/30	-1,40	X-	SLD/27	-2,21
Y+	SLD/41	-1,69	Y+	SLD/31	-1,20	Y+	SLD/31	-1,34	Y+	SLD/41	-2,10
Y-	SLD/43	-1,77	Y-	SLD/37	-1,23	Y-	SLD/37	-1,44	Y-	SLD/43	-2,22
262	SLD/1	-2,77	263	SLD/1	-2,21	264	SLD/1	-2,19	265	SLD/1	-2,57
	SLD/2	-2,69		SLD/2	-2,15		SLD/2	-2,13		SLD/2	-2,51
	SLD/3	-2,77		SLD/3	-2,21		SLD/3	-2,19		SLD/3	-2,57
	SLD/4	-2,69		SLD/4	-2,15		SLD/4	-2,13		SLD/4	-2,50
	SLD/5	-2,65		SLD/5	-2,11		SLD/5	-2,09		SLD/5	-2,45
	SLD/6	-2,77		SLD/6	-2,21		SLD/6	-2,18		SLD/6	-2,57
	SLD/7	-2,69		SLD/7	-2,15		SLD/7	-2,12		SLD/7	-2,51
	SLD/8	-2,64		SLD/8	-2,11		SLD/8	-2,08		SLD/8	-2,46
	SLD/9	-2,77		SLD/9	-2,21		SLD/9	-2,19		SLD/9	-2,57
	SLD/10	-2,70		SLD/10	-2,15		SLD/10	-2,13		SLD/10	-2,51
	SLD/11	-2,65		SLD/11	-2,11		SLD/11	-2,09		SLD/11	-2,47
	SLD/12	-2,77		SLD/12	-2,21		SLD/12	-2,19		SLD/12	-2,57
	SLD/13	-2,70		SLD/13	-2,15		SLD/13	-2,14		SLD/13	-2,51
	SLD/14	-2,66		SLD/14	-2,12		SLD/14	-2,10		SLD/14	-2,46
X+	SLD/20	-1,82	X+	SLD/21	-1,45	X+	SLD/20	-1,44	X+	SLD/18	-1,65
X-	SLD/27	-1,85	X-	SLD/30	-1,46	X-	SLD/27	-1,46	X-	SLD/25	-1,74
Y+	SLD/41	-1,80	Y+	SLD/40	-1,43	Y+	SLD/41	-1,38	Y+	SLD/41	-1,72
Y-	SLD/43	-1,86	Y-	SLD/46	-1,47	Y-	SLD/43	-1,50	Y-	SLD/43	-1,69
266	SLD/1	-2,38	267	SLD/1	-1,97	268	SLD/1	-3,85	269	SLD/1	-3,25
	SLD/2	-2,32		SLD/2	-1,93		SLD/2	-3,76		SLD/2	-3,18
	SLD/3	-2,38		SLD/3	-1,97		SLD/3	-3,85		SLD/3	-3,25
	SLD/4	-2,32		SLD/4	-1,92		SLD/4	-3,76		SLD/4	-3,17
	SLD/5	-2,27		SLD/5	-1,88		SLD/5	-3,69		SLD/5	-3,11
	SLD/6	-2,38		SLD/6	-1,97		SLD/6	-3,85		SLD/6	-3,25
	SLD/7	-2,32		SLD/7	-1,93		SLD/7	-3,76		SLD/7	-3,18
	SLD/8	-2,28		SLD/8	-1,89		SLD/8	-3,69		SLD/8	-3,12
	SLD/9	-2,38		SLD/9	-1,98		SLD/9	-3,85		SLD/9	-3,26
	SLD/10	-2,33		SLD/10	-1,93		SLD/10	-3,76		SLD/10	-3,18
	SLD/11	-2,28		SLD/11	-1,89		SLD/11	-3,70		SLD/11	-3,12
	SLD/12	-2,38		SLD/12	-1,98		SLD/12	-3,85		SLD/12	-3,25
	SLD/13	-2,32		SLD/13	-1,93		SLD/13	-3,76		SLD/13	-3,18
	SLD/14	-2,28		SLD/14	-1,89		SLD/14	-3,70		SLD/14	-3,12
X+	SLD/20	-1,53	X+	SLD/20	-1,26	X+	SLD/20	-2,52	X+	SLD/18	-2,12
X-	SLD/27	-1,61	X-	SLD/27	-1,34	X-	SLD/27	-2,58	X-	SLD/25	-2,18
Y+	SLD/41	-1,57	Y+	SLD/41	-1,30	Y+	SLD/41	-2,53	Y+	SLD/41	-2,16
Y-	SLD/43	-1,59	Y-	SLD/43	-1,32	Y-	SLD/43	-2,58	Y-	SLD/43	-2,16
270	SLD/1	-3,12	271	SLD/1	-3,43	272	SLD/1	-3,51	273	SLD/1	-2,86
	SLD/2	-3,04		SLD/2	-3,34		SLD/2	-3,43		SLD/2	-2,79
	SLD/3	-3,11		SLD/3	-3,42		SLD/3	-3,51		SLD/3	-2,86
	SLD/4	-3,04		SLD/4	-3,34		SLD/4	-3,42		SLD/4	-2,79
	SLD/5	-2,98		SLD/5	-3,28		SLD/5	-3,36		SLD/5	-2,74
	SLD/6	-3,12		SLD/6	-3,43		SLD/6	-3,51		SLD/6	-2,86
	SLD/7	-3,04		SLD/7	-3,34		SLD/7	-3,42		SLD/7	-2,79
	SLD/8	-2,99		SLD/8	-3,28		SLD/8	-3,36		SLD/8	-2,73
	SLD/9	-3,12		SLD/9	-3,43		SLD/9	-3,51		SLD/9	-2,86
	SLD/10	-3,05		SLD/10	-3,35		SLD/10	-3,43		SLD/10	-2,79
	SLD/11	-2,99		SLD/11	-3,29		SLD/11	-3,37		SLD/11	-2,74
	SLD/12	-3,12		SLD/12	-3,43		SLD/12	-3,51		SLD/12	-2,86
	SLD/13	-3,04		SLD/13	-3,34		SLD/13	-3,43		SLD/13	-2,79
	SLD/14	-2,99		SLD/14	-3,29		SLD/14	-3,37		SLD/14	-2,74
X+	SLD/20	-2,03	X+	SLD/20	-2,24	X+	SLD/20	-2,29	X+	SLD/20	-1,89
X-	SLD/27	-2,10	X-	SLD/27	-2,30	X-	SLD/27	-2,37	X-	SLD/27	-1,88
Y+	SLD/41	-2,06	Y+	SLD/41	-2,27	Y+	SLD/41	-2,31	Y+	SLD/34	-1,87
Y-	SLD/43	-2,08	Y-	SLD/43	-2,28	Y-	SLD/43	-2,36	Y-	SLD/36	-1,89
274	SLD/1	-2,73	275	SLD/1	-3,45	276	SLD/1	-1,97	277	SLD/1	-2,90
	SLD/2	-2,67		SLD/2	-3,37		SLD/2	-1,92		SLD/2	-2,84
	SLD/3	-2,73		SLD/3	-3,45		SLD/3	-1,97		SLD/3	-2,90
	SLD/4	-2,67		SLD/4	-3,36		SLD/4	-1,92		SLD/4	-2,83
	SLD/5	-2,62		SLD/5	-3,30		SLD/5	-1,88		SLD/5	-2,78
	SLD/6	-2,73		SLD/6	-3,45		SLD/6	-1,97		SLD/6	-2,91

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/7	-2,67		SLD/7	-3,37		SLD/7	-1,92		SLD/7	-2,84
	SLD/8	-2,62		SLD/8	-3,31		SLD/8	-1,88		SLD/8	-2,79
	SLD/9	-2,73		SLD/9	-3,45		SLD/9	-1,97		SLD/9	-2,91
	SLD/10	-2,67		SLD/10	-3,37		SLD/10	-1,92		SLD/10	-2,84
	SLD/11	-2,62		SLD/11	-3,31		SLD/11	-1,89		SLD/11	-2,79
	SLD/12	-2,73		SLD/12	-3,45		SLD/12	-1,97		SLD/12	-2,90
	SLD/13	-2,67		SLD/13	-3,37		SLD/13	-1,92		SLD/13	-2,83
	SLD/14	-2,62		SLD/14	-3,31		SLD/14	-1,89		SLD/14	-2,78
X+	SLD/21	-1,82	X+	SLD/20	-2,26	X+	SLD/21	-1,29	X+	SLD/18	-1,90
X-	SLD/30	-1,79	X-	SLD/27	-2,30	X-	SLD/30	-1,31	X-	SLD/25	-1,94
Y+	SLD/31	-1,81	Y+	SLD/41	-2,28	Y+	SLD/40	-1,29	Y+	SLD/41	-1,93
Y-	SLD/37	-1,81	Y-	SLD/43	-2,29	Y-	SLD/46	-1,31	Y-	SLD/43	-1,92
278	SLD/1	-2,48	279	SLD/1	-2,93	280	SLD/1	-1,73	281	SLD/1	-1,76
	SLD/2	-2,42		SLD/2	-2,87		SLD/2	-1,68		SLD/2	-1,70
	SLD/3	-2,48		SLD/3	-2,93		SLD/3	-1,73		SLD/3	-1,76
	SLD/4	-2,42		SLD/4	-2,86		SLD/4	-1,67		SLD/4	-1,70
	SLD/5	-2,37		SLD/5	-2,81		SLD/5	-1,64		SLD/5	-1,67
	SLD/6	-2,48		SLD/6	-2,94		SLD/6	-1,74		SLD/6	-1,76
	SLD/7	-2,42		SLD/7	-2,87		SLD/7	-1,68		SLD/7	-1,71
	SLD/8	-2,38		SLD/8	-2,82		SLD/8	-1,65		SLD/8	-1,68
	SLD/9	-2,48		SLD/9	-2,94		SLD/9	-1,74		SLD/9	-1,76
	SLD/10	-2,42		SLD/10	-2,87		SLD/10	-1,68		SLD/10	-1,70
	SLD/11	-2,37		SLD/11	-2,82		SLD/11	-1,65		SLD/11	-1,68
	SLD/12	-2,48		SLD/12	-2,93		SLD/12	-1,73		SLD/12	-1,75
	SLD/13	-2,42		SLD/13	-2,86		SLD/13	-1,67		SLD/13	-1,70
	SLD/14	-2,37		SLD/14	-2,81		SLD/14	-1,64		SLD/14	-1,67
X+	SLD/15	-1,64	X+	SLD/18	-1,90	X+	SLD/18	-1,07	X+	SLD/18	-1,13
X-	SLD/24	-1,64	X-	SLD/25	-1,98	X-	SLD/25	-1,18	X-	SLD/25	-1,20
Y+	SLD/40	-1,65	Y+	SLD/41	-1,97	Y+	SLD/41	-1,17	Y+	SLD/41	-1,20
Y-	SLD/46	-1,61	Y-	SLD/43	-1,93	Y-	SLD/43	-1,09	Y-	SLD/43	-1,13
282	SLD/1	-2,19	283	SLD/1	-2,55	284	SLD/1	-3,94	285	SLD/1	-3,17
	SLD/2	-2,11		SLD/2	-2,47		SLD/2	-3,86		SLD/2	-3,07
	SLD/3	-2,19		SLD/3	-2,55		SLD/3	-3,93		SLD/3	-3,16
	SLD/4	-2,11		SLD/4	-2,47		SLD/4	-3,85		SLD/4	-3,07
	SLD/5	-2,08		SLD/5	-2,42		SLD/5	-3,79		SLD/5	-3,03
	SLD/6	-2,19		SLD/6	-2,56		SLD/6	-3,97		SLD/6	-3,18
	SLD/7	-2,12		SLD/7	-2,47		SLD/7	-3,88		SLD/7	-3,08
	SLD/8	-2,09		SLD/8	-2,43		SLD/8	-3,84		SLD/8	-3,05
	SLD/9	-2,19		SLD/9	-2,56		SLD/9	-3,95		SLD/9	-3,17
	SLD/10	-2,12		SLD/10	-2,47		SLD/10	-3,87		SLD/10	-3,08
	SLD/11	-2,09		SLD/11	-2,43		SLD/11	-3,82		SLD/11	-3,04
	SLD/12	-2,19		SLD/12	-2,55		SLD/12	-3,92		SLD/12	-3,16
	SLD/13	-2,11		SLD/13	-2,46		SLD/13	-3,83		SLD/13	-3,06
	SLD/14	-2,08		SLD/14	-2,42		SLD/14	-3,76		SLD/14	-3,02
X+	SLD/18	-1,42	X+	SLD/18	-1,64	X+	SLD/18	-2,64	X+	SLD/18	-2,11
X-	SLD/25	-1,48	X-	SLD/25	-1,69	X-	SLD/25	-2,89	X-	SLD/25	-2,20
Y+	SLD/41	-1,49	Y+	SLD/41	-1,71	Y+	SLD/41	-2,98	Y+	SLD/41	-2,25
Y-	SLD/43	-1,41	Y-	SLD/43	-1,62	Y-	SLD/43	-2,48	Y-	SLD/43	-2,03
286	SLD/1	-2,64	287	SLD/1	-3,44	288	SLD/1	-3,77	289	SLD/1	-2,95
	SLD/2	-2,55		SLD/2	-3,37		SLD/2	-3,69		SLD/2	-2,87
	SLD/3	-2,63		SLD/3	-3,43		SLD/3	-3,75		SLD/3	-2,95
	SLD/4	-2,55		SLD/4	-3,35		SLD/4	-3,67		SLD/4	-2,87
	SLD/5	-2,52		SLD/5	-3,31		SLD/5	-3,62		SLD/5	-2,83
	SLD/6	-2,64		SLD/6	-3,46		SLD/6	-3,79		SLD/6	-2,96
	SLD/7	-2,56		SLD/7	-3,39		SLD/7	-3,71		SLD/7	-2,88
	SLD/8	-2,54		SLD/8	-3,36		SLD/8	-3,68		SLD/8	-2,86
	SLD/9	-2,64		SLD/9	-3,45		SLD/9	-3,78		SLD/9	-2,96
	SLD/10	-2,56		SLD/10	-3,38		SLD/10	-3,71		SLD/10	-2,88
	SLD/11	-2,53		SLD/11	-3,34		SLD/11	-3,67		SLD/11	-2,85
	SLD/12	-2,63		SLD/12	-3,42		SLD/12	-3,75		SLD/12	-2,95
	SLD/13	-2,54		SLD/13	-3,35		SLD/13	-3,67		SLD/13	-2,86
	SLD/14	-2,52		SLD/14	-3,29		SLD/14	-3,61		SLD/14	-2,83
X+	SLD/18	-1,75	X+	SLD/18	-2,28	X+	SLD/18	-2,43	X+	SLD/18	-1,95
X-	SLD/25	-1,84	X-	SLD/25	-2,56	X-	SLD/25	-2,85	X-	SLD/25	-2,09
Y+	SLD/41	-1,86	Y+	SLD/41	-2,61	Y+	SLD/41	-2,84	Y+	SLD/41	-2,10
Y-	SLD/43	-1,71	Y-	SLD/43	-2,19	Y-	SLD/43	-2,44	Y-	SLD/43	-1,94
290	SLD/1	-2,34	291	SLD/1	-2,64	292	SLD/1	-2,52	293	SLD/1	-2,80
	SLD/2	-2,26		SLD/2	-2,55		SLD/2	-2,44		SLD/2	-2,71
	SLD/3	-2,34		SLD/3	-2,64		SLD/3	-2,53		SLD/3	-2,80
	SLD/4	-2,26		SLD/4	-2,55		SLD/4	-2,44		SLD/4	-2,71
	SLD/5	-2,23		SLD/5	-2,53		SLD/5	-2,41		SLD/5	-2,68
	SLD/6	-2,34		SLD/6	-2,64		SLD/6	-2,53		SLD/6	-2,79
	SLD/7	-2,26		SLD/7	-2,55		SLD/7	-2,44		SLD/7	-2,71
	SLD/8	-2,24		SLD/8	-2,53		SLD/8	-2,40		SLD/8	-2,66
	SLD/9	-2,34		SLD/9	-2,64		SLD/9	-2,52		SLD/9	-2,79
	SLD/10	-2,26		SLD/10	-2,55		SLD/10	-2,44		SLD/10	-2,71
	SLD/11	-2,23		SLD/11	-2,53		SLD/11	-2,40		SLD/11	-2,67
	SLD/12	-2,34		SLD/12	-2,64		SLD/12	-2,52		SLD/12	-2,80

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/13	-2,25		SLD/13	-2,55		SLD/13	-2,44		SLD/13	-2,72
	SLD/14	-2,23		SLD/14	-2,53		SLD/14	-2,40		SLD/14	-2,68
X+	SLD/18	-1,55	X+	SLD/18	-1,76	X+	SLD/18	-1,66	X+	SLD/21	-1,89
X-	SLD/25	-1,55	X-	SLD/25	-1,76	X-	SLD/25	-1,64	X-	SLD/30	-1,83
Y+	SLD/41	-1,56	Y+	SLD/41	-1,76	Y+	SLD/34	-1,66	Y+	SLD/31	-1,80
Y-	SLD/43	-1,53	Y-	SLD/43	-1,75	Y-	SLD/36	-1,65	Y-	SLD/37	-1,91
294	SLD/1	-3,26	295	SLD/1	-3,69	296	SLD/1	-5,05	297	SLD/1	-1,74
	SLD/2	-3,18		SLD/2	-3,62		SLD/2	-4,97		SLD/2	-1,69
	SLD/3	-3,26		SLD/3	-3,68		SLD/3	-5,02		SLD/3	-1,74
	SLD/4	-3,18		SLD/4	-3,61		SLD/4	-4,94		SLD/4	-1,69
	SLD/5	-3,14		SLD/5	-3,55		SLD/5	-4,85		SLD/5	-1,65
	SLD/6	-3,26		SLD/6	-3,70		SLD/6	-5,08		SLD/6	-1,74
	SLD/7	-3,18		SLD/7	-3,63		SLD/7	-5,00		SLD/7	-1,69
	SLD/8	-3,14		SLD/8	-3,59		SLD/8	-4,95		SLD/8	-1,66
	SLD/9	-3,26		SLD/9	-3,70		SLD/9	-5,08		SLD/9	-1,74
	SLD/10	-3,18		SLD/10	-3,62		SLD/10	-5,00		SLD/10	-1,69
	SLD/11	-3,14		SLD/11	-3,58		SLD/11	-4,94		SLD/11	-1,65
	SLD/12	-3,26		SLD/12	-3,68		SLD/12	-5,02		SLD/12	-1,74
	SLD/13	-3,18		SLD/13	-3,60		SLD/13	-4,94		SLD/13	-1,69
	SLD/14	-3,14		SLD/14	-3,54		SLD/14	-4,84		SLD/14	-1,64
X+	SLD/18	-2,17	X+	SLD/18	-2,45	X+	SLD/18	-3,20	X+	SLD/18	-1,14
X-	SLD/25	-2,23	X-	SLD/25	-2,68	X-	SLD/25	-3,93	X-	SLD/25	-1,11
Y+	SLD/41	-2,21	Y+	SLD/41	-2,70	Y+	SLD/41	-3,90	Y+	SLD/34	-1,15
Y-	SLD/43	-2,20	Y-	SLD/43	-2,41	Y-	SLD/43	-3,26	Y-	SLD/36	-1,09
298	SLD/1	-2,00	299	SLD/1	-2,71	300	SLD/1	-2,73	301	SLD/1	-2,08
	SLD/2	-1,95		SLD/2	-2,63		SLD/2	-2,64		SLD/2	-2,02
	SLD/3	-2,00		SLD/3	-2,71		SLD/3	-2,73		SLD/3	-2,08
	SLD/4	-1,95		SLD/4	-2,63		SLD/4	-2,64		SLD/4	-2,02
	SLD/5	-1,91		SLD/5	-2,58		SLD/5	-2,59		SLD/5	-1,98
	SLD/6	-2,01		SLD/6	-2,71		SLD/6	-2,73		SLD/6	-2,08
	SLD/7	-1,95		SLD/7	-2,63		SLD/7	-2,65		SLD/7	-2,02
	SLD/8	-1,91		SLD/8	-2,58		SLD/8	-2,60		SLD/8	-1,98
	SLD/9	-2,01		SLD/9	-2,71		SLD/9	-2,73		SLD/9	-2,08
	SLD/10	-1,95		SLD/10	-2,63		SLD/10	-2,64		SLD/10	-2,03
	SLD/11	-1,91		SLD/11	-2,58		SLD/11	-2,59		SLD/11	-1,99
	SLD/12	-2,00		SLD/12	-2,71		SLD/12	-2,72		SLD/12	-2,08
	SLD/13	-1,95		SLD/13	-2,62		SLD/13	-2,64		SLD/13	-2,02
	SLD/14	-1,90		SLD/14	-2,57		SLD/14	-2,58		SLD/14	-1,98
X+	SLD/18	-1,29	X+	SLD/18	-1,76	X+	SLD/18	-1,78	X+	SLD/18	-1,31
X-	SLD/25	-1,31	X-	SLD/25	-1,77	X-	SLD/25	-1,76	X-	SLD/25	-1,40
Y+	SLD/41	-1,32	Y+	SLD/41	-1,77	Y+	SLD/34	-1,81	Y+	SLD/41	-1,38
Y-	SLD/43	-1,28	Y-	SLD/43	-1,74	Y-	SLD/36	-1,72	Y-	SLD/43	-1,36
302	SLD/1	-2,80	303	SLD/1	-2,59	304	SLD/1	-2,63	305	SLD/1	-2,79
	SLD/2	-2,71		SLD/2	-2,50		SLD/2	-2,55		SLD/2	-2,71
	SLD/3	-2,79		SLD/3	-2,59		SLD/3	-2,63		SLD/3	-2,79
	SLD/4	-2,71		SLD/4	-2,51		SLD/4	-2,55		SLD/4	-2,71
	SLD/5	-2,66		SLD/5	-2,46		SLD/5	-2,51		SLD/5	-2,67
	SLD/6	-2,80		SLD/6	-2,59		SLD/6	-2,63		SLD/6	-2,78
	SLD/7	-2,71		SLD/7	-2,50		SLD/7	-2,55		SLD/7	-2,70
	SLD/8	-2,66		SLD/8	-2,46		SLD/8	-2,50		SLD/8	-2,65
	SLD/9	-2,80		SLD/9	-2,59		SLD/9	-2,63		SLD/9	-2,79
	SLD/10	-2,71		SLD/10	-2,50		SLD/10	-2,55		SLD/10	-2,70
	SLD/11	-2,67		SLD/11	-2,46		SLD/11	-2,50		SLD/11	-2,65
	SLD/12	-2,79		SLD/12	-2,59		SLD/12	-2,63		SLD/12	-2,80
	SLD/13	-2,71		SLD/13	-2,51		SLD/13	-2,55		SLD/13	-2,71
	SLD/14	-2,66		SLD/14	-2,47		SLD/14	-2,50		SLD/14	-2,67
X+	SLD/18	-1,79	X+	SLD/20	-1,70	X+	SLD/20	-1,73	X+	SLD/21	-1,88
X-	SLD/25	-1,85	X-	SLD/27	-1,68	X-	SLD/27	-1,69	X-	SLD/30	-1,80
Y+	SLD/41	-1,84	Y+	SLD/34	-1,67	Y+	SLD/34	-1,71	Y+	SLD/31	-1,78
Y-	SLD/43	-1,82	Y-	SLD/36	-1,70	Y-	SLD/36	-1,72	Y-	SLD/37	-1,90
306	SLD/1	-2,67	307	SLD/1	-2,66	308	SLD/1	-2,70	309	SLD/1	-2,06
	SLD/2	-2,59		SLD/2	-2,58		SLD/2	-2,62		SLD/2	-2,00
	SLD/3	-2,67		SLD/3	-2,66		SLD/3	-2,70		SLD/3	-2,05
	SLD/4	-2,59		SLD/4	-2,57		SLD/4	-2,62		SLD/4	-2,00
	SLD/5	-2,55		SLD/5	-2,53		SLD/5	-2,57		SLD/5	-1,96
	SLD/6	-2,66		SLD/6	-2,66		SLD/6	-2,69		SLD/6	-2,06
	SLD/7	-2,58		SLD/7	-2,57		SLD/7	-2,61		SLD/7	-2,00
	SLD/8	-2,53		SLD/8	-2,53		SLD/8	-2,56		SLD/8	-1,96
	SLD/9	-2,67		SLD/9	-2,66		SLD/9	-2,70		SLD/9	-2,06
	SLD/10	-2,58		SLD/10	-2,58		SLD/10	-2,62		SLD/10	-2,00
	SLD/11	-2,54		SLD/11	-2,53		SLD/11	-2,57		SLD/11	-1,97
	SLD/12	-2,68		SLD/12	-2,66		SLD/12	-2,71		SLD/12	-2,05
	SLD/13	-2,59		SLD/13	-2,58		SLD/13	-2,62		SLD/13	-2,00
	SLD/14	-2,55		SLD/14	-2,54		SLD/14	-2,58		SLD/14	-1,96
X+	SLD/21	-1,79	X+	SLD/21	-1,73	X+	SLD/21	-1,78	X+	SLD/18	-1,32
X-	SLD/30	-1,72	X-	SLD/30	-1,74	X-	SLD/30	-1,76	X-	SLD/25	-1,38
Y+	SLD/31	-1,70	Y+	SLD/40	-1,70	Y+	SLD/31	-1,69	Y+	SLD/41	-1,37
Y-	SLD/37	-1,80	Y-	SLD/46	-1,76	Y-	SLD/37	-1,82	Y-	SLD/43	-1,34

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
310	SLD/1	-1,91	311	SLD/1	-1,63	312	SLD/1	-3,69	313	SLD/1	-3,23
	SLD/2	-1,85		SLD/2	-1,59		SLD/2	-3,60		SLD/2	-3,15
	SLD/3	-1,91		SLD/3	-1,63		SLD/3	-3,69		SLD/3	-3,24
	SLD/4	-1,85		SLD/4	-1,59		SLD/4	-3,60		SLD/4	-3,16
	SLD/5	-1,82		SLD/5	-1,56		SLD/5	-3,55		SLD/5	-3,10
	SLD/6	-1,91		SLD/6	-1,64		SLD/6	-3,68		SLD/6	-3,22
	SLD/7	-1,85		SLD/7	-1,59		SLD/7	-3,60		SLD/7	-3,14
	SLD/8	-1,81		SLD/8	-1,56		SLD/8	-3,53		SLD/8	-3,07
	SLD/9	-1,91		SLD/9	-1,64		SLD/9	-3,69		SLD/9	-3,23
	SLD/10	-1,85		SLD/10	-1,60		SLD/10	-3,60		SLD/10	-3,14
	SLD/11	-1,82		SLD/11	-1,57		SLD/11	-3,54		SLD/11	-3,08
	SLD/12	-1,91		SLD/12	-1,63		SLD/12	-3,70		SLD/12	-3,24
	SLD/13	-1,85		SLD/13	-1,59		SLD/13	-3,61		SLD/13	-3,16
	SLD/14	-1,82		SLD/14	-1,56		SLD/14	-3,56		SLD/14	-3,11
X+	SLD/21	-1,23	X+	SLD/18	-1,04	X+	SLD/21	-2,50	X+	SLD/21	-2,24
X-	SLD/30	-1,26	X-	SLD/25	-1,10	X-	SLD/30	-2,47	X-	SLD/30	-2,06
Y+	SLD/40	-1,23	Y+	SLD/41	-1,09	Y+	SLD/31	-2,39	Y+	SLD/31	-2,05
Y-	SLD/46	-1,27	Y-	SLD/43	-1,07	Y-	SLD/37	-2,54	Y-	SLD/37	-2,24
314	SLD/1	-2,95	315	SLD/1	-2,95	316	SLD/1	-3,52	317	SLD/1	-3,04
	SLD/2	-2,87		SLD/2	-2,87		SLD/2	-3,44		SLD/2	-2,97
	SLD/3	-2,96		SLD/3	-2,96		SLD/3	-3,52		SLD/3	-3,04
	SLD/4	-2,87		SLD/4	-2,87		SLD/4	-3,44		SLD/4	-2,97
	SLD/5	-2,82		SLD/5	-2,83		SLD/5	-3,39		SLD/5	-2,93
	SLD/6	-2,94		SLD/6	-2,95		SLD/6	-3,51		SLD/6	-3,04
	SLD/7	-2,86		SLD/7	-2,86		SLD/7	-3,43		SLD/7	-2,97
	SLD/8	-2,80		SLD/8	-2,81		SLD/8	-3,36		SLD/8	-2,92
	SLD/9	-2,94		SLD/9	-2,94		SLD/9	-3,51		SLD/9	-3,04
	SLD/10	-2,86		SLD/10	-2,86		SLD/10	-3,43		SLD/10	-2,97
	SLD/11	-2,80		SLD/11	-2,81		SLD/11	-3,36		SLD/11	-2,93
	SLD/12	-2,96		SLD/12	-2,95		SLD/12	-3,52		SLD/12	-3,05
	SLD/13	-2,87		SLD/13	-2,87		SLD/13	-3,44		SLD/13	-2,98
	SLD/14	-2,82		SLD/14	-2,82		SLD/14	-3,39		SLD/14	-2,94
X+	SLD/21	-2,01	X+	SLD/20	-2,03	X+	SLD/21	-2,44	X+	SLD/21	-2,10
X-	SLD/30	-1,86	X-	SLD/27	-1,86	X-	SLD/30	-2,27	X-	SLD/30	-2,04
Y+	SLD/31	-1,87	Y+	SLD/34	-1,92	Y+	SLD/31	-2,29	Y+	SLD/31	-1,99
Y-	SLD/37	-2,01	Y-	SLD/36	-2,00	Y-	SLD/37	-2,44	Y-	SLD/37	-2,12
318	SLD/1	-2,71	319	SLD/1	-2,87	320	SLD/1	-2,75	321	SLD/1	-2,43
	SLD/2	-2,62		SLD/2	-2,78		SLD/2	-2,67		SLD/2	-2,35
	SLD/3	-2,71		SLD/3	-2,87		SLD/3	-2,76		SLD/3	-2,43
	SLD/4	-2,63		SLD/4	-2,79		SLD/4	-2,67		SLD/4	-2,35
	SLD/5	-2,59		SLD/5	-2,73		SLD/5	-2,62		SLD/5	-2,32
	SLD/6	-2,70		SLD/6	-2,86		SLD/6	-2,75		SLD/6	-2,43
	SLD/7	-2,62		SLD/7	-2,78		SLD/7	-2,67		SLD/7	-2,35
	SLD/8	-2,59		SLD/8	-2,71		SLD/8	-2,62		SLD/8	-2,32
	SLD/9	-2,70		SLD/9	-2,87		SLD/9	-2,75		SLD/9	-2,43
	SLD/10	-2,62		SLD/10	-2,78		SLD/10	-2,66		SLD/10	-2,34
	SLD/11	-2,59		SLD/11	-2,72		SLD/11	-2,61		SLD/11	-2,31
	SLD/12	-2,71		SLD/12	-2,88		SLD/12	-2,75		SLD/12	-2,43
	SLD/13	-2,63		SLD/13	-2,79		SLD/13	-2,67		SLD/13	-2,34
	SLD/14	-2,59		SLD/14	-2,74		SLD/14	-2,61		SLD/14	-2,31
X+	SLD/21	-1,84	X+	SLD/21	-1,90	X+	SLD/18	-1,82	X+	SLD/18	-1,62
X-	SLD/30	-1,77	X-	SLD/30	-1,84	X-	SLD/25	-1,75	X-	SLD/25	-1,57
Y+	SLD/31	-1,78	Y+	SLD/31	-1,79	Y+	SLD/34	-1,81	Y+	SLD/34	-1,62
Y-	SLD/37	-1,83	Y-	SLD/37	-1,92	Y-	SLD/36	-1,77	Y-	SLD/36	-1,57
322	SLD/1	-2,07	323	SLD/1	-1,72	324	SLD/1	-3,16	325	SLD/1	-3,94
	SLD/2	-2,01		SLD/2	-1,67		SLD/2	-3,08		SLD/2	-3,86
	SLD/3	-2,07		SLD/3	-1,72		SLD/3	-3,15		SLD/3	-3,93
	SLD/4	-2,01		SLD/4	-1,67		SLD/4	-3,07		SLD/4	-3,85
	SLD/5	-1,97		SLD/5	-1,63		SLD/5	-3,03		SLD/5	-3,79
	SLD/6	-2,07		SLD/6	-1,71		SLD/6	-3,17		SLD/6	-3,95
	SLD/7	-2,00		SLD/7	-1,66		SLD/7	-3,09		SLD/7	-3,87
	SLD/8	-1,96		SLD/8	-1,62		SLD/8	-3,06		SLD/8	-3,83
	SLD/9	-2,07		SLD/9	-1,72		SLD/9	-3,17		SLD/9	-3,95
	SLD/10	-2,01		SLD/10	-1,67		SLD/10	-3,09		SLD/10	-3,88
	SLD/11	-1,97		SLD/11	-1,63		SLD/11	-3,06		SLD/11	-3,84
	SLD/12	-2,08		SLD/12	-1,73		SLD/12	-3,15		SLD/12	-3,93
	SLD/13	-2,02		SLD/13	-1,68		SLD/13	-3,07		SLD/13	-3,86
	SLD/14	-1,98		SLD/14	-1,64		SLD/14	-3,03		SLD/14	-3,80
X+	SLD/21	-1,35	X+	SLD/21	-1,11	X+	SLD/15	-2,08	X+	SLD/15	-2,56
X-	SLD/30	-1,37	X-	SLD/30	-1,12	X-	SLD/24	-2,24	X-	SLD/24	-2,89
Y+	SLD/40	-1,28	Y+	SLD/40	-1,05	Y+	SLD/40	-2,22	Y+	SLD/40	-2,82
Y-	SLD/46	-1,40	Y-	SLD/46	-1,16	Y-	SLD/46	-2,11	Y-	SLD/46	-2,71
326	SLD/1	-4,70	327	SLD/1	-3,60	328	SLD/1	-3,15	329	SLD/1	-2,76
	SLD/2	-4,63		SLD/2	-3,52		SLD/2	-3,08		SLD/2	-2,68
	SLD/3	-4,67		SLD/3	-3,59		SLD/3	-3,14		SLD/3	-2,76
	SLD/4	-4,60		SLD/4	-3,51		SLD/4	-3,07		SLD/4	-2,68
	SLD/5	-4,52		SLD/5	-3,46		SLD/5	-3,04		SLD/5	-2,65

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/6	-4,74		SLD/6	-3,62		SLD/6	-3,14		SLD/6	-2,76
	SLD/7	-4,66		SLD/7	-3,54		SLD/7	-3,07		SLD/7	-2,68
	SLD/8	-4,62		SLD/8	-3,51		SLD/8	-3,03		SLD/8	-2,65
	SLD/9	-4,72		SLD/9	-3,61		SLD/9	-3,15		SLD/9	-2,76
	SLD/10	-4,65		SLD/10	-3,54		SLD/10	-3,08		SLD/10	-2,68
	SLD/11	-4,60		SLD/11	-3,50		SLD/11	-3,05		SLD/11	-2,65
	SLD/12	-4,66		SLD/12	-3,58		SLD/12	-3,15		SLD/12	-2,76
	SLD/13	-4,59		SLD/13	-3,50		SLD/13	-3,08		SLD/13	-2,68
	SLD/14	-4,49		SLD/14	-3,44		SLD/14	-3,05		SLD/14	-2,65
X+	SLD/15	-3,03	X+	SLD/15	-2,35	X+	SLD/21	-2,12	X+	SLD/21	-1,85
X-	SLD/24	-3,64	X-	SLD/24	-2,65	X-	SLD/30	-2,22	X-	SLD/30	-1,87
Y+	SLD/40	-3,68	Y+	SLD/40	-2,68	Y+	SLD/40	-2,12	Y+	SLD/40	-1,85
Y-	SLD/46	-2,96	Y-	SLD/46	-2,30	Y-	SLD/46	-2,22	Y-	SLD/46	-1,87
330	SLD/1	-2,47	331	SLD/1	-2,94	332	SLD/1	-3,38	333	SLD/1	-2,73
	SLD/2	-2,39		SLD/2	-2,86		SLD/2	-3,30		SLD/2	-2,64
	SLD/3	-2,47		SLD/3	-2,94		SLD/3	-3,37		SLD/3	-2,73
	SLD/4	-2,39		SLD/4	-2,86		SLD/4	-3,29		SLD/4	-2,64
	SLD/5	-2,36		SLD/5	-2,82		SLD/5	-3,24		SLD/5	-2,60
	SLD/6	-2,48		SLD/6	-2,95		SLD/6	-3,39		SLD/6	-2,73
	SLD/7	-2,39		SLD/7	-2,87		SLD/7	-3,31		SLD/7	-2,64
	SLD/8	-2,37		SLD/8	-2,83		SLD/8	-3,27		SLD/8	-2,60
	SLD/9	-2,47		SLD/9	-2,95		SLD/9	-3,38		SLD/9	-2,73
	SLD/10	-2,39		SLD/10	-2,87		SLD/10	-3,31		SLD/10	-2,65
	SLD/11	-2,36		SLD/11	-2,83		SLD/11	-3,26		SLD/11	-2,60
	SLD/12	-2,47		SLD/12	-2,94		SLD/12	-3,36		SLD/12	-2,73
	SLD/13	-2,39		SLD/13	-2,86		SLD/13	-3,29		SLD/13	-2,64
	SLD/14	-2,36		SLD/14	-2,82		SLD/14	-3,23		SLD/14	-2,60
X+	SLD/15	-1,64	X+	SLD/15	-1,94	X+	SLD/15	-2,21	X+	SLD/21	-1,75
X-	SLD/24	-1,65	X-	SLD/24	-2,03	X-	SLD/24	-2,39	X-	SLD/30	-1,81
Y+	SLD/40	-1,66	Y+	SLD/40	-2,03	Y+	SLD/40	-2,40	Y+	SLD/40	-1,79
Y-	SLD/46	-1,62	Y-	SLD/46	-1,93	Y-	SLD/46	-2,18	Y-	SLD/46	-1,79
334	SLD/1	-2,32	335	SLD/1	-2,36	336	SLD/1	-2,71	337	SLD/1	-2,47
	SLD/2	-2,25		SLD/2	-2,29		SLD/2	-2,62		SLD/2	-2,41
	SLD/3	-2,32		SLD/3	-2,35		SLD/3	-2,70		SLD/3	-2,47
	SLD/4	-2,25		SLD/4	-2,28		SLD/4	-2,62		SLD/4	-2,40
	SLD/5	-2,21		SLD/5	-2,23		SLD/5	-2,56		SLD/5	-2,36
	SLD/6	-2,32		SLD/6	-2,35		SLD/6	-2,70		SLD/6	-2,48
	SLD/7	-2,25		SLD/7	-2,28		SLD/7	-2,62		SLD/7	-2,41
	SLD/8	-2,21		SLD/8	-2,23		SLD/8	-2,56		SLD/8	-2,37
	SLD/9	-2,32		SLD/9	-2,36		SLD/9	-2,71		SLD/9	-2,48
	SLD/10	-2,25		SLD/10	-2,29		SLD/10	-2,62		SLD/10	-2,41
	SLD/11	-2,22		SLD/11	-2,24		SLD/11	-2,57		SLD/11	-2,36
	SLD/12	-2,32		SLD/12	-2,36		SLD/12	-2,71		SLD/12	-2,47
	SLD/13	-2,25		SLD/13	-2,29		SLD/13	-2,62		SLD/13	-2,40
	SLD/14	-2,21		SLD/14	-2,25		SLD/14	-2,57		SLD/14	-2,36
X+	SLD/21	-1,49	X+	SLD/21	-1,51	X+	SLD/21	-1,71	X+	SLD/18	-1,60
X-	SLD/30	-1,54	X-	SLD/30	-1,56	X-	SLD/30	-1,80	X-	SLD/25	-1,65
Y+	SLD/40	-1,50	Y+	SLD/40	-1,47	Y+	SLD/40	-1,73	Y+	SLD/41	-1,64
Y-	SLD/46	-1,54	Y-	SLD/46	-1,59	Y-	SLD/46	-1,78	Y-	SLD/43	-1,61
338	SLD/1	-2,99	339	SLD/1	-2,62	340	SLD/1	-2,89	341	SLD/1	-1,67
	SLD/2	-2,91		SLD/2	-2,54		SLD/2	-2,80		SLD/2	-1,63
	SLD/3	-2,99		SLD/3	-2,61		SLD/3	-2,88		SLD/3	-1,67
	SLD/4	-2,90		SLD/4	-2,54		SLD/4	-2,79		SLD/4	-1,63
	SLD/5	-2,85		SLD/5	-2,47		SLD/5	-2,72		SLD/5	-1,59
	SLD/6	-2,99		SLD/6	-2,61		SLD/6	-2,89		SLD/6	-1,67
	SLD/7	-2,91		SLD/7	-2,53		SLD/7	-2,80		SLD/7	-1,63
	SLD/8	-2,86		SLD/8	-2,47		SLD/8	-2,73		SLD/8	-1,60
	SLD/9	-2,99		SLD/9	-2,62		SLD/9	-2,89		SLD/9	-1,67
	SLD/10	-2,91		SLD/10	-2,54		SLD/10	-2,80		SLD/10	-1,63
	SLD/11	-2,86		SLD/11	-2,48		SLD/11	-2,74		SLD/11	-1,60
	SLD/12	-2,99		SLD/12	-2,62		SLD/12	-2,89		SLD/12	-1,67
	SLD/13	-2,90		SLD/13	-2,54		SLD/13	-2,80		SLD/13	-1,62
	SLD/14	-2,85		SLD/14	-2,49		SLD/14	-2,74		SLD/14	-1,59
X+	SLD/18	-1,94	X+	SLD/21	-1,65	X+	SLD/21	-1,78	X+	SLD/18	-1,09
X-	SLD/25	-2,00	X-	SLD/30	-1,72	X-	SLD/30	-1,92	X-	SLD/25	-1,10
Y+	SLD/41	-1,99	Y+	SLD/40	-1,63	Y+	SLD/40	-1,84	Y+	SLD/41	-1,11
Y-	SLD/43	-1,95	Y-	SLD/46	-1,73	Y-	SLD/46	-1,88	Y-	SLD/43	-1,09
342	SLD/1	-2,29	343	SLD/1	-2,31	344	SLD/1	-3,00	345	SLD/1	-2,73
	SLD/2	-2,24		SLD/2	-2,26		SLD/2	-2,91		SLD/2	-2,64
	SLD/3	-2,29		SLD/3	-2,31		SLD/3	-2,99		SLD/3	-2,72
	SLD/4	-2,24		SLD/4	-2,25		SLD/4	-2,91		SLD/4	-2,64
	SLD/5	-2,20		SLD/5	-2,21		SLD/5	-2,86		SLD/5	-2,59
	SLD/6	-2,30		SLD/6	-2,32		SLD/6	-3,00		SLD/6	-2,73
	SLD/7	-2,24		SLD/7	-2,26		SLD/7	-2,92		SLD/7	-2,64
	SLD/8	-2,20		SLD/8	-2,22		SLD/8	-2,87		SLD/8	-2,60
	SLD/9	-2,29		SLD/9	-2,32		SLD/9	-3,00		SLD/9	-2,73
	SLD/10	-2,24		SLD/10	-2,26		SLD/10	-2,91		SLD/10	-2,64
	SLD/11	-2,20		SLD/11	-2,22		SLD/11	-2,87		SLD/11	-2,60

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/12	-2,29		SLD/12	-2,31		SLD/12	-2,99		SLD/12	-2,72
	SLD/13	-2,24		SLD/13	-2,25		SLD/13	-2,91		SLD/13	-2,64
	SLD/14	-2,19		SLD/14	-2,21		SLD/14	-2,85		SLD/14	-2,59
X+	SLD/18	-1,51	X+	SLD/18	-1,49	X+	SLD/18	-1,95	X+	SLD/15	-1,76
X-	SLD/25	-1,53	X-	SLD/25	-1,57	X-	SLD/25	-2,01	X-	SLD/24	-1,81
Y+	SLD/41	-1,53	Y+	SLD/41	-1,57	Y+	SLD/41	-2,02	Y+	SLD/40	-1,81
Y-	SLD/43	-1,50	Y-	SLD/43	-1,50	Y-	SLD/43	-1,92	Y-	SLD/46	-1,76
346	SLD/1	-2,37	347	SLD/1	-1,84	348	SLD/1	-2,17	349	SLD/1	-2,71
	SLD/2	-2,30		SLD/2	-1,79		SLD/2	-2,11		SLD/2	-2,63
	SLD/3	-2,37		SLD/3	-1,84		SLD/3	-2,17		SLD/3	-2,71
	SLD/4	-2,30		SLD/4	-1,79		SLD/4	-2,11		SLD/4	-2,62
	SLD/5	-2,26		SLD/5	-1,75		SLD/5	-2,07		SLD/5	-2,57
	SLD/6	-2,38		SLD/6	-1,84		SLD/6	-2,18		SLD/6	-2,71
	SLD/7	-2,31		SLD/7	-1,80		SLD/7	-2,11		SLD/7	-2,63
	SLD/8	-2,27		SLD/8	-1,76		SLD/8	-2,08		SLD/8	-2,58
	SLD/9	-2,37		SLD/9	-1,84		SLD/9	-2,18		SLD/9	-2,72
	SLD/10	-2,30		SLD/10	-1,79		SLD/10	-2,11		SLD/10	-2,63
	SLD/11	-2,26		SLD/11	-1,76		SLD/11	-2,07		SLD/11	-2,58
	SLD/12	-2,36		SLD/12	-1,83		SLD/12	-2,17		SLD/12	-2,71
	SLD/13	-2,30		SLD/13	-1,79		SLD/13	-2,10		SLD/13	-2,63
	SLD/14	-2,25		SLD/14	-1,75		SLD/14	-2,06		SLD/14	-2,58
X+	SLD/18	-1,57	X+	SLD/18	-1,21	X+	SLD/15	-1,42	X+	SLD/21	-1,70
X-	SLD/25	-1,57	X-	SLD/25	-1,23	X-	SLD/24	-1,43	X-	SLD/30	-1,79
Y+	SLD/41	-1,62	Y+	SLD/41	-1,25	Y+	SLD/40	-1,46	Y+	SLD/40	-1,76
Y-	SLD/43	-1,48	Y-	SLD/43	-1,16	Y-	SLD/46	-1,37	Y-	SLD/46	-1,76
350	SLD/1	-2,95	351	SLD/1	-2,18	352	SLD/1	-2,25	353	SLD/1	-1,60
	SLD/2	-2,86		SLD/2	-2,11		SLD/2	-2,18		SLD/2	-1,55
	SLD/3	-2,94		SLD/3	-2,17		SLD/3	-2,24		SLD/3	-1,60
	SLD/4	-2,85		SLD/4	-2,11		SLD/4	-2,18		SLD/4	-1,55
	SLD/5	-2,78		SLD/5	-2,06		SLD/5	-2,12		SLD/5	-1,52
	SLD/6	-2,94		SLD/6	-2,18		SLD/6	-2,24		SLD/6	-1,61
	SLD/7	-2,85		SLD/7	-2,11		SLD/7	-2,18		SLD/7	-1,56
	SLD/8	-2,79		SLD/8	-2,07		SLD/8	-2,12		SLD/8	-1,53
	SLD/9	-2,95		SLD/9	-2,18		SLD/9	-2,25		SLD/9	-1,60
	SLD/10	-2,86		SLD/10	-2,11		SLD/10	-2,18		SLD/10	-1,55
	SLD/11	-2,80		SLD/11	-2,07		SLD/11	-2,13		SLD/11	-1,52
	SLD/12	-2,95		SLD/12	-2,18		SLD/12	-2,25		SLD/12	-1,60
	SLD/13	-2,86		SLD/13	-2,11		SLD/13	-2,18		SLD/13	-1,55
	SLD/14	-2,79		SLD/14	-2,06		SLD/14	-2,13		SLD/14	-1,51
X+	SLD/21	-1,78	X+	SLD/15	-1,38	X+	SLD/21	-1,38	X+	SLD/18	-1,04
X-	SLD/30	-1,97	X-	SLD/24	-1,42	X-	SLD/30	-1,48	X-	SLD/25	-1,04
Y+	SLD/40	-1,89	Y+	SLD/40	-1,41	Y+	SLD/40	-1,42	Y+	SLD/41	-1,08
Y-	SLD/46	-1,92	Y-	SLD/46	-1,40	Y-	SLD/46	-1,46	Y-	SLD/43	-0,98
354	SLD/1	-1,58	355	SLD/1	-1,76	356	SLD/1	-1,99	357	SLD/1	-2,18
	SLD/2	-1,52		SLD/2	-1,70		SLD/2	-1,94		SLD/2	-2,14
	SLD/3	-1,58		SLD/3	-1,76		SLD/3	-1,99		SLD/3	-2,18
	SLD/4	-1,52		SLD/4	-1,70		SLD/4	-1,94		SLD/4	-2,14
	SLD/5	-1,50		SLD/5	-1,68		SLD/5	-1,91		SLD/5	-2,09
	SLD/6	-1,58		SLD/6	-1,76		SLD/6	-1,99		SLD/6	-2,19
	SLD/7	-1,53		SLD/7	-1,71		SLD/7	-1,94		SLD/7	-2,14
	SLD/8	-1,51		SLD/8	-1,69		SLD/8	-1,91		SLD/8	-2,11
	SLD/9	-1,58		SLD/9	-1,76		SLD/9	-1,99		SLD/9	-2,19
	SLD/10	-1,52		SLD/10	-1,70		SLD/10	-1,94		SLD/10	-2,14
	SLD/11	-1,50		SLD/11	-1,68		SLD/11	-1,91		SLD/11	-2,11
	SLD/12	-1,57		SLD/12	-1,76		SLD/12	-1,99		SLD/12	-2,18
	SLD/13	-1,52		SLD/13	-1,70		SLD/13	-1,94		SLD/13	-2,13
	SLD/14	-1,49		SLD/14	-1,68		SLD/14	-1,90		SLD/14	-2,09
X+	SLD/18	-1,04	X+	SLD/18	-1,16	X+	SLD/15	-1,31	X+	SLD/15	-1,42
X-	SLD/25	-1,04	X-	SLD/25	-1,18	X-	SLD/24	-1,36	X-	SLD/24	-1,52
Y+	SLD/34	-1,08	Y+	SLD/41	-1,19	Y+	SLD/40	-1,36	Y+	SLD/40	-1,52
Y-	SLD/36	-0,97	Y-	SLD/43	-1,13	Y-	SLD/46	-1,31	Y-	SLD/46	-1,42
358	SLD/1	-2,11	359	SLD/1	-2,39	360	SLD/1	-2,71	361	SLD/1	-2,52
	SLD/2	-2,04		SLD/2	-2,30		SLD/2	-2,62		SLD/2	-2,44
	SLD/3	-2,11		SLD/3	-2,38		SLD/3	-2,71		SLD/3	-2,52
	SLD/4	-2,04		SLD/4	-2,30		SLD/4	-2,62		SLD/4	-2,44
	SLD/5	-2,00		SLD/5	-2,26		SLD/5	-2,56		SLD/5	-2,38
	SLD/6	-2,12		SLD/6	-2,39		SLD/6	-2,72		SLD/6	-2,53
	SLD/7	-2,05		SLD/7	-2,31		SLD/7	-2,63		SLD/7	-2,45
	SLD/8	-2,02		SLD/8	-2,27		SLD/8	-2,57		SLD/8	-2,40
	SLD/9	-2,11		SLD/9	-2,39		SLD/9	-2,72		SLD/9	-2,52
	SLD/10	-2,04		SLD/10	-2,31		SLD/10	-2,63		SLD/10	-2,44
	SLD/11	-2,01		SLD/11	-2,27		SLD/11	-2,57		SLD/11	-2,39
	SLD/12	-2,10		SLD/12	-2,38		SLD/12	-2,71		SLD/12	-2,51
	SLD/13	-2,03		SLD/13	-2,30		SLD/13	-2,62		SLD/13	-2,43
	SLD/14	-1,99		SLD/14	-2,26		SLD/14	-2,56		SLD/14	-2,37
X+	SLD/18	-1,37	X+	SLD/15	-1,51	X+	SLD/15	-1,67	X+	SLD/18	-1,60
X-	SLD/25	-1,40	X-	SLD/24	-1,59	X-	SLD/24	-1,81	X-	SLD/25	-1,65
Y+	SLD/41	-1,44	Y+	SLD/40	-1,59	Y+	SLD/40	-1,79	Y+	SLD/41	-1,68

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	Y- SLD/43	-1,30		Y- SLD/46	-1,51		Y- SLD/46	-1,70		Y- SLD/43	-1,55
362	SLD/1	-1,92	363	SLD/1	-2,43	364	SLD/1	-2,73	365	SLD/1	-2,44
	SLD/2	-1,85		SLD/2	-2,34		SLD/2	-2,65		SLD/2	-2,35
	SLD/3	-1,91		SLD/3	-2,43		SLD/3	-2,73		SLD/3	-2,43
	SLD/4	-1,85		SLD/4	-2,34		SLD/4	-2,64		SLD/4	-2,35
	SLD/5	-1,82		SLD/5	-2,31		SLD/5	-2,57		SLD/5	-2,30
	SLD/6	-1,92		SLD/6	-2,43		SLD/6	-2,74		SLD/6	-2,44
	SLD/7	-1,85		SLD/7	-2,35		SLD/7	-2,65		SLD/7	-2,35
	SLD/8	-1,83		SLD/8	-2,32		SLD/8	-2,59		SLD/8	-2,31
	SLD/9	-1,92		SLD/9	-2,43		SLD/9	-2,74		SLD/9	-2,44
	SLD/10	-1,85		SLD/10	-2,35		SLD/10	-2,65		SLD/10	-2,36
	SLD/11	-1,83		SLD/11	-2,32		SLD/11	-2,60		SLD/11	-2,32
	SLD/12	-1,91		SLD/12	-2,42		SLD/12	-2,73		SLD/12	-2,43
	SLD/13	-1,85		SLD/13	-2,34		SLD/13	-2,64		SLD/13	-2,35
	SLD/14	-1,82		SLD/14	-2,31		SLD/14	-2,58		SLD/14	-2,31
X+	SLD/18	-1,26	X+	SLD/15	-1,58	X+	SLD/15	-1,65	X+	SLD/15	-1,53
X-	SLD/25	-1,28	X-	SLD/24	-1,62	X-	SLD/24	-1,84	X-	SLD/24	-1,63
Y+	SLD/41	-1,29	Y+	SLD/40	-1,63	Y+	SLD/40	-1,79	Y+	SLD/40	-1,61
Y-	SLD/43	-1,23	Y-	SLD/46	-1,57	Y-	SLD/46	-1,75	Y-	SLD/46	-1,56
366	SLD/1	-1,82	367	SLD/1	-1,99	368	SLD/1	-2,46	369	SLD/1	-1,98
	SLD/2	-1,76		SLD/2	-1,93		SLD/2	-2,38		SLD/2	-1,92
	SLD/3	-1,81		SLD/3	-1,99		SLD/3	-2,46		SLD/3	-1,98
	SLD/4	-1,76		SLD/4	-1,92		SLD/4	-2,38		SLD/4	-1,92
	SLD/5	-1,71		SLD/5	-1,89		SLD/5	-2,35		SLD/5	-1,89
	SLD/6	-1,82		SLD/6	-2,00		SLD/6	-2,47		SLD/6	-1,98
	SLD/7	-1,76		SLD/7	-1,93		SLD/7	-2,38		SLD/7	-1,92
	SLD/8	-1,72		SLD/8	-1,89		SLD/8	-2,35		SLD/8	-1,89
	SLD/9	-1,82		SLD/9	-2,00		SLD/9	-2,47		SLD/9	-1,98
	SLD/10	-1,76		SLD/10	-1,93		SLD/10	-2,38		SLD/10	-1,92
	SLD/11	-1,72		SLD/11	-1,90		SLD/11	-2,35		SLD/11	-1,89
	SLD/12	-1,81		SLD/12	-1,99		SLD/12	-2,46		SLD/12	-1,98
	SLD/13	-1,76		SLD/13	-1,93		SLD/13	-2,38		SLD/13	-1,92
	SLD/14	-1,71		SLD/14	-1,89		SLD/14	-2,35		SLD/14	-1,89
X+	SLD/15	-1,11	X+	SLD/15	-1,26	X+	SLD/15	-1,60	X+	SLD/21	-1,29
X-	SLD/24	-1,20	X-	SLD/24	-1,31	X-	SLD/24	-1,64	X-	SLD/30	-1,31
Y+	SLD/40	-1,18	Y+	SLD/40	-1,30	Y+	SLD/40	-1,63	Y+	SLD/40	-1,29
Y-	SLD/46	-1,15	Y-	SLD/46	-1,28	Y-	SLD/46	-1,61	Y-	SLD/46	-1,31
370	SLD/1	-2,89	371	SLD/1	-2,77	372	SLD/1	-2,36	373	SLD/1	-3,19
	SLD/2	-2,80		SLD/2	-2,69		SLD/2	-2,29		SLD/2	-3,12
	SLD/3	-2,88		SLD/3	-2,77		SLD/3	-2,36		SLD/3	-3,19
	SLD/4	-2,80		SLD/4	-2,69		SLD/4	-2,29		SLD/4	-3,12
	SLD/5	-2,76		SLD/5	-2,65		SLD/5	-2,26		SLD/5	-3,06
	SLD/6	-2,89		SLD/6	-2,77		SLD/6	-2,36		SLD/6	-3,20
	SLD/7	-2,80		SLD/7	-2,69		SLD/7	-2,30		SLD/7	-3,13
	SLD/8	-2,76		SLD/8	-2,66		SLD/8	-2,26		SLD/8	-3,08
	SLD/9	-2,89		SLD/9	-2,77		SLD/9	-2,36		SLD/9	-3,20
	SLD/10	-2,80		SLD/10	-2,69		SLD/10	-2,30		SLD/10	-3,13
	SLD/11	-2,76		SLD/11	-2,65		SLD/11	-2,26		SLD/11	-3,07
	SLD/12	-2,88		SLD/12	-2,77		SLD/12	-2,36		SLD/12	-3,19
	SLD/13	-2,80		SLD/13	-2,68		SLD/13	-2,29		SLD/13	-3,11
	SLD/14	-2,76		SLD/14	-2,65		SLD/14	-2,25		SLD/14	-3,06
X+	SLD/18	-1,91	X+	SLD/15	-1,82	X+	SLD/15	-1,55	X+	SLD/15	-2,09
X-	SLD/25	-1,92	X-	SLD/24	-1,86	X-	SLD/24	-1,60	X-	SLD/24	-2,20
Y+	SLD/41	-1,92	Y+	SLD/40	-1,87	Y+	SLD/40	-1,60	Y+	SLD/40	-2,20
Y-	SLD/43	-1,89	Y-	SLD/46	-1,82	Y-	SLD/46	-1,55	Y-	SLD/46	-2,09
374	SLD/1	-3,17	375	SLD/1	-3,28	376	SLD/1	-2,49	377	SLD/1	-2,92
	SLD/2	-3,09		SLD/2	-3,20		SLD/2	-2,43		SLD/2	-2,86
	SLD/3	-3,17		SLD/3	-3,28		SLD/3	-2,49		SLD/3	-2,92
	SLD/4	-3,09		SLD/4	-3,20		SLD/4	-2,43		SLD/4	-2,86
	SLD/5	-3,04		SLD/5	-3,15		SLD/5	-2,39		SLD/5	-2,81
	SLD/6	-3,17		SLD/6	-3,28		SLD/6	-2,49		SLD/6	-2,92
	SLD/7	-3,09		SLD/7	-3,20		SLD/7	-2,43		SLD/7	-2,86
	SLD/8	-3,05		SLD/8	-3,15		SLD/8	-2,39		SLD/8	-2,81
	SLD/9	-3,17		SLD/9	-3,28		SLD/9	-2,49		SLD/9	-2,92
	SLD/10	-3,09		SLD/10	-3,20		SLD/10	-2,43		SLD/10	-2,86
	SLD/11	-3,04		SLD/11	-3,15		SLD/11	-2,39		SLD/11	-2,80
	SLD/12	-3,16		SLD/12	-3,27		SLD/12	-2,49		SLD/12	-2,92
	SLD/13	-3,09		SLD/13	-3,20		SLD/13	-2,43		SLD/13	-2,86
	SLD/14	-3,03		SLD/14	-3,14		SLD/14	-2,39		SLD/14	-2,80
X+	SLD/15	-2,09	X+	SLD/18	-2,19	X+	SLD/18	-1,66	X+	SLD/18	-1,96
X-	SLD/24	-2,15	X-	SLD/25	-2,19	X-	SLD/25	-1,64	X-	SLD/25	-1,93
Y+	SLD/40	-2,15	Y+	SLD/34	-2,21	Y+	SLD/34	-1,65	Y+	SLD/34	-1,98
Y-	SLD/46	-2,08	Y-	SLD/36	-2,14	Y-	SLD/36	-1,65	Y-	SLD/36	-1,91
378	SLD/1	-3,40	379	SLD/1	-2,32	380	SLD/1	-2,17	381	SLD/1	-2,78
	SLD/2	-3,32		SLD/2	-2,27		SLD/2	-2,11		SLD/2	-2,70
	SLD/3	-3,41		SLD/3	-2,33		SLD/3	-2,17		SLD/3	-2,79
	SLD/4	-3,33		SLD/4	-2,28		SLD/4	-2,11		SLD/4	-2,70

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/5	-3,27		SLD/5	-2,23		SLD/5	-2,08		SLD/5	-2,67
	SLD/6	-3,38		SLD/6	-2,31		SLD/6	-2,17		SLD/6	-2,78
	SLD/7	-3,30		SLD/7	-2,27		SLD/7	-2,11		SLD/7	-2,69
	SLD/8	-3,23		SLD/8	-2,21		SLD/8	-2,07		SLD/8	-2,65
	SLD/9	-3,39		SLD/9	-2,31		SLD/9	-2,16		SLD/9	-2,78
	SLD/10	-3,31		SLD/10	-2,27		SLD/10	-2,11		SLD/10	-2,69
	SLD/11	-3,24		SLD/11	-2,22		SLD/11	-2,07		SLD/11	-2,65
	SLD/12	-3,41		SLD/12	-2,33		SLD/12	-2,17		SLD/12	-2,79
	SLD/13	-3,33		SLD/13	-2,28		SLD/13	-2,11		SLD/13	-2,70
	SLD/14	-3,28		SLD/14	-2,23		SLD/14	-2,08		SLD/14	-2,67
X+	SLD/21	-2,41	X+	SLD/21	-1,62	X+	SLD/21	-1,49	X+	SLD/21	-1,93
X-	SLD/30	-2,19	X-	SLD/30	-1,49	X-	SLD/30	-1,40	X-	SLD/30	-1,80
Y+	SLD/31	-2,16	Y+	SLD/31	-1,50	Y+	SLD/31	-1,43	Y+	SLD/31	-1,81
Y-	SLD/37	-2,43	Y-	SLD/37	-1,62	Y-	SLD/37	-1,48	Y-	SLD/37	-1,92
382	SLD/1	-3,39	383	SLD/1	-2,64	384	SLD/1	-2,37	385	SLD/1	-2,30
	SLD/2	-3,32		SLD/2	-2,55		SLD/2	-2,29		SLD/2	-2,21
	SLD/3	-3,40		SLD/3	-2,64		SLD/3	-2,37		SLD/3	-2,30
	SLD/4	-3,32		SLD/4	-2,56		SLD/4	-2,29		SLD/4	-2,21
	SLD/5	-3,27		SLD/5	-2,53		SLD/5	-2,27		SLD/5	-2,19
	SLD/6	-3,37		SLD/6	-2,63		SLD/6	-2,37		SLD/6	-2,30
	SLD/7	-3,29		SLD/7	-2,55		SLD/7	-2,29		SLD/7	-2,21
	SLD/8	-3,22		SLD/8	-2,51		SLD/8	-2,26		SLD/8	-2,19
	SLD/9	-3,39		SLD/9	-2,63		SLD/9	-2,37		SLD/9	-2,29
	SLD/10	-3,31		SLD/10	-2,55		SLD/10	-2,28		SLD/10	-2,21
	SLD/11	-3,24		SLD/11	-2,52		SLD/11	-2,26		SLD/11	-2,18
	SLD/12	-3,42		SLD/12	-2,64		SLD/12	-2,37		SLD/12	-2,30
	SLD/13	-3,34		SLD/13	-2,56		SLD/13	-2,29		SLD/13	-2,21
	SLD/14	-3,29		SLD/14	-2,53		SLD/14	-2,27		SLD/14	-2,19
X+	SLD/21	-2,43	X+	SLD/21	-1,82	X+	SLD/21	-1,62	X+	SLD/21	-1,56
X-	SLD/30	-2,21	X-	SLD/30	-1,71	X-	SLD/30	-1,53	X-	SLD/30	-1,48
Y+	SLD/31	-2,08	Y+	SLD/31	-1,71	Y+	SLD/31	-1,56	Y+	SLD/31	-1,52
Y-	SLD/37	-2,51	Y-	SLD/37	-1,82	Y-	SLD/37	-1,60	Y-	SLD/37	-1,53
386	SLD/1	-1,84	387	SLD/1	-2,13	388	SLD/1	-2,39	389	SLD/1	-2,08
	SLD/2	-1,78		SLD/2	-2,07		SLD/2	-2,31		SLD/2	-2,02
	SLD/3	-1,84		SLD/3	-2,14		SLD/3	-2,40		SLD/3	-2,08
	SLD/4	-1,78		SLD/4	-2,07		SLD/4	-2,32		SLD/4	-2,02
	SLD/5	-1,76		SLD/5	-2,04		SLD/5	-2,29		SLD/5	-1,99
	SLD/6	-1,84		SLD/6	-2,13		SLD/6	-2,39		SLD/6	-2,07
	SLD/7	-1,78		SLD/7	-2,06		SLD/7	-2,31		SLD/7	-2,01
	SLD/8	-1,75		SLD/8	-2,03		SLD/8	-2,28		SLD/8	-1,97
	SLD/9	-1,84		SLD/9	-2,13		SLD/9	-2,39		SLD/9	-2,07
	SLD/10	-1,78		SLD/10	-2,06		SLD/10	-2,30		SLD/10	-2,01
	SLD/11	-1,75		SLD/11	-2,03		SLD/11	-2,27		SLD/11	-1,97
	SLD/12	-1,84		SLD/12	-2,14		SLD/12	-2,40		SLD/12	-2,08
	SLD/13	-1,78		SLD/13	-2,07		SLD/13	-2,31		SLD/13	-2,02
	SLD/14	-1,76		SLD/14	-2,04		SLD/14	-2,29		SLD/14	-1,99
X+	SLD/21	-1,25	X+	SLD/21	-1,46	X+	SLD/21	-1,65	X+	SLD/21	-1,44
X-	SLD/30	-1,19	X-	SLD/30	-1,38	X-	SLD/30	-1,51	X-	SLD/30	-1,31
Y+	SLD/31	-1,21	Y+	SLD/31	-1,37	Y+	SLD/31	-1,57	Y+	SLD/31	-1,32
Y-	SLD/37	-1,25	Y-	SLD/37	-1,47	Y-	SLD/37	-1,63	Y-	SLD/37	-1,44
390	SLD/1	-2,25	391	SLD/1	-2,32	392	SLD/1	-2,14	393	SLD/1	-2,71
	SLD/2	-2,18		SLD/2	-2,23		SLD/2	-2,07		SLD/2	-2,62
	SLD/3	-2,26		SLD/3	-2,32		SLD/3	-2,14		SLD/3	-2,71
	SLD/4	-2,19		SLD/4	-2,24		SLD/4	-2,07		SLD/4	-2,63
	SLD/5	-2,16		SLD/5	-2,21		SLD/5	-2,04		SLD/5	-2,59
	SLD/6	-2,25		SLD/6	-2,32		SLD/6	-2,14		SLD/6	-2,70
	SLD/7	-2,18		SLD/7	-2,23		SLD/7	-2,07		SLD/7	-2,62
	SLD/8	-2,14		SLD/8	-2,21		SLD/8	-2,03		SLD/8	-2,58
	SLD/9	-2,24		SLD/9	-2,31		SLD/9	-2,13		SLD/9	-2,70
	SLD/10	-2,17		SLD/10	-2,23		SLD/10	-2,06		SLD/10	-2,62
	SLD/11	-2,13		SLD/11	-2,20		SLD/11	-2,02		SLD/11	-2,58
	SLD/12	-2,25		SLD/12	-2,32		SLD/12	-2,14		SLD/12	-2,71
	SLD/13	-2,19		SLD/13	-2,23		SLD/13	-2,07		SLD/13	-2,63
	SLD/14	-2,15		SLD/14	-2,21		SLD/14	-2,03		SLD/14	-2,59
X+	SLD/21	-1,60	X+	SLD/21	-1,58	X+	SLD/21	-1,47	X+	SLD/21	-1,85
X-	SLD/30	-1,37	X-	SLD/30	-1,46	X-	SLD/30	-1,31	X-	SLD/30	-1,76
Y+	SLD/31	-1,48	Y+	SLD/31	-1,53	Y+	SLD/31	-1,41	Y+	SLD/31	-1,77
Y-	SLD/37	-1,55	Y-	SLD/37	-1,54	Y-	SLD/37	-1,42	Y-	SLD/37	-1,85
394	SLD/1	-3,46	395	SLD/1	-3,25	396	SLD/1	-2,34	397	SLD/1	-1,99
	SLD/2	-3,38		SLD/2	-3,18		SLD/2	-2,28		SLD/2	-1,92
	SLD/3	-3,47		SLD/3	-3,25		SLD/3	-2,35		SLD/3	-1,99
	SLD/4	-3,39		SLD/4	-3,18		SLD/4	-2,28		SLD/4	-1,93
	SLD/5	-3,33		SLD/5	-3,12		SLD/5	-2,25		SLD/5	-1,90
	SLD/6	-3,44		SLD/6	-3,22		SLD/6	-2,35		SLD/6	-1,99
	SLD/7	-3,36		SLD/7	-3,15		SLD/7	-2,28		SLD/7	-1,93
	SLD/8	-3,28		SLD/8	-3,08		SLD/8	-2,25		SLD/8	-1,90
	SLD/9	-3,46		SLD/9	-3,24		SLD/9	-2,34		SLD/9	-1,99
	SLD/10	-3,38		SLD/10	-3,17		SLD/10	-2,28		SLD/10	-1,92

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/11	-3,31		SLD/11	-3,11		SLD/11	-2,24		SLD/11	-1,90
	SLD/12	-3,49		SLD/12	-3,27		SLD/12	-2,34		SLD/12	-1,99
	SLD/13	-3,41		SLD/13	-3,20		SLD/13	-2,28		SLD/13	-1,92
	SLD/14	-3,36		SLD/14	-3,15		SLD/14	-2,24		SLD/14	-1,89
X+	SLD/21	-2,44	X+	SLD/21	-2,26	X+	SLD/15	-1,59	X+	SLD/15	-1,33
X-	SLD/30	-2,30	X-	SLD/30	-2,17	X-	SLD/24	-1,54	X-	SLD/24	-1,29
Y+	SLD/31	-2,06	Y+	SLD/31	-1,94	Y+	SLD/31	-1,59	Y+	SLD/31	-1,33
Y-	SLD/37	-2,57	Y-	SLD/37	-2,39	Y-	SLD/37	-1,54	Y-	SLD/37	-1,29
398	SLD/1	-2,33	399	SLD/1	-2,35	400	SLD/1	-2,73	401	SLD/1	-2,01
	SLD/2	-2,24		SLD/2	-2,27		SLD/2	-2,64		SLD/2	-1,94
	SLD/3	-2,33		SLD/3	-2,35		SLD/3	-2,73		SLD/3	-2,02
	SLD/4	-2,24		SLD/4	-2,27		SLD/4	-2,64		SLD/4	-1,95
	SLD/5	-2,22		SLD/5	-2,24		SLD/5	-2,59		SLD/5	-1,91
	SLD/6	-2,33		SLD/6	-2,35		SLD/6	-2,73		SLD/6	-2,01
	SLD/7	-2,24		SLD/7	-2,27		SLD/7	-2,64		SLD/7	-1,94
	SLD/8	-2,22		SLD/8	-2,23		SLD/8	-2,58		SLD/8	-1,90
	SLD/9	-2,32		SLD/9	-2,35		SLD/9	-2,72		SLD/9	-2,01
	SLD/10	-2,24		SLD/10	-2,26		SLD/10	-2,63		SLD/10	-1,94
	SLD/11	-2,21		SLD/11	-2,23		SLD/11	-2,58		SLD/11	-1,91
	SLD/12	-2,33		SLD/12	-2,35		SLD/12	-2,73		SLD/12	-2,02
	SLD/13	-2,24		SLD/13	-2,27		SLD/13	-2,64		SLD/13	-1,95
	SLD/14	-2,21		SLD/14	-2,23		SLD/14	-2,59		SLD/14	-1,92
X+	SLD/15	-1,56	X+	SLD/21	-1,56	X+	SLD/21	-1,80	X+	SLD/20	-1,32
X-	SLD/24	-1,50	X-	SLD/30	-1,49	X-	SLD/30	-1,71	X-	SLD/27	-1,29
Y+	SLD/31	-1,55	Y+	SLD/31	-1,52	Y+	SLD/31	-1,76	Y+	SLD/34	-1,26
Y-	SLD/37	-1,52	Y-	SLD/37	-1,55	Y-	SLD/37	-1,78	Y-	SLD/36	-1,34
402	SLD/1	-1,67	403	SLD/1	-2,45	404	SLD/1	-3,03	405	SLD/1	-3,05
	SLD/2	-1,62		SLD/2	-2,39		SLD/2	-2,95		SLD/2	-2,96
	SLD/3	-1,67		SLD/3	-2,46		SLD/3	-3,04		SLD/3	-3,06
	SLD/4	-1,62		SLD/4	-2,40		SLD/4	-2,96		SLD/4	-2,97
	SLD/5	-1,58		SLD/5	-2,36		SLD/5	-2,91		SLD/5	-2,93
	SLD/6	-1,67		SLD/6	-2,45		SLD/6	-3,04		SLD/6	-3,05
	SLD/7	-1,61		SLD/7	-2,39		SLD/7	-2,95		SLD/7	-2,96
	SLD/8	-1,58		SLD/8	-2,35		SLD/8	-2,90		SLD/8	-2,91
	SLD/9	-1,67		SLD/9	-2,45		SLD/9	-3,02		SLD/9	-3,04
	SLD/10	-1,62		SLD/10	-2,39		SLD/10	-2,94		SLD/10	-2,95
	SLD/11	-1,58		SLD/11	-2,34		SLD/11	-2,89		SLD/11	-2,89
	SLD/12	-1,67		SLD/12	-2,45		SLD/12	-3,03		SLD/12	-3,05
	SLD/13	-1,62		SLD/13	-2,39		SLD/13	-2,95		SLD/13	-2,96
	SLD/14	-1,59		SLD/14	-2,35		SLD/14	-2,89		SLD/14	-2,91
X+	SLD/20	-1,08	X+	SLD/15	-1,68	X+	SLD/15	-2,11	X+	SLD/15	-2,14
X-	SLD/27	-1,06	X-	SLD/24	-1,56	X-	SLD/24	-1,90	X-	SLD/24	-1,87
Y+	SLD/34	-1,03	Y+	SLD/31	-1,64	Y+	SLD/31	-2,06	Y+	SLD/31	-2,05
Y-	SLD/36	-1,09	Y-	SLD/37	-1,63	Y-	SLD/37	-2,00	Y-	SLD/37	-2,04
406	SLD/1	-2,59	407	SLD/1	-3,14	408	SLD/1	-2,85	409	SLD/1	-2,53
	SLD/2	-2,53		SLD/2	-3,05		SLD/2	-2,77		SLD/2	-2,46
	SLD/3	-2,60		SLD/3	-3,15		SLD/3	-2,86		SLD/3	-2,53
	SLD/4	-2,53		SLD/4	-3,06		SLD/4	-2,77		SLD/4	-2,47
	SLD/5	-2,49		SLD/5	-3,01		SLD/5	-2,73		SLD/5	-2,43
	SLD/6	-2,59		SLD/6	-3,15		SLD/6	-2,86		SLD/6	-2,53
	SLD/7	-2,53		SLD/7	-3,05		SLD/7	-2,77		SLD/7	-2,46
	SLD/8	-2,48		SLD/8	-3,00		SLD/8	-2,73		SLD/8	-2,42
	SLD/9	-2,59		SLD/9	-3,13		SLD/9	-2,84		SLD/9	-2,52
	SLD/10	-2,52		SLD/10	-3,04		SLD/10	-2,76		SLD/10	-2,45
	SLD/11	-2,47		SLD/11	-2,98		SLD/11	-2,71		SLD/11	-2,40
	SLD/12	-2,59		SLD/12	-3,14		SLD/12	-2,84		SLD/12	-2,52
	SLD/13	-2,53		SLD/13	-3,04		SLD/13	-2,76		SLD/13	-2,45
	SLD/14	-2,48		SLD/14	-2,99		SLD/14	-2,71		SLD/14	-2,41
X+	SLD/21	-1,78	X+	SLD/15	-2,18	X+	SLD/15	-1,97	X+	SLD/15	-1,78
X-	SLD/30	-1,64	X-	SLD/24	-1,96	X-	SLD/24	-1,82	X-	SLD/24	-1,57
Y+	SLD/31	-1,72	Y+	SLD/31	-2,13	Y+	SLD/31	-1,96	Y+	SLD/31	-1,74
Y-	SLD/37	-1,74	Y-	SLD/37	-2,05	Y-	SLD/37	-1,84	Y-	SLD/37	-1,65
410	SLD/1	-2,41	411	SLD/1	-2,02	412	SLD/1	-1,72	413	SLD/1	-1,98
	SLD/2	-2,34		SLD/2	-1,97		SLD/2	-1,67		SLD/2	-1,93
	SLD/3	-2,41		SLD/3	-2,02		SLD/3	-1,72		SLD/3	-1,99
	SLD/4	-2,34		SLD/4	-1,97		SLD/4	-1,68		SLD/4	-1,94
	SLD/5	-2,31		SLD/5	-1,94		SLD/5	-1,65		SLD/5	-1,91
	SLD/6	-2,41		SLD/6	-2,02		SLD/6	-1,72		SLD/6	-1,99
	SLD/7	-2,35		SLD/7	-1,97		SLD/7	-1,68		SLD/7	-1,93
	SLD/8	-2,31		SLD/8	-1,93		SLD/8	-1,65		SLD/8	-1,91
	SLD/9	-2,40		SLD/9	-2,01		SLD/9	-1,71		SLD/9	-1,98
	SLD/10	-2,33		SLD/10	-1,96		SLD/10	-1,67		SLD/10	-1,92
	SLD/11	-2,29		SLD/11	-1,92		SLD/11	-1,63		SLD/11	-1,88
	SLD/12	-2,40		SLD/12	-2,01		SLD/12	-1,71		SLD/12	-1,98
	SLD/13	-2,33		SLD/13	-1,96		SLD/13	-1,67		SLD/13	-1,92
	SLD/14	-2,29		SLD/14	-1,92		SLD/14	-1,63		SLD/14	-1,89
X+	SLD/15	-1,67	X+	SLD/15	-1,39	X+	SLD/15	-1,19	X+	SLD/15	-1,41
X-	SLD/24	-1,55	X-	SLD/24	-1,27	X-	SLD/24	-1,08	X-	SLD/24	-1,23

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	Y+ SLD/31	-1,67		Y+ SLD/31	-1,36		Y+ SLD/31	-1,19		Y+ SLD/31	-1,38
	Y- SLD/37	-1,54		Y- SLD/37	-1,33		Y- SLD/37	-1,09		Y- SLD/37	-1,28
414	SLD/1	-2,65	415	SLD/1	-1,99	416	SLD/1	-3,20	417	SLD/1	-2,94
	SLD/2	-2,57		SLD/2	-1,94		SLD/2	-3,10		SLD/2	-2,85
	SLD/3	-2,65		SLD/3	-2,00		SLD/3	-3,20		SLD/3	-2,94
	SLD/4	-2,57		SLD/4	-1,94		SLD/4	-3,11		SLD/4	-2,85
	SLD/5	-2,54		SLD/5	-1,91		SLD/5	-3,05		SLD/5	-2,81
	SLD/6	-2,66		SLD/6	-2,00		SLD/6	-3,21		SLD/6	-2,95
	SLD/7	-2,57		SLD/7	-1,94		SLD/7	-3,12		SLD/7	-2,87
	SLD/8	-2,54		SLD/8	-1,91		SLD/8	-3,06		SLD/8	-2,82
	SLD/9	-2,64		SLD/9	-1,99		SLD/9	-3,19		SLD/9	-2,93
	SLD/10	-2,56		SLD/10	-1,93		SLD/10	-3,10		SLD/10	-2,85
	SLD/11	-2,52		SLD/11	-1,90		SLD/11	-3,03		SLD/11	-2,80
	SLD/12	-2,64		SLD/12	-1,99		SLD/12	-3,19		SLD/12	-2,92
	SLD/13	-2,56		SLD/13	-1,93		SLD/13	-3,09		SLD/13	-2,84
	SLD/14	-2,52		SLD/14	-1,89		SLD/14	-3,02		SLD/14	-2,78
X+	SLD/15	-1,83	X+	SLD/15	-1,36	X+	SLD/15	-2,16	X+	SLD/15	-2,00
X-	SLD/24	-1,69	X-	SLD/24	-1,29	X-	SLD/24	-2,05	X-	SLD/24	-1,93
Y+	SLD/31	-1,83	Y+	SLD/31	-1,39	Y+	SLD/31	-2,20	Y+	SLD/31	-2,06
Y-	SLD/37	-1,69	Y-	SLD/37	-1,24	Y-	SLD/37	-1,98	Y-	SLD/37	-1,81
418	SLD/1	-2,62	419	SLD/1	-2,88	420	SLD/1	-2,54	421	SLD/1	-2,58
	SLD/2	-2,55		SLD/2	-2,80		SLD/2	-2,48		SLD/2	-2,52
	SLD/3	-2,62		SLD/3	-2,88		SLD/3	-2,54		SLD/3	-2,58
	SLD/4	-2,55		SLD/4	-2,80		SLD/4	-2,48		SLD/4	-2,52
	SLD/5	-2,50		SLD/5	-2,74		SLD/5	-2,43		SLD/5	-2,47
	SLD/6	-2,63		SLD/6	-2,90		SLD/6	-2,55		SLD/6	-2,59
	SLD/7	-2,56		SLD/7	-2,82		SLD/7	-2,49		SLD/7	-2,53
	SLD/8	-2,52		SLD/8	-2,77		SLD/8	-2,45		SLD/8	-2,49
	SLD/9	-2,61		SLD/9	-2,88		SLD/9	-2,54		SLD/9	-2,58
	SLD/10	-2,55		SLD/10	-2,80		SLD/10	-2,48		SLD/10	-2,52
	SLD/11	-2,49		SLD/11	-2,73		SLD/11	-2,44		SLD/11	-2,47
	SLD/12	-2,60		SLD/12	-2,86		SLD/12	-2,53		SLD/12	-2,56
	SLD/13	-2,53		SLD/13	-2,78		SLD/13	-2,47		SLD/13	-2,50
	SLD/14	-2,47		SLD/14	-2,70		SLD/14	-2,42		SLD/14	-2,45
X+	SLD/15	-1,77	X+	SLD/15	-1,94	X+	SLD/15	-1,71	X+	SLD/15	-1,73
X-	SLD/24	-1,75	X-	SLD/24	-1,88	X-	SLD/24	-1,72	X-	SLD/24	-1,75
Y+	SLD/31	-1,88	Y+	SLD/31	-2,05	Y+	SLD/40	-1,78	Y+	SLD/40	-1,83
Y-	SLD/37	-1,55	Y-	SLD/37	-1,67	Y-	SLD/46	-1,58	Y-	SLD/46	-1,59
422	SLD/1	-1,93	423	SLD/1	-2,11	424	SLD/1	-2,98	425	SLD/1	-2,63
	SLD/2	-1,87		SLD/2	-2,05		SLD/2	-2,90		SLD/2	-2,55
	SLD/3	-1,93		SLD/3	-2,11		SLD/3	-2,98		SLD/3	-2,63
	SLD/4	-1,88		SLD/4	-2,05		SLD/4	-2,90		SLD/4	-2,55
	SLD/5	-1,85		SLD/5	-2,02		SLD/5	-2,86		SLD/5	-2,52
	SLD/6	-1,93		SLD/6	-2,12		SLD/6	-2,99		SLD/6	-2,64
	SLD/7	-1,88		SLD/7	-2,06		SLD/7	-2,91		SLD/7	-2,55
	SLD/8	-1,85		SLD/8	-2,04		SLD/8	-2,87		SLD/8	-2,53
	SLD/9	-1,92		SLD/9	-2,11		SLD/9	-2,98		SLD/9	-2,63
	SLD/10	-1,87		SLD/10	-2,06		SLD/10	-2,90		SLD/10	-2,54
	SLD/11	-1,84		SLD/11	-2,02		SLD/11	-2,86		SLD/11	-2,51
	SLD/12	-1,92		SLD/12	-2,10		SLD/12	-2,98		SLD/12	-2,62
	SLD/13	-1,87		SLD/13	-2,05		SLD/13	-2,89		SLD/13	-2,54
	SLD/14	-1,84		SLD/14	-2,01		SLD/14	-2,85		SLD/14	-2,51
X+	SLD/15	-1,33	X+	SLD/15	-1,41	X+	SLD/15	-2,01	X+	SLD/15	-1,79
X-	SLD/24	-1,25	X-	SLD/24	-1,44	X-	SLD/24	-2,02	X-	SLD/24	-1,72
Y+	SLD/31	-1,34	Y+	SLD/40	-1,48	Y+	SLD/40	-2,06	Y+	SLD/31	-1,81
Y-	SLD/37	-1,24	Y-	SLD/46	-1,34	Y-	SLD/46	-1,93	Y-	SLD/37	-1,70
426	SLD/1	-3,57	427	SLD/1	-2,63	428	SLD/1	-2,03	429	SLD/1	-2,64
	SLD/2	-3,49		SLD/2	-2,57		SLD/2	-1,98		SLD/2	-2,56
	SLD/3	-3,57		SLD/3	-2,63		SLD/3	-2,04		SLD/3	-2,64
	SLD/4	-3,49		SLD/4	-2,58		SLD/4	-1,98		SLD/4	-2,56
	SLD/5	-3,43		SLD/5	-2,53		SLD/5	-1,95		SLD/5	-2,53
	SLD/6	-3,53		SLD/6	-2,61		SLD/6	-2,04		SLD/6	-2,64
	SLD/7	-3,46		SLD/7	-2,56		SLD/7	-1,98		SLD/7	-2,56
	SLD/8	-3,38		SLD/8	-2,49		SLD/8	-1,95		SLD/8	-2,52
	SLD/9	-3,56		SLD/9	-2,62		SLD/9	-2,03		SLD/9	-2,64
	SLD/10	-3,49		SLD/10	-2,57		SLD/10	-1,98		SLD/10	-2,56
	SLD/11	-3,43		SLD/11	-2,52		SLD/11	-1,95		SLD/11	-2,53
	SLD/12	-3,60		SLD/12	-2,64		SLD/12	-2,03		SLD/12	-2,64
	SLD/13	-3,52		SLD/13	-2,59		SLD/13	-1,97		SLD/13	-2,56
	SLD/14	-3,48		SLD/14	-2,55		SLD/14	-1,94		SLD/14	-2,53
X+	SLD/20	-2,51	X+	SLD/20	-1,83	X+	SLD/15	-1,38	X+	SLD/21	-1,77
X-	SLD/27	-2,45	X-	SLD/27	-1,76	X-	SLD/24	-1,35	X-	SLD/30	-1,75
Y+	SLD/34	-2,10	Y+	SLD/34	-1,59	Y+	SLD/31	-1,39	Y+	SLD/31	-1,74
Y-	SLD/36	-2,70	Y-	SLD/36	-1,92	Y-	SLD/37	-1,32	Y-	SLD/37	-1,77
430	SLD/1	-2,51	431	SLD/1	-3,50	432	SLD/1	-2,20	433	SLD/1	-1,71
	SLD/2	-2,43		SLD/2	-3,42		SLD/2	-2,11		SLD/2	-1,65
	SLD/3	-2,51		SLD/3	-3,50		SLD/3	-2,20		SLD/3	-1,71

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/4	-2,43		SLD/4	-3,42		SLD/4	-2,11		SLD/4	-1,65
	SLD/5	-2,41		SLD/5	-3,38		SLD/5	-2,09		SLD/5	-1,63
	SLD/6	-2,50		SLD/6	-3,46		SLD/6	-2,20		SLD/6	-1,71
	SLD/7	-2,42		SLD/7	-3,38		SLD/7	-2,12		SLD/7	-1,65
	SLD/8	-2,39		SLD/8	-3,31		SLD/8	-2,10		SLD/8	-1,63
	SLD/9	-2,51		SLD/9	-3,50		SLD/9	-2,20		SLD/9	-1,71
	SLD/10	-2,43		SLD/10	-3,42		SLD/10	-2,11		SLD/10	-1,65
	SLD/11	-2,41		SLD/11	-3,37		SLD/11	-2,09		SLD/11	-1,62
	SLD/12	-2,52		SLD/12	-3,54		SLD/12	-2,19		SLD/12	-1,70
	SLD/13	-2,43		SLD/13	-3,46		SLD/13	-2,11		SLD/13	-1,64
	SLD/14	-2,42		SLD/14	-3,44		SLD/14	-2,08		SLD/14	-1,62
X+	SLD/20	-1,70	X+	SLD/20	-2,50	X+	SLD/15	-1,46	X+	SLD/15	-1,14
X-	SLD/27	-1,70	X-	SLD/27	-2,47	X-	SLD/24	-1,45	X-	SLD/24	-1,12
Y+	SLD/41	-1,61	Y+	SLD/34	-2,02	Y+	SLD/31	-1,49	Y+	SLD/31	-1,15
Y-	SLD/43	-1,75	Y-	SLD/36	-2,75	Y-	SLD/37	-1,39	Y-	SLD/37	-1,09
434	SLD/1	-1,71	435	SLD/1	-2,18	436	SLD/1	-1,52	437	SLD/1	-2,22
	SLD/2	-1,65		SLD/2	-2,09		SLD/2	-1,47		SLD/2	-2,14
	SLD/3	-1,72		SLD/3	-2,18		SLD/3	-1,52		SLD/3	-2,22
	SLD/4	-1,66		SLD/4	-2,09		SLD/4	-1,47		SLD/4	-2,14
	SLD/5	-1,63		SLD/5	-2,07		SLD/5	-1,44		SLD/5	-2,10
	SLD/6	-1,71		SLD/6	-2,18		SLD/6	-1,52		SLD/6	-2,22
	SLD/7	-1,65		SLD/7	-2,10		SLD/7	-1,47		SLD/7	-2,14
	SLD/8	-1,62		SLD/8	-2,07		SLD/8	-1,43		SLD/8	-2,10
	SLD/9	-1,71		SLD/9	-2,18		SLD/9	-1,52		SLD/9	-2,22
	SLD/10	-1,65		SLD/10	-2,09		SLD/10	-1,47		SLD/10	-2,14
	SLD/11	-1,62		SLD/11	-2,06		SLD/11	-1,44		SLD/11	-2,10
	SLD/12	-1,72		SLD/12	-2,18		SLD/12	-1,53		SLD/12	-2,22
	SLD/13	-1,66		SLD/13	-2,09		SLD/13	-1,48		SLD/13	-2,14
	SLD/14	-1,63		SLD/14	-2,06		SLD/14	-1,44		SLD/14	-2,10
X+	SLD/20	-1,12	X+	SLD/15	-1,42	X+	SLD/20	-0,99	X+	SLD/15	-1,44
X-	SLD/27	-1,09	X-	SLD/24	-1,40	X-	SLD/27	-0,95	X-	SLD/24	-1,39
Y+	SLD/34	-1,07	Y+	SLD/31	-1,42	Y+	SLD/34	-0,94	Y+	SLD/31	-1,43
Y-	SLD/36	-1,13	Y-	SLD/37	-1,40	Y-	SLD/36	-1,00	Y-	SLD/37	-1,42
438	SLD/1	-2,08	439	SLD/1	-2,10	440	SLD/1	-2,67	441	SLD/1	-2,17
	SLD/2	-2,00		SLD/2	-2,02		SLD/2	-2,59		SLD/2	-2,09
	SLD/3	-2,08		SLD/3	-2,10		SLD/3	-2,68		SLD/3	-2,17
	SLD/4	-2,00		SLD/4	-2,02		SLD/4	-2,59		SLD/4	-2,09
	SLD/5	-1,98		SLD/5	-2,00		SLD/5	-2,57		SLD/5	-2,08
	SLD/6	-2,09		SLD/6	-2,11		SLD/6	-2,66		SLD/6	-2,18
	SLD/7	-2,00		SLD/7	-2,02		SLD/7	-2,57		SLD/7	-2,09
	SLD/8	-1,99		SLD/8	-2,01		SLD/8	-2,54		SLD/8	-2,08
	SLD/9	-2,08		SLD/9	-2,10		SLD/9	-2,67		SLD/9	-2,17
	SLD/10	-2,00		SLD/10	-2,02		SLD/10	-2,59		SLD/10	-2,09
	SLD/11	-1,99		SLD/11	-2,00		SLD/11	-2,57		SLD/11	-2,08
	SLD/12	-2,08		SLD/12	-2,10		SLD/12	-2,69		SLD/12	-2,17
	SLD/13	-1,99		SLD/13	-2,01		SLD/13	-2,61		SLD/13	-2,08
	SLD/14	-1,98		SLD/14	-1,99		SLD/14	-2,59		SLD/14	-2,07
X+	SLD/15	-1,39	X+	SLD/15	-1,39	X+	SLD/20	-1,86	X+	SLD/15	-1,46
X-	SLD/24	-1,39	X-	SLD/24	-1,39	X-	SLD/27	-1,84	X-	SLD/24	-1,46
Y+	SLD/40	-1,42	Y+	SLD/40	-1,43	Y+	SLD/34	-1,67	Y+	SLD/40	-1,48
Y-	SLD/46	-1,33	Y-	SLD/46	-1,32	Y-	SLD/36	-1,95	Y-	SLD/46	-1,42
442	SLD/1	-2,11	443	SLD/1	-2,25	444	SLD/1	-3,76	445	SLD/1	-3,28
	SLD/2	-2,03		SLD/2	-2,16		SLD/2	-3,68		SLD/2	-3,19
	SLD/3	-2,11		SLD/3	-2,25		SLD/3	-3,76		SLD/3	-3,28
	SLD/4	-2,03		SLD/4	-2,16		SLD/4	-3,69		SLD/4	-3,20
	SLD/5	-2,00		SLD/5	-2,14		SLD/5	-3,64		SLD/5	-3,17
	SLD/6	-2,11		SLD/6	-2,25		SLD/6	-3,71		SLD/6	-3,25
	SLD/7	-2,04		SLD/7	-2,17		SLD/7	-3,63		SLD/7	-3,17
	SLD/8	-2,01		SLD/8	-2,16		SLD/8	-3,54		SLD/8	-3,12
	SLD/9	-2,11		SLD/9	-2,25		SLD/9	-3,76		SLD/9	-3,28
	SLD/10	-2,03		SLD/10	-2,16		SLD/10	-3,68		SLD/10	-3,19
	SLD/11	-2,00		SLD/11	-2,14		SLD/11	-3,63		SLD/11	-3,15
	SLD/12	-2,11		SLD/12	-2,24		SLD/12	-3,82		SLD/12	-3,31
	SLD/13	-2,03		SLD/13	-2,15		SLD/13	-3,74		SLD/13	-3,22
	SLD/14	-2,00		SLD/14	-2,13		SLD/14	-3,72		SLD/14	-3,20
X+	SLD/15	-1,39	X+	SLD/15	-1,51	X+	SLD/20	-2,75	X+	SLD/20	-2,36
X-	SLD/24	-1,38	X-	SLD/24	-1,51	X-	SLD/27	-2,71	X-	SLD/27	-2,25
Y+	SLD/31	-1,41	Y+	SLD/40	-1,56	Y+	SLD/34	-2,10	Y+	SLD/34	-2,00
Y-	SLD/37	-1,33	Y-	SLD/46	-1,41	Y-	SLD/36	-3,09	Y-	SLD/36	-2,50
446	SLD/1	-4,80	447	SLD/1	-2,57	448	SLD/1	-2,46	449	SLD/1	-2,73
	SLD/2	-4,71		SLD/2	-2,48		SLD/2	-2,39		SLD/2	-2,64
	SLD/3	-4,80		SLD/3	-2,57		SLD/3	-2,46		SLD/3	-2,73
	SLD/4	-4,72		SLD/4	-2,48		SLD/4	-2,39		SLD/4	-2,64
	SLD/5	-4,65		SLD/5	-2,46		SLD/5	-2,35		SLD/5	-2,61
	SLD/6	-4,71		SLD/6	-2,57		SLD/6	-2,47		SLD/6	-2,74
	SLD/7	-4,63		SLD/7	-2,48		SLD/7	-2,39		SLD/7	-2,65
	SLD/8	-4,50		SLD/8	-2,46		SLD/8	-2,36		SLD/8	-2,63
	SLD/9	-4,79		SLD/9	-2,57		SLD/9	-2,46		SLD/9	-2,73

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/10	-4,71		SLD/10	-2,47		SLD/10	-2,38		SLD/10	-2,64
	SLD/11	-4,63		SLD/11	-2,46		SLD/11	-2,35		SLD/11	-2,61
	SLD/12	-4,88		SLD/12	-2,57		SLD/12	-2,45		SLD/12	-2,72
	SLD/13	-4,80		SLD/13	-2,48		SLD/13	-2,38		SLD/13	-2,63
	SLD/14	-4,78		SLD/14	-2,46		SLD/14	-2,34		SLD/14	-2,60
X+	SLD/20	-3,64	X+	SLD/15	-1,74	X+	SLD/15	-1,65	X+	SLD/15	-1,86
X-	SLD/27	-3,43	X-	SLD/24	-1,70	X-	SLD/24	-1,65	X-	SLD/24	-1,84
Y+	SLD/34	-2,59	Y+	SLD/31	-1,73	Y+	SLD/31	-1,69	Y+	SLD/31	-1,91
Y-	SLD/36	-4,11	Y-	SLD/37	-1,72	Y-	SLD/37	-1,56	Y-	SLD/37	-1,74
450	SLD/1	-3,15	451	SLD/1	-3,10	452	SLD/1	-2,84	453	SLD/1	-2,49
	SLD/2	-3,07		SLD/2	-3,02		SLD/2	-2,76		SLD/2	-2,42
	SLD/3	-3,15		SLD/3	-3,10		SLD/3	-2,85		SLD/3	-2,49
	SLD/4	-3,07		SLD/4	-3,02		SLD/4	-2,76		SLD/4	-2,42
	SLD/5	-3,02		SLD/5	-2,97		SLD/5	-2,71		SLD/5	-2,37
	SLD/6	-3,16		SLD/6	-3,12		SLD/6	-2,86		SLD/6	-2,51
	SLD/7	-3,08		SLD/7	-3,04		SLD/7	-2,77		SLD/7	-2,44
	SLD/8	-3,04		SLD/8	-3,00		SLD/8	-2,73		SLD/8	-2,39
	SLD/9	-3,14		SLD/9	-3,10		SLD/9	-2,84		SLD/9	-2,49
	SLD/10	-3,07		SLD/10	-3,02		SLD/10	-2,76		SLD/10	-2,42
	SLD/11	-3,02		SLD/11	-2,96		SLD/11	-2,70		SLD/11	-2,36
	SLD/12	-3,14		SLD/12	-3,09		SLD/12	-2,83		SLD/12	-2,47
	SLD/13	-3,06		SLD/13	-3,00		SLD/13	-2,74		SLD/13	-2,40
	SLD/14	-3,01		SLD/14	-2,94		SLD/14	-2,68		SLD/14	-2,33
X+	SLD/15	-2,16	X+	SLD/15	-2,12	X+	SLD/15	-1,91	X+	SLD/15	-1,68
X-	SLD/24	-2,11	X-	SLD/24	-2,07	X-	SLD/24	-1,86	X-	SLD/24	-1,63
Y+	SLD/31	-2,20	Y+	SLD/31	-2,21	Y+	SLD/31	-1,98	Y+	SLD/31	-1,78
Y-	SLD/37	-2,02	Y-	SLD/37	-1,90	Y-	SLD/37	-1,72	Y-	SLD/37	-1,43
454	SLD/1	-2,18	455	SLD/1	-3,07	456	SLD/1	-3,06	457	SLD/1	-1,88
	SLD/2	-2,12		SLD/2	-2,99		SLD/2	-2,96		SLD/2	-1,84
	SLD/3	-2,18		SLD/3	-3,08		SLD/3	-3,06		SLD/3	-1,88
	SLD/4	-2,13		SLD/4	-3,00		SLD/4	-2,96		SLD/4	-1,84
	SLD/5	-2,08		SLD/5	-2,95		SLD/5	-2,92		SLD/5	-1,81
	SLD/6	-2,19		SLD/6	-3,09		SLD/6	-3,07		SLD/6	-1,89
	SLD/7	-2,14		SLD/7	-3,01		SLD/7	-2,97		SLD/7	-1,85
	SLD/8	-2,10		SLD/8	-2,98		SLD/8	-2,93		SLD/8	-1,82
	SLD/9	-2,18		SLD/9	-3,07		SLD/9	-3,06		SLD/9	-1,88
	SLD/10	-2,12		SLD/10	-2,99		SLD/10	-2,96		SLD/10	-1,84
	SLD/11	-2,08		SLD/11	-2,95		SLD/11	-2,91		SLD/11	-1,80
	SLD/12	-2,16		SLD/12	-3,06		SLD/12	-3,05		SLD/12	-1,87
	SLD/13	-2,11		SLD/13	-2,98		SLD/13	-2,95		SLD/13	-1,83
	SLD/14	-2,06		SLD/14	-2,92		SLD/14	-2,90		SLD/14	-1,79
X+	SLD/15	-1,48	X+	SLD/15	-2,13	X+	SLD/15	-2,05	X+	SLD/15	-1,29
X-	SLD/24	-1,45	X-	SLD/24	-2,07	X-	SLD/24	-2,02	X-	SLD/24	-1,26
Y+	SLD/31	-1,57	Y+	SLD/31	-2,21	Y+	SLD/31	-2,10	Y+	SLD/31	-1,34
Y-	SLD/37	-1,30	Y-	SLD/37	-1,92	Y-	SLD/37	-1,92	Y-	SLD/37	-1,17
458	SLD/1	-3,18	459	SLD/1	-3,25	460	SLD/1	-3,50	461	SLD/1	-3,36
	SLD/2	-3,11		SLD/2	-3,18		SLD/2	-3,41		SLD/2	-3,28
	SLD/3	-3,18		SLD/3	-3,25		SLD/3	-3,51		SLD/3	-3,36
	SLD/4	-3,12		SLD/4	-3,19		SLD/4	-3,41		SLD/4	-3,28
	SLD/5	-3,07		SLD/5	-3,14		SLD/5	-3,37		SLD/5	-3,24
	SLD/6	-3,20		SLD/6	-3,27		SLD/6	-3,52		SLD/6	-3,38
	SLD/7	-3,13		SLD/7	-3,21		SLD/7	-3,42		SLD/7	-3,30
	SLD/8	-3,09		SLD/8	-3,17		SLD/8	-3,38		SLD/8	-3,27
	SLD/9	-3,18		SLD/9	-3,24		SLD/9	-3,50		SLD/9	-3,35
	SLD/10	-3,11		SLD/10	-3,18		SLD/10	-3,41		SLD/10	-3,27
	SLD/11	-3,05		SLD/11	-3,13		SLD/11	-3,36		SLD/11	-3,22
	SLD/12	-3,16		SLD/12	-3,23		SLD/12	-3,49		SLD/12	-3,34
	SLD/13	-3,10		SLD/13	-3,16		SLD/13	-3,40		SLD/13	-3,26
	SLD/14	-3,03		SLD/14	-3,10		SLD/14	-3,34		SLD/14	-3,20
X+	SLD/15	-2,24	X+	SLD/15	-2,33	X+	SLD/15	-2,41	X+	SLD/15	-2,41
X-	SLD/24	-2,14	X-	SLD/24	-2,22	X-	SLD/24	-2,34	X-	SLD/24	-2,27
Y+	SLD/31	-2,31	Y+	SLD/31	-2,44	Y+	SLD/31	-2,46	Y+	SLD/31	-2,50
Y-	SLD/37	-1,99	Y-	SLD/37	-2,02	Y-	SLD/37	-2,24	Y-	SLD/37	-2,10
462	SLD/1	-4,13	463	SLD/1	-4,09	464	SLD/1	-3,54	465	SLD/1	-4,46
	SLD/2	-4,04		SLD/2	-4,01		SLD/2	-3,48		SLD/2	-4,39
	SLD/3	-4,13		SLD/3	-4,10		SLD/3	-3,55		SLD/3	-4,48
	SLD/4	-4,05		SLD/4	-4,02		SLD/4	-3,49		SLD/4	-4,42
	SLD/5	-3,99		SLD/5	-3,97		SLD/5	-3,44		SLD/5	-4,37
	SLD/6	-4,15		SLD/6	-4,13		SLD/6	-3,58		SLD/6	-4,53
	SLD/7	-4,06		SLD/7	-4,05		SLD/7	-3,52		SLD/7	-4,46
	SLD/8	-4,01		SLD/8	-4,01		SLD/8	-3,49		SLD/8	-4,44
	SLD/9	-4,12		SLD/9	-4,07		SLD/9	-3,53		SLD/9	-4,44
	SLD/10	-4,03		SLD/10	-3,99		SLD/10	-3,47		SLD/10	-4,37
	SLD/11	-3,96		SLD/11	-3,93		SLD/11	-3,42		SLD/11	-4,29
	SLD/12	-4,11		SLD/12	-4,05		SLD/12	-3,50		SLD/12	-4,39
	SLD/13	-4,02		SLD/13	-3,97		SLD/13	-3,44		SLD/13	-4,33
	SLD/14	-3,94		SLD/14	-3,89		SLD/14	-3,37		SLD/14	-4,22
X+	SLD/15	-2,93	X+	SLD/15	-3,08	X+	SLD/15	-2,65	X+	SLD/15	-3,58

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	X- SLD/24	-2,75		X- SLD/24	-2,73		X- SLD/24	-2,45		X- SLD/24	-3,02
	Y+ SLD/31	-2,99		Y+ SLD/31	-3,20		Y+ SLD/31	-2,82		Y+ SLD/31	-3,82
	Y- SLD/37	-2,64		Y- SLD/37	-2,52		Y- SLD/37	-2,14		Y- SLD/37	-2,60
466	SLD/1	-1,84	467	SLD/1	-2,47	468	SLD/1	-1,96	469	SLD/1	-2,48
	SLD/2	-1,78		SLD/2	-2,39		SLD/2	-1,90		SLD/2	-2,39
	SLD/3	-1,84		SLD/3	-2,47		SLD/3	-1,96		SLD/3	-2,48
	SLD/4	-1,78		SLD/4	-2,39		SLD/4	-1,90		SLD/4	-2,39
	SLD/5	-1,75		SLD/5	-2,36		SLD/5	-1,87		SLD/5	-2,36
	SLD/6	-1,84		SLD/6	-2,48		SLD/6	-1,96		SLD/6	-2,48
	SLD/7	-1,78		SLD/7	-2,39		SLD/7	-1,90		SLD/7	-2,39
	SLD/8	-1,76		SLD/8	-2,36		SLD/8	-1,87		SLD/8	-2,35
	SLD/9	-1,84		SLD/9	-2,47		SLD/9	-1,96		SLD/9	-2,47
	SLD/10	-1,78		SLD/10	-2,38		SLD/10	-1,90		SLD/10	-2,39
	SLD/11	-1,75		SLD/11	-2,35		SLD/11	-1,86		SLD/11	-2,35
	SLD/12	-1,83		SLD/12	-2,47		SLD/12	-1,96		SLD/12	-2,48
	SLD/13	-1,78		SLD/13	-2,38		SLD/13	-1,90		SLD/13	-2,39
	SLD/14	-1,74		SLD/14	-2,35		SLD/14	-1,86		SLD/14	-2,35
X+	SLD/15	-1,22	X+	SLD/15	-1,66	X+	SLD/15	-1,27	X+	SLD/18	-1,63
X-	SLD/24	-1,19	X-	SLD/24	-1,60	X-	SLD/24	-1,26	X-	SLD/25	-1,59
Y+	SLD/31	-1,24	Y+	SLD/31	-1,67	Y+	SLD/31	-1,27	Y+	SLD/34	-1,62
Y-	SLD/37	-1,16	Y-	SLD/37	-1,58	Y-	SLD/37	-1,26	Y-	SLD/36	-1,61
470	SLD/1	-2,48	471	SLD/1	-2,71	472	SLD/1	-2,50	473	SLD/1	-2,71
	SLD/2	-2,40		SLD/2	-2,62		SLD/2	-2,41		SLD/2	-2,62
	SLD/3	-2,49		SLD/3	-2,71		SLD/3	-2,50		SLD/3	-2,71
	SLD/4	-2,40		SLD/4	-2,62		SLD/4	-2,41		SLD/4	-2,62
	SLD/5	-2,38		SLD/5	-2,58		SLD/5	-2,38		SLD/5	-2,58
	SLD/6	-2,49		SLD/6	-2,71		SLD/6	-2,50		SLD/6	-2,70
	SLD/7	-2,40		SLD/7	-2,62		SLD/7	-2,41		SLD/7	-2,62
	SLD/8	-2,38		SLD/8	-2,57		SLD/8	-2,38		SLD/8	-2,58
	SLD/9	-2,48		SLD/9	-2,71		SLD/9	-2,49		SLD/9	-2,71
	SLD/10	-2,40		SLD/10	-2,62		SLD/10	-2,41		SLD/10	-2,62
	SLD/11	-2,37		SLD/11	-2,56		SLD/11	-2,38		SLD/11	-2,58
	SLD/12	-2,48		SLD/12	-2,71		SLD/12	-2,50		SLD/12	-2,71
	SLD/13	-2,40		SLD/13	-2,62		SLD/13	-2,41		SLD/13	-2,62
	SLD/14	-2,37		SLD/14	-2,57		SLD/14	-2,38		SLD/14	-2,58
X+	SLD/15	-1,66	X+	SLD/20	-1,80	X+	SLD/18	-1,64	X+	SLD/20	-1,78
X-	SLD/24	-1,63	X-	SLD/27	-1,70	X-	SLD/25	-1,64	X-	SLD/27	-1,76
Y+	SLD/31	-1,67	Y+	SLD/34	-1,75	Y+	SLD/34	-1,64	Y+	SLD/34	-1,76
Y-	SLD/37	-1,62	Y-	SLD/36	-1,77	Y-	SLD/36	-1,64	Y-	SLD/36	-1,79
474	SLD/1	-1,66	475	SLD/1	-2,49	476	SLD/1	-2,33	477	SLD/1	-2,05
	SLD/2	-1,61		SLD/2	-2,41		SLD/2	-2,25		SLD/2	-1,98
	SLD/3	-1,66		SLD/3	-2,50		SLD/3	-2,33		SLD/3	-2,05
	SLD/4	-1,61		SLD/4	-2,41		SLD/4	-2,25		SLD/4	-1,98
	SLD/5	-1,58		SLD/5	-2,37		SLD/5	-2,22		SLD/5	-1,94
	SLD/6	-1,66		SLD/6	-2,49		SLD/6	-2,33		SLD/6	-2,05
	SLD/7	-1,61		SLD/7	-2,41		SLD/7	-2,25		SLD/7	-1,98
	SLD/8	-1,58		SLD/8	-2,37		SLD/8	-2,22		SLD/8	-1,94
	SLD/9	-1,66		SLD/9	-2,49		SLD/9	-2,33		SLD/9	-2,05
	SLD/10	-1,61		SLD/10	-2,41		SLD/10	-2,25		SLD/10	-1,98
	SLD/11	-1,57		SLD/11	-2,36		SLD/11	-2,21		SLD/11	-1,94
	SLD/12	-1,66		SLD/12	-2,49		SLD/12	-2,33		SLD/12	-2,05
	SLD/13	-1,61		SLD/13	-2,41		SLD/13	-2,25		SLD/13	-1,98
	SLD/14	-1,57		SLD/14	-2,36		SLD/14	-2,22		SLD/14	-1,94
X+	SLD/18	-1,07	X+	SLD/18	-1,65	X+	SLD/20	-1,53	X+	SLD/18	-1,33
X-	SLD/25	-1,05	X-	SLD/25	-1,56	X-	SLD/27	-1,50	X-	SLD/25	-1,32
Y+	SLD/34	-1,08	Y+	SLD/34	-1,63	Y+	SLD/34	-1,52	Y+	SLD/34	-1,33
Y-	SLD/36	-1,05	Y-	SLD/36	-1,62	Y-	SLD/36	-1,52	Y-	SLD/36	-1,31
478	SLD/1	-2,04	479	SLD/1	-2,91	480	SLD/1	-2,97	481	SLD/1	-3,32
	SLD/2	-1,98		SLD/2	-2,83		SLD/2	-2,89		SLD/2	-3,25
	SLD/3	-2,04		SLD/3	-2,91		SLD/3	-2,97		SLD/3	-3,32
	SLD/4	-1,98		SLD/4	-2,83		SLD/4	-2,88		SLD/4	-3,25
	SLD/5	-1,94		SLD/5	-2,80		SLD/5	-2,84		SLD/5	-3,20
	SLD/6	-2,04		SLD/6	-2,92		SLD/6	-2,97		SLD/6	-3,32
	SLD/7	-1,98		SLD/7	-2,83		SLD/7	-2,88		SLD/7	-3,25
	SLD/8	-1,93		SLD/8	-2,80		SLD/8	-2,84		SLD/8	-3,20
	SLD/9	-2,04		SLD/9	-2,91		SLD/9	-2,97		SLD/9	-3,32
	SLD/10	-1,98		SLD/10	-2,83		SLD/10	-2,89		SLD/10	-3,25
	SLD/11	-1,93		SLD/11	-2,80		SLD/11	-2,85		SLD/11	-3,20
	SLD/12	-2,05		SLD/12	-2,91		SLD/12	-2,97		SLD/12	-3,31
	SLD/13	-1,98		SLD/13	-2,83		SLD/13	-2,89		SLD/13	-3,25
	SLD/14	-1,94		SLD/14	-2,79		SLD/14	-2,85		SLD/14	-3,19
X+	SLD/20	-1,32	X+	SLD/15	-1,95	X+	SLD/20	-1,97	X+	SLD/15	-2,23
X-	SLD/27	-1,29	X-	SLD/24	-1,95	X-	SLD/27	-1,99	X-	SLD/24	-2,24
Y+	SLD/34	-1,29	Y+	SLD/40	-1,96	Y+	SLD/41	-1,95	Y+	SLD/40	-2,25
Y-	SLD/36	-1,32	Y-	SLD/46	-1,92	Y-	SLD/43	-2,00	Y-	SLD/46	-2,21
482	SLD/1	-3,21	483	SLD/1	-2,13	484	SLD/1	-3,47	485	SLD/1	-3,82
	SLD/2	-3,15		SLD/2	-2,08		SLD/2	-3,40		SLD/2	-3,74

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/3	-3,21		SLD/3	-2,13		SLD/3	-3,47		SLD/3	-3,81
	SLD/4	-3,15		SLD/4	-2,08		SLD/4	-3,40		SLD/4	-3,74
	SLD/5	-3,09		SLD/5	-2,04		SLD/5	-3,33		SLD/5	-3,66
	SLD/6	-3,22		SLD/6	-2,14		SLD/6	-3,46		SLD/6	-3,81
	SLD/7	-3,16		SLD/7	-2,09		SLD/7	-3,39		SLD/7	-3,73
	SLD/8	-3,11		SLD/8	-2,06		SLD/8	-3,33		SLD/8	-3,65
	SLD/9	-3,21		SLD/9	-2,13		SLD/9	-3,47		SLD/9	-3,82
	SLD/10	-3,15		SLD/10	-2,08		SLD/10	-3,40		SLD/10	-3,75
	SLD/11	-3,10		SLD/11	-2,05		SLD/11	-3,34		SLD/11	-3,67
	SLD/12	-3,20		SLD/12	-2,12		SLD/12	-3,47		SLD/12	-3,83
	SLD/13	-3,14		SLD/13	-2,07		SLD/13	-3,40		SLD/13	-3,75
	SLD/14	-3,08		SLD/14	-2,03		SLD/14	-3,35		SLD/14	-3,68
X+	SLD/15	-2,17	X+	SLD/15	-1,43	X+	SLD/20	-2,32	X+	SLD/20	-2,53
X-	SLD/24	-2,20	X-	SLD/24	-1,47	X-	SLD/27	-2,35	X-	SLD/27	-2,59
Y+	SLD/40	-2,25	Y+	SLD/40	-1,52	Y+	SLD/41	-2,27	Y+	SLD/41	-2,45
Y-	SLD/46	-2,08	Y-	SLD/46	-1,34	Y-	SLD/43	-2,38	Y-	SLD/43	-2,64
486	SLD/1	-3,18	487	SLD/1	-2,48	488	SLD/1	-2,35	489	SLD/1	-2,38
	SLD/2	-3,09		SLD/2	-2,40		SLD/2	-2,27		SLD/2	-2,30
	SLD/3	-3,17		SLD/3	-2,48		SLD/3	-2,35		SLD/3	-2,38
	SLD/4	-3,09		SLD/4	-2,40		SLD/4	-2,27		SLD/4	-2,30
	SLD/5	-3,04		SLD/5	-2,36		SLD/5	-2,24		SLD/5	-2,28
	SLD/6	-3,17		SLD/6	-2,48		SLD/6	-2,35		SLD/6	-2,38
	SLD/7	-3,09		SLD/7	-2,39		SLD/7	-2,27		SLD/7	-2,30
	SLD/8	-3,04		SLD/8	-2,36		SLD/8	-2,24		SLD/8	-2,27
	SLD/9	-3,18		SLD/9	-2,48		SLD/9	-2,35		SLD/9	-2,38
	SLD/10	-3,10		SLD/10	-2,40		SLD/10	-2,27		SLD/10	-2,30
	SLD/11	-3,05		SLD/11	-2,36		SLD/11	-2,24		SLD/11	-2,27
	SLD/12	-3,18		SLD/12	-2,48		SLD/12	-2,35		SLD/12	-2,38
	SLD/13	-3,10		SLD/13	-2,40		SLD/13	-2,27		SLD/13	-2,30
	SLD/14	-3,05		SLD/14	-2,36		SLD/14	-2,25		SLD/14	-2,28
X+	SLD/21	-2,07	X+	SLD/20	-1,63	X+	SLD/20	-1,55	X+	SLD/20	-1,58
X-	SLD/30	-2,16	X-	SLD/27	-1,61	X-	SLD/27	-1,55	X-	SLD/27	-1,57
Y+	SLD/40	-2,07	Y+	SLD/34	-1,61	Y+	SLD/34	-1,54	Y+	SLD/34	-1,57
Y-	SLD/46	-2,16	Y-	SLD/36	-1,63	Y-	SLD/36	-1,56	Y-	SLD/36	-1,58
490	SLD/1	-1,84	491	SLD/1	-2,78	492	SLD/1	-2,27	493	SLD/1	-2,38
	SLD/2	-1,78		SLD/2	-2,70		SLD/2	-2,21		SLD/2	-2,29
	SLD/3	-1,84		SLD/3	-2,78		SLD/3	-2,27		SLD/3	-2,38
	SLD/4	-1,78		SLD/4	-2,70		SLD/4	-2,21		SLD/4	-2,29
	SLD/5	-1,76		SLD/5	-2,67		SLD/5	-2,17		SLD/5	-2,27
	SLD/6	-1,84		SLD/6	-2,78		SLD/6	-2,27		SLD/6	-2,38
	SLD/7	-1,78		SLD/7	-2,70		SLD/7	-2,21		SLD/7	-2,29
	SLD/8	-1,75		SLD/8	-2,66		SLD/8	-2,17		SLD/8	-2,27
	SLD/9	-1,84		SLD/9	-2,78		SLD/9	-2,26		SLD/9	-2,38
	SLD/10	-1,78		SLD/10	-2,70		SLD/10	-2,21		SLD/10	-2,29
	SLD/11	-1,76		SLD/11	-2,66		SLD/11	-2,17		SLD/11	-2,27
	SLD/12	-1,84		SLD/12	-2,78		SLD/12	-2,27		SLD/12	-2,38
	SLD/13	-1,78		SLD/13	-2,70		SLD/13	-2,21		SLD/13	-2,29
	SLD/14	-1,76		SLD/14	-2,66		SLD/14	-2,17		SLD/14	-2,27
X+	SLD/20	-1,21	X+	SLD/18	-1,86	X+	SLD/20	-1,51	X+	SLD/20	-1,58
X-	SLD/27	-1,21	X-	SLD/25	-1,83	X-	SLD/27	-1,49	X-	SLD/27	-1,57
Y+	SLD/34	-1,20	Y+	SLD/34	-1,85	Y+	SLD/34	-1,50	Y+	SLD/34	-1,57
Y-	SLD/36	-1,22	Y-	SLD/36	-1,84	Y-	SLD/36	-1,51	Y-	SLD/36	-1,58
494	SLD/1	-2,37	495	SLD/1	-3,15	496	SLD/1	-2,64	497	SLD/1	-2,56
	SLD/2	-2,32		SLD/2	-3,07		SLD/2	-2,56		SLD/2	-2,48
	SLD/3	-2,37		SLD/3	-3,15		SLD/3	-2,64		SLD/3	-2,56
	SLD/4	-2,32		SLD/4	-3,07		SLD/4	-2,56		SLD/4	-2,48
	SLD/5	-2,28		SLD/5	-3,03		SLD/5	-2,53		SLD/5	-2,45
	SLD/6	-2,37		SLD/6	-3,15		SLD/6	-2,64		SLD/6	-2,56
	SLD/7	-2,32		SLD/7	-3,08		SLD/7	-2,56		SLD/7	-2,48
	SLD/8	-2,28		SLD/8	-3,03		SLD/8	-2,53		SLD/8	-2,45
	SLD/9	-2,37		SLD/9	-3,15		SLD/9	-2,64		SLD/9	-2,56
	SLD/10	-2,32		SLD/10	-3,07		SLD/10	-2,56		SLD/10	-2,48
	SLD/11	-2,27		SLD/11	-3,02		SLD/11	-2,53		SLD/11	-2,45
	SLD/12	-2,37		SLD/12	-3,15		SLD/12	-2,64		SLD/12	-2,57
	SLD/13	-2,32		SLD/13	-3,07		SLD/13	-2,56		SLD/13	-2,48
	SLD/14	-2,27		SLD/14	-3,02		SLD/14	-2,53		SLD/14	-2,45
X+	SLD/18	-1,60	X+	SLD/18	-2,12	X+	SLD/18	-1,76	X+	SLD/20	-1,69
X-	SLD/25	-1,56	X-	SLD/25	-2,08	X-	SLD/25	-1,75	X-	SLD/27	-1,71
Y+	SLD/34	-1,61	Y+	SLD/34	-2,13	Y+	SLD/34	-1,77	Y+	SLD/41	-1,68
Y-	SLD/36	-1,55	Y-	SLD/36	-2,06	Y-	SLD/36	-1,75	Y-	SLD/43	-1,72
498	SLD/1	-2,53	499	SLD/1	-2,90	500	SLD/1	-2,82	501	SLD/1	-2,78
	SLD/2	-2,45		SLD/2	-2,82		SLD/2	-2,74		SLD/2	-2,70
	SLD/3	-2,53		SLD/3	-2,90		SLD/3	-2,82		SLD/3	-2,77
	SLD/4	-2,45		SLD/4	-2,82		SLD/4	-2,74		SLD/4	-2,69
	SLD/5	-2,42		SLD/5	-2,78		SLD/5	-2,70		SLD/5	-2,65
	SLD/6	-2,53		SLD/6	-2,90		SLD/6	-2,82		SLD/6	-2,77
	SLD/7	-2,44		SLD/7	-2,82		SLD/7	-2,74		SLD/7	-2,69
	SLD/8	-2,42		SLD/8	-2,78		SLD/8	-2,71		SLD/8	-2,65

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/9	-2,53		SLD/9	-2,90		SLD/9	-2,82		SLD/9	-2,78
	SLD/10	-2,45		SLD/10	-2,82		SLD/10	-2,74		SLD/10	-2,70
	SLD/11	-2,42		SLD/11	-2,78		SLD/11	-2,70		SLD/11	-2,66
	SLD/12	-2,53		SLD/12	-2,89		SLD/12	-2,82		SLD/12	-2,78
	SLD/13	-2,45		SLD/13	-2,81		SLD/13	-2,74		SLD/13	-2,70
	SLD/14	-2,42		SLD/14	-2,77		SLD/14	-2,70		SLD/14	-2,66
X+	SLD/20	-1,68	X+	SLD/15	-1,95	X+	SLD/15	-1,88	X+	SLD/21	-1,79
X-	SLD/27	-1,69	X-	SLD/24	-1,93	X-	SLD/24	-1,88	X-	SLD/30	-1,89
Y+	SLD/41	-1,67	Y+	SLD/31	-1,97	Y+	SLD/40	-1,89	Y+	SLD/40	-1,82
Y-	SLD/43	-1,69	Y-	SLD/37	-1,89	Y-	SLD/46	-1,87	Y-	SLD/46	-1,87
502	SLD/1	-2,52	503	SLD/1	-3,16	504	SLD/1	-2,11	505	SLD/1	-2,55
	SLD/2	-2,45		SLD/2	-3,09		SLD/2	-2,05		SLD/2	-2,49
	SLD/3	-2,52		SLD/3	-3,16		SLD/3	-2,11		SLD/3	-2,55
	SLD/4	-2,45		SLD/4	-3,09		SLD/4	-2,05		SLD/4	-2,49
	SLD/5	-2,41		SLD/5	-3,03		SLD/5	-2,02		SLD/5	-2,45
	SLD/6	-2,51		SLD/6	-3,16		SLD/6	-2,11		SLD/6	-2,55
	SLD/7	-2,44		SLD/7	-3,09		SLD/7	-2,04		SLD/7	-2,49
	SLD/8	-2,41		SLD/8	-3,03		SLD/8	-2,02		SLD/8	-2,45
	SLD/9	-2,52		SLD/9	-3,17		SLD/9	-2,11		SLD/9	-2,55
	SLD/10	-2,45		SLD/10	-3,09		SLD/10	-2,05		SLD/10	-2,49
	SLD/11	-2,41		SLD/11	-3,03		SLD/11	-2,02		SLD/11	-2,45
	SLD/12	-2,52		SLD/12	-3,17		SLD/12	-2,11		SLD/12	-2,55
	SLD/13	-2,45		SLD/13	-3,09		SLD/13	-2,05		SLD/13	-2,49
	SLD/14	-2,41		SLD/14	-3,04		SLD/14	-2,03		SLD/14	-2,45
X+	SLD/20	-1,66	X+	SLD/20	-2,07	X+	SLD/20	-1,41	X+	SLD/21	-1,70
X-	SLD/27	-1,69	X-	SLD/27	-2,12	X-	SLD/27	-1,42	X-	SLD/30	-1,71
Y+	SLD/41	-1,65	Y+	SLD/41	-2,06	Y+	SLD/41	-1,38	Y+	SLD/40	-1,71
Y-	SLD/43	-1,69	Y-	SLD/43	-2,13	Y-	SLD/43	-1,44	Y-	SLD/46	-1,71
506	SLD/1	-3,44	507	SLD/1	-3,16	508	SLD/1	-2,23	509	SLD/1	-3,18
	SLD/2	-3,37		SLD/2	-3,08		SLD/2	-2,15		SLD/2	-3,08
	SLD/3	-3,44		SLD/3	-3,16		SLD/3	-2,23		SLD/3	-3,18
	SLD/4	-3,37		SLD/4	-3,08		SLD/4	-2,15		SLD/4	-3,08
	SLD/5	-3,30		SLD/5	-3,04		SLD/5	-2,13		SLD/5	-3,04
	SLD/6	-3,44		SLD/6	-3,17		SLD/6	-2,23		SLD/6	-3,18
	SLD/7	-3,37		SLD/7	-3,09		SLD/7	-2,14		SLD/7	-3,08
	SLD/8	-3,32		SLD/8	-3,05		SLD/8	-2,13		SLD/8	-3,04
	SLD/9	-3,44		SLD/9	-3,16		SLD/9	-2,23		SLD/9	-3,18
	SLD/10	-3,37		SLD/10	-3,08		SLD/10	-2,15		SLD/10	-3,08
	SLD/11	-3,30		SLD/11	-3,04		SLD/11	-2,13		SLD/11	-3,04
	SLD/12	-3,43		SLD/12	-3,16		SLD/12	-2,23		SLD/12	-3,18
	SLD/13	-3,36		SLD/13	-3,08		SLD/13	-2,15		SLD/13	-3,08
	SLD/14	-3,29		SLD/14	-3,03		SLD/14	-2,13		SLD/14	-3,05
X+	SLD/15	-2,31	X+	SLD/15	-2,12	X+	SLD/20	-1,48	X+	SLD/20	-2,12
X-	SLD/24	-2,32	X-	SLD/24	-2,12	X-	SLD/27	-1,48	X-	SLD/27	-2,11
Y+	SLD/40	-2,36	Y+	SLD/40	-2,16	Y+	SLD/34	-1,46	Y+	SLD/34	-2,09
Y-	SLD/46	-2,22	Y-	SLD/46	-2,06	Y-	SLD/36	-1,49	Y-	SLD/36	-2,14
510	SLD/1	-2,56	511	SLD/1	-2,13	512	SLD/1	-2,46	513	SLD/1	-1,94
	SLD/2	-2,47		SLD/2	-2,04		SLD/2	-2,37		SLD/2	-1,85
	SLD/3	-2,56		SLD/3	-2,13		SLD/3	-2,46		SLD/3	-1,94
	SLD/4	-2,47		SLD/4	-2,04		SLD/4	-2,38		SLD/4	-1,85
	SLD/5	-2,45		SLD/5	-2,03		SLD/5	-2,35		SLD/5	-1,84
	SLD/6	-2,56		SLD/6	-2,13		SLD/6	-2,46		SLD/6	-1,94
	SLD/7	-2,47		SLD/7	-2,04		SLD/7	-2,37		SLD/7	-1,85
	SLD/8	-2,45		SLD/8	-2,03		SLD/8	-2,34		SLD/8	-1,84
	SLD/9	-2,56		SLD/9	-2,13		SLD/9	-2,46		SLD/9	-1,94
	SLD/10	-2,47		SLD/10	-2,04		SLD/10	-2,37		SLD/10	-1,85
	SLD/11	-2,45		SLD/11	-2,03		SLD/11	-2,35		SLD/11	-1,84
	SLD/12	-2,56		SLD/12	-2,13		SLD/12	-2,46		SLD/12	-1,94
	SLD/13	-2,47		SLD/13	-2,04		SLD/13	-2,38		SLD/13	-1,85
	SLD/14	-2,45		SLD/14	-2,03		SLD/14	-2,35		SLD/14	-1,84
X+	SLD/20	-1,71	X+	SLD/21	-1,40	X+	SLD/20	-1,65	X+	SLD/21	-1,27
X-	SLD/27	-1,72	X-	SLD/30	-1,42	X-	SLD/27	-1,61	X-	SLD/30	-1,28
Y+	SLD/41	-1,68	Y+	SLD/40	-1,41	Y+	SLD/34	-1,61	Y+	SLD/40	-1,27
Y-	SLD/43	-1,73	Y-	SLD/46	-1,42	Y-	SLD/36	-1,65	Y-	SLD/46	-1,28
514	SLD/1	-1,86	515	SLD/1	-1,80	516	SLD/1	-1,66	517	SLD/1	-1,65
	SLD/2	-1,77		SLD/2	-1,71		SLD/2	-1,57		SLD/2	-1,55
	SLD/3	-1,86		SLD/3	-1,80		SLD/3	-1,66		SLD/3	-1,64
	SLD/4	-1,77		SLD/4	-1,71		SLD/4	-1,57		SLD/4	-1,55
	SLD/5	-1,77		SLD/5	-1,71		SLD/5	-1,57		SLD/5	-1,56
	SLD/6	-1,86		SLD/6	-1,80		SLD/6	-1,66		SLD/6	-1,65
	SLD/7	-1,77		SLD/7	-1,71		SLD/7	-1,57		SLD/7	-1,55
	SLD/8	-1,77		SLD/8	-1,71		SLD/8	-1,57		SLD/8	-1,56
	SLD/9	-1,87		SLD/9	-1,80		SLD/9	-1,66		SLD/9	-1,65
	SLD/10	-1,78		SLD/10	-1,71		SLD/10	-1,58		SLD/10	-1,56
	SLD/11	-1,78		SLD/11	-1,72		SLD/11	-1,58		SLD/11	-1,57
	SLD/12	-1,86		SLD/12	-1,80		SLD/12	-1,66		SLD/12	-1,65
	SLD/13	-1,77		SLD/13	-1,71		SLD/13	-1,57		SLD/13	-1,55
	SLD/14	-1,77		SLD/14	-1,71		SLD/14	-1,58		SLD/14	-1,56

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	X+ SLD/21	-1,21		X+ SLD/21	-1,17		X+ SLD/21	-1,07		X+ SLD/21	-1,05
	X- SLD/30	-1,25		X- SLD/30	-1,22		X- SLD/30	-1,12		X- SLD/30	-1,12
	Y+ SLD/40	-1,23		Y+ SLD/40	-1,20		Y+ SLD/40	-1,10		Y+ SLD/40	-1,10
	Y- SLD/46	-1,24		Y- SLD/46	-1,20		Y- SLD/46	-1,11		Y- SLD/46	-1,10
518	SLD/1	-3,77	519	SLD/1	-2,23	520	SLD/1	-2,97	521	SLD/1	-1,69
	SLD/2	-3,67		SLD/2	-2,14		SLD/2	-2,88		SLD/2	-1,61
	SLD/3	-3,77		SLD/3	-2,23		SLD/3	-2,97		SLD/3	-1,69
	SLD/4	-3,67		SLD/4	-2,14		SLD/4	-2,88		SLD/4	-1,60
	SLD/5	-3,61		SLD/5	-2,13		SLD/5	-2,85		SLD/5	-1,60
	SLD/6	-3,76		SLD/6	-2,23		SLD/6	-2,97		SLD/6	-1,69
	SLD/7	-3,66		SLD/7	-2,14		SLD/7	-2,88		SLD/7	-1,60
	SLD/8	-3,60		SLD/8	-2,13		SLD/8	-2,85		SLD/8	-1,60
	SLD/9	-3,76		SLD/9	-2,23		SLD/9	-2,97		SLD/9	-1,69
	SLD/10	-3,67		SLD/10	-2,14		SLD/10	-2,88		SLD/10	-1,61
	SLD/11	-3,60		SLD/11	-2,13		SLD/11	-2,85		SLD/11	-1,61
	SLD/12	-3,77		SLD/12	-2,23		SLD/12	-2,97		SLD/12	-1,70
	SLD/13	-3,67		SLD/13	-2,14		SLD/13	-2,88		SLD/13	-1,61
	SLD/14	-3,61		SLD/14	-2,13		SLD/14	-2,85		SLD/14	-1,62
X+	SLD/20	-2,54	X+	SLD/15	-1,47	X+	SLD/15	-1,97	X+	SLD/20	-1,10
X-	SLD/27	-2,46	X-	SLD/24	-1,50	X-	SLD/24	-1,99	X-	SLD/27	-1,16
Y+	SLD/34	-2,46	Y+	SLD/40	-1,49	Y+	SLD/40	-1,99	Y+	SLD/41	-1,08
Y-	SLD/36	-2,55	Y-	SLD/46	-1,48	Y-	SLD/46	-1,98	Y-	SLD/43	-1,17
522	SLD/1	-1,65	523	SLD/1	-2,14	524	SLD/1	-1,99	525	SLD/1	-3,17
	SLD/2	-1,56		SLD/2	-2,06		SLD/2	-1,90		SLD/2	-3,10
	SLD/3	-1,65		SLD/3	-2,14		SLD/3	-1,99		SLD/3	-3,19
	SLD/4	-1,56		SLD/4	-2,06		SLD/4	-1,90		SLD/4	-3,11
	SLD/5	-1,56		SLD/5	-2,05		SLD/5	-1,90		SLD/5	-3,08
	SLD/6	-1,65		SLD/6	-2,12		SLD/6	-1,98		SLD/6	-3,14
	SLD/7	-1,56		SLD/7	-2,04		SLD/7	-1,89		SLD/7	-3,06
	SLD/8	-1,56		SLD/8	-2,02		SLD/8	-1,89		SLD/8	-3,00
	SLD/9	-1,66		SLD/9	-2,14		SLD/9	-1,99		SLD/9	-3,16
	SLD/10	-1,56		SLD/10	-2,05		SLD/10	-1,90		SLD/10	-3,08
	SLD/11	-1,57		SLD/11	-2,04		SLD/11	-1,90		SLD/11	-3,04
	SLD/12	-1,65		SLD/12	-2,16		SLD/12	-2,00		SLD/12	-3,21
	SLD/13	-1,56		SLD/13	-2,07		SLD/13	-1,91		SLD/13	-3,13
	SLD/14	-1,57		SLD/14	-2,07		SLD/14	-1,91		SLD/14	-3,12
X+	SLD/21	-1,06	X+	SLD/20	-1,51	X+	SLD/20	-1,35	X+	SLD/20	-2,46
X-	SLD/30	-1,14	X-	SLD/27	-1,46	X-	SLD/27	-1,36	X-	SLD/27	-2,13
Y+	SLD/40	-1,08	Y+	SLD/34	-1,31	Y+	SLD/41	-1,27	Y+	SLD/34	-1,93
Y-	SLD/46	-1,12	Y-	SLD/36	-1,60	Y-	SLD/43	-1,40	Y-	SLD/36	-2,58
526	SLD/1	-2,78	527	SLD/1	-1,88	528	SLD/1	-1,60	529	SLD/1	-1,60
	SLD/2	-2,70		SLD/2	-1,79		SLD/2	-1,51		SLD/2	-1,51
	SLD/3	-2,79		SLD/3	-1,88		SLD/3	-1,60		SLD/3	-1,60
	SLD/4	-2,71		SLD/4	-1,79		SLD/4	-1,51		SLD/4	-1,51
	SLD/5	-2,69		SLD/5	-1,79		SLD/5	-1,51		SLD/5	-1,51
	SLD/6	-2,76		SLD/6	-1,88		SLD/6	-1,60		SLD/6	-1,60
	SLD/7	-2,68		SLD/7	-1,79		SLD/7	-1,51		SLD/7	-1,51
	SLD/8	-2,65		SLD/8	-1,80		SLD/8	-1,52		SLD/8	-1,52
	SLD/9	-2,77		SLD/9	-1,88		SLD/9	-1,60		SLD/9	-1,61
	SLD/10	-2,69		SLD/10	-1,80		SLD/10	-1,51		SLD/10	-1,51
	SLD/11	-2,67		SLD/11	-1,80		SLD/11	-1,52		SLD/11	-1,52
	SLD/12	-2,80		SLD/12	-1,88		SLD/12	-1,60		SLD/12	-1,60
	SLD/13	-2,72		SLD/13	-1,79		SLD/13	-1,51		SLD/13	-1,51
	SLD/14	-2,71		SLD/14	-1,80		SLD/14	-1,52		SLD/14	-1,52
X+	SLD/20	-2,06	X+	SLD/21	-1,24	X+	SLD/21	-1,01	X+	SLD/21	-1,02
X-	SLD/27	-1,85	X-	SLD/30	-1,27	X-	SLD/30	-1,11	X-	SLD/30	-1,10
Y+	SLD/34	-1,80	Y+	SLD/40	-1,26	Y+	SLD/40	-1,07	Y+	SLD/40	-1,07
Y-	SLD/36	-2,09	Y-	SLD/46	-1,26	Y-	SLD/46	-1,08	Y-	SLD/46	-1,07
530	SLD/1	-3,00	531	SLD/1	-3,57	532	SLD/1	-2,54	533	SLD/1	-4,42
	SLD/2	-2,94		SLD/2	-3,51		SLD/2	-2,46		SLD/2	-4,36
	SLD/3	-3,02		SLD/3	-3,60		SLD/3	-2,54		SLD/3	-4,45
	SLD/4	-2,96		SLD/4	-3,53		SLD/4	-2,46		SLD/4	-4,39
	SLD/5	-2,94		SLD/5	-3,50		SLD/5	-2,45		SLD/5	-4,34
	SLD/6	-3,00		SLD/6	-3,55		SLD/6	-2,54		SLD/6	-4,36
	SLD/7	-2,94		SLD/7	-3,49		SLD/7	-2,46		SLD/7	-4,29
	SLD/8	-2,91		SLD/8	-3,43		SLD/8	-2,44		SLD/8	-4,19
	SLD/9	-2,99		SLD/9	-3,55		SLD/9	-2,53		SLD/9	-4,39
	SLD/10	-2,93		SLD/10	-3,49		SLD/10	-2,45		SLD/10	-4,33
	SLD/11	-2,89		SLD/11	-3,43		SLD/11	-2,43		SLD/11	-4,24
	SLD/12	-3,00		SLD/12	-3,60		SLD/12	-2,54		SLD/12	-4,49
	SLD/13	-2,94		SLD/13	-3,53		SLD/13	-2,46		SLD/13	-4,42
	SLD/14	-2,92		SLD/14	-3,51		SLD/14	-2,44		SLD/14	-4,40
X+	SLD/18	-2,29	X+	SLD/20	-2,83	X+	SLD/18	-1,81	X+	SLD/20	-3,70
X-	SLD/25	-1,89	X-	SLD/27	-2,29	X-	SLD/25	-1,65	X-	SLD/27	-2,89
Y+	SLD/34	-2,16	Y+	SLD/34	-2,39	Y+	SLD/34	-1,76	Y+	SLD/34	-2,70
Y-	SLD/36	-2,15	Y-	SLD/36	-2,79	Y-	SLD/36	-1,75	Y-	SLD/36	-3,83
534	SLD/1	-3,63	535	SLD/1	-2,32	536	SLD/1	-1,62	537	SLD/1	-1,84

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/2	-3,54		SLD/2	-2,24		SLD/2	-1,53		SLD/2	-1,75
	SLD/3	-3,63		SLD/3	-2,32		SLD/3	-1,62		SLD/3	-1,84
	SLD/4	-3,53		SLD/4	-2,24		SLD/4	-1,53		SLD/4	-1,75
	SLD/5	-3,48		SLD/5	-2,21		SLD/5	-1,53		SLD/5	-1,75
	SLD/6	-3,63		SLD/6	-2,32		SLD/6	-1,62		SLD/6	-1,84
	SLD/7	-3,54		SLD/7	-2,24		SLD/7	-1,53		SLD/7	-1,75
	SLD/8	-3,49		SLD/8	-2,22		SLD/8	-1,54		SLD/8	-1,75
	SLD/9	-3,63		SLD/9	-2,32		SLD/9	-1,63		SLD/9	-1,84
	SLD/10	-3,54		SLD/10	-2,24		SLD/10	-1,54		SLD/10	-1,75
	SLD/11	-3,48		SLD/11	-2,22		SLD/11	-1,55		SLD/11	-1,75
	SLD/12	-3,62		SLD/12	-2,31		SLD/12	-1,62		SLD/12	-1,84
	SLD/13	-3,53		SLD/13	-2,23		SLD/13	-1,53		SLD/13	-1,75
	SLD/14	-3,47		SLD/14	-2,21		SLD/14	-1,54		SLD/14	-1,75
X+	SLD/15	-2,42	X+	SLD/15	-1,53	X+	SLD/21	-1,03	X+	SLD/21	-1,19
X-	SLD/24	-2,45	X-	SLD/24	-1,56	X-	SLD/30	-1,11	X-	SLD/30	-1,25
Y+	SLD/40	-2,48	Y+	SLD/40	-1,57	Y+	SLD/40	-1,08	Y+	SLD/40	-1,22
Y-	SLD/46	-2,36	Y-	SLD/46	-1,52	Y-	SLD/46	-1,09	Y-	SLD/46	-1,23
538	SLD/1	-1,80	539	SLD/1	-1,57	540	SLD/1	-1,65	541	SLD/1	-1,64
	SLD/2	-1,71		SLD/2	-1,49		SLD/2	-1,55		SLD/2	-1,55
	SLD/3	-1,80		SLD/3	-1,57		SLD/3	-1,64		SLD/3	-1,63
	SLD/4	-1,71		SLD/4	-1,48		SLD/4	-1,55		SLD/4	-1,55
	SLD/5	-1,71		SLD/5	-1,49		SLD/5	-1,56		SLD/5	-1,55
	SLD/6	-1,80		SLD/6	-1,57		SLD/6	-1,65		SLD/6	-1,64
	SLD/7	-1,71		SLD/7	-1,49		SLD/7	-1,56		SLD/7	-1,56
	SLD/8	-1,71		SLD/8	-1,49		SLD/8	-1,56		SLD/8	-1,56
	SLD/9	-1,80		SLD/9	-1,57		SLD/9	-1,65		SLD/9	-1,64
	SLD/10	-1,72		SLD/10	-1,49		SLD/10	-1,56		SLD/10	-1,55
	SLD/11	-1,71		SLD/11	-1,50		SLD/11	-1,57		SLD/11	-1,56
	SLD/12	-1,80		SLD/12	-1,57		SLD/12	-1,64		SLD/12	-1,63
	SLD/13	-1,71		SLD/13	-1,49		SLD/13	-1,55		SLD/13	-1,55
	SLD/14	-1,71		SLD/14	-1,49		SLD/14	-1,56		SLD/14	-1,55
X+	SLD/15	-1,16	X+	SLD/15	-1,00	X+	SLD/15	-1,05	X+	SLD/15	-1,07
X-	SLD/24	-1,22	X-	SLD/24	-1,07	X-	SLD/24	-1,14	X-	SLD/24	-1,13
Y+	SLD/40	-1,20	Y+	SLD/40	-1,05	Y+	SLD/40	-1,12	Y+	SLD/40	-1,14
Y-	SLD/46	-1,20	Y-	SLD/46	-1,05	Y-	SLD/46	-1,09	Y-	SLD/46	-1,05
542	SLD/1	-1,99	543	SLD/1	-2,11	544	SLD/1	-2,79	545	SLD/1	-3,27
	SLD/2	-1,90		SLD/2	-2,03		SLD/2	-2,71		SLD/2	-3,21
	SLD/3	-1,99		SLD/3	-2,11		SLD/3	-2,80		SLD/3	-3,29
	SLD/4	-1,90		SLD/4	-2,03		SLD/4	-2,72		SLD/4	-3,23
	SLD/5	-1,90		SLD/5	-2,02		SLD/5	-2,71		SLD/5	-3,21
	SLD/6	-2,00		SLD/6	-2,12		SLD/6	-2,81		SLD/6	-3,29
	SLD/7	-1,91		SLD/7	-2,04		SLD/7	-2,73		SLD/7	-3,23
	SLD/8	-1,91		SLD/8	-2,04		SLD/8	-2,72		SLD/8	-3,21
	SLD/9	-1,99		SLD/9	-2,11		SLD/9	-2,78		SLD/9	-3,25
	SLD/10	-1,90		SLD/10	-2,02		SLD/10	-2,70		SLD/10	-3,19
	SLD/11	-1,90		SLD/11	-2,01		SLD/11	-2,68		SLD/11	-3,14
	SLD/12	-1,99		SLD/12	-2,09		SLD/12	-2,78		SLD/12	-3,25
	SLD/13	-1,90		SLD/13	-2,01		SLD/13	-2,69		SLD/13	-3,19
	SLD/14	-1,89		SLD/14	-1,99		SLD/14	-2,66		SLD/14	-3,14
X+	SLD/15	-1,35	X+	SLD/15	-1,49	X+	SLD/15	-2,06	X+	SLD/18	-2,58
X-	SLD/24	-1,35	X-	SLD/24	-1,43	X-	SLD/24	-1,83	X-	SLD/25	-2,06
Y+	SLD/40	-1,40	Y+	SLD/31	-1,57	Y+	SLD/31	-2,09	Y+	SLD/34	-2,55
Y-	SLD/46	-1,27	Y-	SLD/37	-1,28	Y-	SLD/37	-1,77	Y-	SLD/36	-2,12
546	SLD/1	-4,40	547	SLD/1	-3,15	548	SLD/1	-2,56	549	SLD/1	-1,89
	SLD/2	-4,34		SLD/2	-3,08		SLD/2	-2,53		SLD/2	-1,86
	SLD/3	-4,44		SLD/3	-3,17		SLD/3	-2,55		SLD/3	-1,89
	SLD/4	-4,37		SLD/4	-3,09		SLD/4	-2,51		SLD/4	-1,85
	SLD/5	-4,33		SLD/5	-3,07		SLD/5	-2,46		SLD/5	-1,82
	SLD/6	-4,47		SLD/6	-3,19		SLD/6	-2,59		SLD/6	-1,91
	SLD/7	-4,40		SLD/7	-3,11		SLD/7	-2,56		SLD/7	-1,87
	SLD/8	-4,38		SLD/8	-3,10		SLD/8	-2,54		SLD/8	-1,85
	SLD/9	-4,37		SLD/9	-3,14		SLD/9	-2,58		SLD/9	-1,90
	SLD/10	-4,30		SLD/10	-3,06		SLD/10	-2,54		SLD/10	-1,86
	SLD/11	-4,21		SLD/11	-3,02		SLD/11	-2,51		SLD/11	-1,84
	SLD/12	-4,34		SLD/12	-3,12		SLD/12	-2,53		SLD/12	-1,88
	SLD/13	-4,27		SLD/13	-3,04		SLD/13	-2,50		SLD/13	-1,84
	SLD/14	-4,16		SLD/14	-2,98		SLD/14	-2,44		SLD/14	-1,80
X+	SLD/15	-3,63	X+	SLD/15	-2,43	X+	SLD/15	-1,66	X+	SLD/15	-1,23
X-	SLD/24	-2,77	X-	SLD/24	-2,07	X-	SLD/24	-2,03	X-	SLD/24	-1,41
Y+	SLD/31	-3,76	Y+	SLD/31	-2,55	Y+	SLD/40	-2,11	Y+	SLD/40	-1,45
Y-	SLD/37	-2,54	Y-	SLD/37	-1,86	Y-	SLD/46	-1,51	Y-	SLD/46	-1,17
550	SLD/1	-1,89	551	SLD/1	-2,28	552	SLD/1	-1,78	553	SLD/1	-1,71
	SLD/2	-1,85		SLD/2	-2,23		SLD/2	-1,74		SLD/2	-1,67
	SLD/3	-1,88		SLD/3	-2,27		SLD/3	-1,78		SLD/3	-1,71
	SLD/4	-1,85		SLD/4	-2,23		SLD/4	-1,74		SLD/4	-1,67
	SLD/5	-1,81		SLD/5	-2,18		SLD/5	-1,71		SLD/5	-1,64
	SLD/6	-1,90		SLD/6	-2,28		SLD/6	-1,78		SLD/6	-1,71
	SLD/7	-1,86		SLD/7	-2,24		SLD/7	-1,75		SLD/7	-1,68

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/8	-1,83		SLD/8	-2,20		SLD/8	-1,72		SLD/8	-1,65
	SLD/9	-1,89		SLD/9	-2,28		SLD/9	-1,78		SLD/9	-1,71
	SLD/10	-1,86		SLD/10	-2,24		SLD/10	-1,75		SLD/10	-1,67
	SLD/11	-1,83		SLD/11	-2,20		SLD/11	-1,72		SLD/11	-1,64
	SLD/12	-1,88		SLD/12	-2,27		SLD/12	-1,78		SLD/12	-1,71
	SLD/13	-1,84		SLD/13	-2,23		SLD/13	-1,74		SLD/13	-1,67
	SLD/14	-1,81		SLD/14	-2,18		SLD/14	-1,71		SLD/14	-1,64
X+	SLD/15	-1,23	X+	SLD/15	-1,48	X+	SLD/15	-1,17	X+	SLD/15	-1,14
X-	SLD/24	-1,35	X-	SLD/24	-1,60	X-	SLD/24	-1,23	X-	SLD/24	-1,16
Y+	SLD/40	-1,36	Y+	SLD/40	-1,60	Y+	SLD/40	-1,23	Y+	SLD/40	-1,17
Y-	SLD/46	-1,21	Y-	SLD/46	-1,48	Y-	SLD/46	-1,16	Y-	SLD/46	-1,12
554	SLD/1	-1,90	555	SLD/1	-1,84	556	SLD/1	-3,10	557	SLD/1	-1,57
	SLD/2	-1,86		SLD/2	-1,80		SLD/2	-3,04		SLD/2	-1,53
	SLD/3	-1,90		SLD/3	-1,84		SLD/3	-3,10		SLD/3	-1,57
	SLD/4	-1,86		SLD/4	-1,81		SLD/4	-3,04		SLD/4	-1,53
	SLD/5	-1,82		SLD/5	-1,77		SLD/5	-2,98		SLD/5	-1,51
	SLD/6	-1,90		SLD/6	-1,84		SLD/6	-3,10		SLD/6	-1,57
	SLD/7	-1,86		SLD/7	-1,81		SLD/7	-3,05		SLD/7	-1,54
	SLD/8	-1,83		SLD/8	-1,78		SLD/8	-2,99		SLD/8	-1,51
	SLD/9	-1,89		SLD/9	-1,84		SLD/9	-3,09		SLD/9	-1,57
	SLD/10	-1,86		SLD/10	-1,80		SLD/10	-3,04		SLD/10	-1,53
	SLD/11	-1,82		SLD/11	-1,77		SLD/11	-2,97		SLD/11	-1,51
	SLD/12	-1,89		SLD/12	-1,84		SLD/12	-3,09		SLD/12	-1,57
	SLD/13	-1,86		SLD/13	-1,80		SLD/13	-3,04		SLD/13	-1,53
	SLD/14	-1,82		SLD/14	-1,76		SLD/14	-2,97		SLD/14	-1,50
X+	SLD/18	-1,28	X+	SLD/18	-1,25	X+	SLD/18	-2,10	X+	SLD/18	-1,06
X-	SLD/25	-1,26	X-	SLD/25	-1,22	X-	SLD/25	-2,05	X-	SLD/25	-1,04
Y+	SLD/34	-1,29	Y+	SLD/34	-1,26	Y+	SLD/34	-2,12	Y+	SLD/34	-1,08
Y-	SLD/36	-1,23	Y-	SLD/36	-1,19	Y-	SLD/36	-2,00	Y-	SLD/36	-1,01
558	SLD/1	-1,60	559	SLD/1	-1,87	560	SLD/1	-1,28	561	SLD/1	-2,11
	SLD/2	-1,57		SLD/2	-1,84		SLD/2	-1,24		SLD/2	-2,06
	SLD/3	-1,60		SLD/3	-1,87		SLD/3	-1,28		SLD/3	-2,10
	SLD/4	-1,57		SLD/4	-1,84		SLD/4	-1,24		SLD/4	-2,06
	SLD/5	-1,54		SLD/5	-1,80		SLD/5	-1,22		SLD/5	-2,02
	SLD/6	-1,61		SLD/6	-1,88		SLD/6	-1,28		SLD/6	-2,11
	SLD/7	-1,57		SLD/7	-1,85		SLD/7	-1,24		SLD/7	-2,07
	SLD/8	-1,55		SLD/8	-1,81		SLD/8	-1,23		SLD/8	-2,03
	SLD/9	-1,60		SLD/9	-1,87		SLD/9	-1,28		SLD/9	-2,11
	SLD/10	-1,57		SLD/10	-1,84		SLD/10	-1,24		SLD/10	-2,07
	SLD/11	-1,54		SLD/11	-1,80		SLD/11	-1,23		SLD/11	-2,02
	SLD/12	-1,60		SLD/12	-1,87		SLD/12	-1,28		SLD/12	-2,10
	SLD/13	-1,56		SLD/13	-1,83		SLD/13	-1,24		SLD/13	-2,06
	SLD/14	-1,53		SLD/14	-1,79		SLD/14	-1,22		SLD/14	-2,01
X+	SLD/15	-1,08	X+	SLD/15	-1,26	X+	SLD/15	-0,85	X+	SLD/15	-1,41
X-	SLD/24	-1,08	X-	SLD/24	-1,27	X-	SLD/24	-0,86	X-	SLD/24	-1,43
Y+	SLD/31	-1,11	Y+	SLD/40	-1,31	Y+	SLD/40	-0,88	Y+	SLD/40	-1,47
Y-	SLD/37	-1,03	Y-	SLD/46	-1,19	Y-	SLD/46	-0,83	Y-	SLD/46	-1,34
562	SLD/1	-0,94	563	SLD/1	-0,77	564	SLD/1	-0,77	565	SLD/1	-0,99
	SLD/2	-0,90		SLD/2	-0,73		SLD/2	-0,73		SLD/2	-0,95
	SLD/3	-0,94		SLD/3	-0,77		SLD/3	-0,77		SLD/3	-0,99
	SLD/4	-0,90		SLD/4	-0,73		SLD/4	-0,73		SLD/4	-0,95
	SLD/5	-0,89		SLD/5	-0,73		SLD/5	-0,73		SLD/5	-0,94
	SLD/6	-0,94		SLD/6	-0,77		SLD/6	-0,77		SLD/6	-1,00
	SLD/7	-0,90		SLD/7	-0,73		SLD/7	-0,73		SLD/7	-0,96
	SLD/8	-0,90		SLD/8	-0,73		SLD/8	-0,74		SLD/8	-0,96
	SLD/9	-0,94		SLD/9	-0,77		SLD/9	-0,77		SLD/9	-0,99
	SLD/10	-0,90		SLD/10	-0,73		SLD/10	-0,73		SLD/10	-0,95
	SLD/11	-0,90		SLD/11	-0,73		SLD/11	-0,73		SLD/11	-0,94
	SLD/12	-0,94		SLD/12	-0,77		SLD/12	-0,77		SLD/12	-0,98
	SLD/13	-0,90		SLD/13	-0,73		SLD/13	-0,73		SLD/13	-0,94
	SLD/14	-0,89		SLD/14	-0,73		SLD/14	-0,73		SLD/14	-0,93
X+	SLD/15	-0,61	X+	SLD/15	-0,49	X+	SLD/15	-0,51	X+	SLD/15	-0,70
X-	SLD/24	-0,63	X-	SLD/24	-0,52	X-	SLD/24	-0,53	X-	SLD/24	-0,67
Y+	SLD/40	-0,63	Y+	SLD/40	-0,52	Y+	SLD/40	-0,54	Y+	SLD/31	-0,75
Y-	SLD/46	-0,62	Y-	SLD/46	-0,51	Y-	SLD/46	-0,49	Y-	SLD/37	-0,59
566	SLD/1	-1,51	567	SLD/1	-2,39	568	SLD/1	-2,53	569	SLD/1	-1,99
	SLD/2	-1,48		SLD/2	-2,36		SLD/2	-2,50		SLD/2	-1,95
	SLD/3	-1,52		SLD/3	-2,41		SLD/3	-2,51		SLD/3	-1,98
	SLD/4	-1,48		SLD/4	-2,38		SLD/4	-2,47		SLD/4	-1,94
	SLD/5	-1,47		SLD/5	-2,35		SLD/5	-2,42		SLD/5	-1,90
	SLD/6	-1,53		SLD/6	-2,43		SLD/6	-2,50		SLD/6	-1,97
	SLD/7	-1,50		SLD/7	-2,40		SLD/7	-2,46		SLD/7	-1,94
	SLD/8	-1,49		SLD/8	-2,39		SLD/8	-2,40		SLD/8	-1,90
	SLD/9	-1,51		SLD/9	-2,37		SLD/9	-2,56		SLD/9	-2,00
	SLD/10	-1,47		SLD/10	-2,34		SLD/10	-2,53		SLD/10	-1,97
	SLD/11	-1,44		SLD/11	-2,28		SLD/11	-2,51		SLD/11	-1,95
	SLD/12	-1,49		SLD/12	-2,34		SLD/12	-2,57		SLD/12	-2,01
	SLD/13	-1,45		SLD/13	-2,31		SLD/13	-2,54		SLD/13	-1,97

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD											
Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
	SLD/14	-1,42		SLD/14	-2,24		SLD/14	-2,52		SLD/14	-1,96
X+	SLD/15	-1,18	X+	SLD/15	-2,00	X+	SLD/21	-1,54	X+	SLD/21	-1,23
X-	SLD/24	-1,00	X-	SLD/24	-1,53	X-	SLD/30	-2,18	X-	SLD/30	-1,59
Y+	SLD/31	-1,26	Y+	SLD/31	-2,13	Y+	SLD/40	-1,50	Y+	SLD/40	-1,24
Y-	SLD/37	-0,85	Y-	SLD/37	-1,29	Y-	SLD/46	-2,20	Y-	SLD/46	-1,58
570	SLD/1	-1,95	571	SLD/1	-2,04	572	SLD/1	-2,48	573	SLD/1	-2,09
	SLD/2	-1,91		SLD/2	-2,01		SLD/2	-2,44		SLD/2	-2,05
	SLD/3	-1,94		SLD/3	-2,04		SLD/3	-2,48		SLD/3	-2,08
	SLD/4	-1,90		SLD/4	-2,00		SLD/4	-2,44		SLD/4	-2,05
	SLD/5	-1,87		SLD/5	-1,96		SLD/5	-2,39		SLD/5	-2,00
	SLD/6	-1,94		SLD/6	-2,04		SLD/6	-2,45		SLD/6	-2,09
	SLD/7	-1,90		SLD/7	-2,00		SLD/7	-2,41		SLD/7	-2,05
	SLD/8	-1,87		SLD/8	-1,96		SLD/8	-2,35		SLD/8	-2,01
	SLD/9	-1,96		SLD/9	-2,05		SLD/9	-2,48		SLD/9	-2,10
	SLD/10	-1,92		SLD/10	-2,02		SLD/10	-2,45		SLD/10	-2,06
	SLD/11	-1,90		SLD/11	-1,99		SLD/11	-2,41		SLD/11	-2,03
	SLD/12	-1,96		SLD/12	-2,05		SLD/12	-2,51		SLD/12	-2,09
	SLD/13	-1,92		SLD/13	-2,01		SLD/13	-2,47		SLD/13	-2,06
	SLD/14	-1,90		SLD/14	-1,98		SLD/14	-2,44		SLD/14	-2,02
X+	SLD/21	-1,23	X+	SLD/20	-1,29	X+	SLD/21	-1,72	X+	SLD/20	-1,33
X-	SLD/30	-1,46	X-	SLD/27	-1,49	X-	SLD/30	-1,82	X-	SLD/27	-1,50
Y+	SLD/40	-1,26	Y+	SLD/41	-1,35	Y+	SLD/40	-1,44	Y+	SLD/41	-1,40
Y-	SLD/46	-1,44	Y-	SLD/43	-1,46	Y-	SLD/46	-1,97	Y-	SLD/43	-1,46
574	SLD/1	-1,97	575	SLD/1	-2,11	576	SLD/1	-2,29	577	SLD/1	-2,49
	SLD/2	-1,93		SLD/2	-2,07		SLD/2	-2,25		SLD/2	-2,45
	SLD/3	-1,97		SLD/3	-2,10		SLD/3	-2,28		SLD/3	-2,49
	SLD/4	-1,93		SLD/4	-2,07		SLD/4	-2,25		SLD/4	-2,45
	SLD/5	-1,89		SLD/5	-2,02		SLD/5	-2,20		SLD/5	-2,40
	SLD/6	-1,97		SLD/6	-2,12		SLD/6	-2,27		SLD/6	-2,48
	SLD/7	-1,93		SLD/7	-2,08		SLD/7	-2,23		SLD/7	-2,44
	SLD/8	-1,90		SLD/8	-2,05		SLD/8	-2,18		SLD/8	-2,38
	SLD/9	-1,98		SLD/9	-2,12		SLD/9	-2,29		SLD/9	-2,49
	SLD/10	-1,94		SLD/10	-2,08		SLD/10	-2,25		SLD/10	-2,45
	SLD/11	-1,91		SLD/11	-2,05		SLD/11	-2,21		SLD/11	-2,40
	SLD/12	-1,97		SLD/12	-2,10		SLD/12	-2,30		SLD/12	-2,50
	SLD/13	-1,93		SLD/13	-2,07		SLD/13	-2,26		SLD/13	-2,46
	SLD/14	-1,90		SLD/14	-2,03		SLD/14	-2,23		SLD/14	-2,42
X+	SLD/18	-1,26	X+	SLD/18	-1,36	X+	SLD/21	-1,57	X+	SLD/21	-1,69
X-	SLD/25	-1,40	X-	SLD/25	-1,53	X-	SLD/30	-1,60	X-	SLD/30	-1,70
Y+	SLD/41	-1,36	Y+	SLD/41	-1,52	Y+	SLD/40	-1,40	Y+	SLD/40	-1,58
Y-	SLD/43	-1,34	Y-	SLD/43	-1,39	Y-	SLD/46	-1,69	Y-	SLD/46	-1,77
578	SLD/1	-1,81	579	SLD/1	-1,80	580	SLD/1	-2,41	581	SLD/1	-2,44
	SLD/2	-1,78		SLD/2	-1,76		SLD/2	-2,36		SLD/2	-2,39
	SLD/3	-1,81		SLD/3	-1,80		SLD/3	-2,41		SLD/3	-2,44
	SLD/4	-1,78		SLD/4	-1,76		SLD/4	-2,36		SLD/4	-2,40
	SLD/5	-1,74		SLD/5	-1,73		SLD/5	-2,31		SLD/5	-2,35
	SLD/6	-1,81		SLD/6	-1,80		SLD/6	-2,40		SLD/6	-2,43
	SLD/7	-1,77		SLD/7	-1,76		SLD/7	-2,35		SLD/7	-2,38
	SLD/8	-1,74		SLD/8	-1,72		SLD/8	-2,30		SLD/8	-2,32
	SLD/9	-1,81		SLD/9	-1,80		SLD/9	-2,40		SLD/9	-2,43
	SLD/10	-1,78		SLD/10	-1,76		SLD/10	-2,35		SLD/10	-2,38
	SLD/11	-1,74		SLD/11	-1,72		SLD/11	-2,30		SLD/11	-2,33
	SLD/12	-1,82		SLD/12	-1,80		SLD/12	-2,41		SLD/12	-2,44
	SLD/13	-1,78		SLD/13	-1,76		SLD/13	-2,36		SLD/13	-2,40
	SLD/14	-1,75		SLD/14	-1,73		SLD/14	-2,32		SLD/14	-2,35
X+	SLD/21	-1,22	X+	SLD/21	-1,22	X+	SLD/21	-1,66	X+	SLD/21	-1,71
X-	SLD/30	-1,22	X-	SLD/30	-1,19	X-	SLD/30	-1,56	X-	SLD/30	-1,56
Y+	SLD/31	-1,16	Y+	SLD/31	-1,17	Y+	SLD/31	-1,56	Y+	SLD/31	-1,56
Y-	SLD/37	-1,25	Y-	SLD/37	-1,23	Y-	SLD/37	-1,66	Y-	SLD/37	-1,71
582	SLD/1	-2,08	583	SLD/1	-2,07	584	SLD/1	-3,16	585	SLD/1	-2,08
	SLD/2	-2,04		SLD/2	-2,03		SLD/2	-3,12		SLD/2	-2,03
	SLD/3	-2,09		SLD/3	-2,08		SLD/3	-3,17		SLD/3	-2,08
	SLD/4	-2,05		SLD/4	-2,04		SLD/4	-3,13		SLD/4	-2,04
	SLD/5	-2,01		SLD/5	-2,00		SLD/5	-3,08		SLD/5	-2,01
	SLD/6	-2,07		SLD/6	-2,06		SLD/6	-3,10		SLD/6	-2,06
	SLD/7	-2,03		SLD/7	-2,02		SLD/7	-3,06		SLD/7	-2,01
	SLD/8	-1,98		SLD/8	-1,96		SLD/8	-2,97		SLD/8	-1,97
	SLD/9	-2,07		SLD/9	-2,07		SLD/9	-3,15		SLD/9	-2,07
	SLD/10	-2,04		SLD/10	-2,03		SLD/10	-3,11		SLD/10	-2,03
	SLD/11	-1,99		SLD/11	-1,98		SLD/11	-3,05		SLD/11	-2,00
	SLD/12	-2,09		SLD/12	-2,09		SLD/12	-3,22		SLD/12	-2,10
	SLD/13	-2,05		SLD/13	-2,05		SLD/13	-3,18		SLD/13	-2,05
	SLD/14	-2,01		SLD/14	-2,02		SLD/14	-3,16		SLD/14	-2,04
X+	SLD/21	-1,49	X+	SLD/21	-1,52	X+	SLD/20	-2,48	X+	SLD/20	-1,54
X-	SLD/30	-1,33	X-	SLD/30	-1,34	X-	SLD/27	-2,21	X-	SLD/27	-1,41
Y+	SLD/31	-1,30	Y+	SLD/31	-1,24	Y+	SLD/34	-1,68	Y+	SLD/34	-1,24
Y-	SLD/37	-1,51	Y-	SLD/37	-1,58	Y-	SLD/36	-2,78	Y-	SLD/36	-1,64

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

RISULTANTI SOLLECITAZIONI NODI PLATEE - SLD

Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)	Nod3d N.ro	Combinazione N.ro	Fz (t)
586	SLD/1	-1,57	587	SLD/1	-1,63	588	SLD/1	-1,97	589	SLD/1	-2,30
	SLD/2	-1,52		SLD/2	-1,59		SLD/2	-1,92		SLD/2	-2,26
	SLD/3	-1,57		SLD/3	-1,64		SLD/3	-1,97		SLD/3	-2,30
	SLD/4	-1,52		SLD/4	-1,59		SLD/4	-1,93		SLD/4	-2,26
	SLD/5	-1,51		SLD/5	-1,57		SLD/5	-1,90		SLD/5	-2,23
	SLD/6	-1,56		SLD/6	-1,64		SLD/6	-1,97		SLD/6	-2,31
	SLD/7	-1,52		SLD/7	-1,59		SLD/7	-1,93		SLD/7	-2,27
	SLD/8	-1,50		SLD/8	-1,58		SLD/8	-1,90		SLD/8	-2,23
	SLD/9	-1,56		SLD/9	-1,63		SLD/9	-1,96		SLD/9	-2,30
	SLD/10	-1,52		SLD/10	-1,59		SLD/10	-1,92		SLD/10	-2,26
	SLD/11	-1,50		SLD/11	-1,57		SLD/11	-1,89		SLD/11	-2,21
	SLD/12	-1,57		SLD/12	-1,63		SLD/12	-1,96		SLD/12	-2,29
	SLD/13	-1,52		SLD/13	-1,58		SLD/13	-1,92		SLD/13	-2,25
	SLD/14	-1,51		SLD/14	-1,56		SLD/14	-1,88		SLD/14	-2,20
X+	SLD/21	-1,09	X+	SLD/15	-1,13	X+	SLD/15	-1,37	X+	SLD/15	-1,62
X-	SLD/30	-1,03	X-	SLD/24	-1,09	X-	SLD/24	-1,31	X-	SLD/24	-1,52
Y+	SLD/31	-1,04	Y+	SLD/31	-1,15	Y+	SLD/31	-1,40	Y+	SLD/31	-1,64
Y-	SLD/37	-1,08	Y-	SLD/37	-1,06	Y-	SLD/37	-1,27	Y-	SLD/37	-1,50
590	SLD/1	-2,56	591	SLD/1	-2,42	592	SLD/1	-2,68	593	SLD/1	-2,34
	SLD/2	-2,52		SLD/2	-2,38		SLD/2	-2,65		SLD/2	-2,30
	SLD/3	-2,57		SLD/3	-2,44		SLD/3	-2,70		SLD/3	-2,34
	SLD/4	-2,53		SLD/4	-2,40		SLD/4	-2,67		SLD/4	-2,30
	SLD/5	-2,48		SLD/5	-2,36		SLD/5	-2,64		SLD/5	-2,25
	SLD/6	-2,58		SLD/6	-2,45		SLD/6	-2,73		SLD/6	-2,35
	SLD/7	-2,53		SLD/7	-2,41		SLD/7	-2,69		SLD/7	-2,31
	SLD/8	-2,50		SLD/8	-2,39		SLD/8	-2,68		SLD/8	-2,27
	SLD/9	-2,56		SLD/9	-2,41		SLD/9	-2,66		SLD/9	-2,34
	SLD/10	-2,51		SLD/10	-2,37		SLD/10	-2,63		SLD/10	-2,30
	SLD/11	-2,46		SLD/11	-2,33		SLD/11	-2,57		SLD/11	-2,25
	SLD/12	-2,55		SLD/12	-2,40		SLD/12	-2,64		SLD/12	-2,33
	SLD/13	-2,51		SLD/13	-2,36		SLD/13	-2,60		SLD/13	-2,29
	SLD/14	-2,45		SLD/14	-2,30		SLD/14	-2,53		SLD/14	-2,24
X+	SLD/15	-1,86	X+	SLD/15	-1,88	X+	SLD/15	-2,26	X+	SLD/15	-1,58
X-	SLD/24	-1,69	X-	SLD/24	-1,59	X-	SLD/24	-1,74	X-	SLD/24	-1,59
Y+	SLD/31	-1,89	Y+	SLD/31	-1,94	Y+	SLD/31	-2,37	Y+	SLD/40	-1,64
Y-	SLD/37	-1,65	Y-	SLD/37	-1,49	Y-	SLD/37	-1,55	Y-	SLD/46	-1,48
594	SLD/1	-1,50	595	SLD/1	-2,34	596	SLD/1	-1,08	597	SLD/1	-0,86
	SLD/2	-1,46		SLD/2	-2,29		SLD/2	-1,04		SLD/2	-0,82
	SLD/3	-1,50		SLD/3	-2,34		SLD/3	-1,08		SLD/3	-0,86
	SLD/4	-1,46		SLD/4	-2,29		SLD/4	-1,04		SLD/4	-0,82
	SLD/5	-1,44		SLD/5	-2,24		SLD/5	-1,03		SLD/5	-0,82
	SLD/6	-1,50		SLD/6	-2,33		SLD/6	-1,08		SLD/6	-0,86
	SLD/7	-1,46		SLD/7	-2,29		SLD/7	-1,04		SLD/7	-0,82
	SLD/8	-1,43		SLD/8	-2,23		SLD/8	-1,03		SLD/8	-0,82
	SLD/9	-1,50		SLD/9	-2,33		SLD/9	-1,08		SLD/9	-0,86
	SLD/10	-1,46		SLD/10	-2,29		SLD/10	-1,04		SLD/10	-0,82
	SLD/11	-1,43		SLD/11	-2,23		SLD/11	-1,03		SLD/11	-0,82
	SLD/12	-1,50		SLD/12	-2,34		SLD/12	-1,08		SLD/12	-0,86
	SLD/13	-1,46		SLD/13	-2,30		SLD/13	-1,04		SLD/13	-0,82
	SLD/14	-1,44		SLD/14	-2,25		SLD/14	-1,03		SLD/14	-0,82
X+	SLD/20	-1,02	X+	SLD/20	-1,59	X+	SLD/20	-0,72	X+	SLD/21	-0,56
X-	SLD/27	-0,97	X-	SLD/27	-1,51	X-	SLD/27	-0,71	X-	SLD/30	-0,57
Y+	SLD/34	-0,98	Y+	SLD/34	-1,51	Y+	SLD/34	-0,71	Y+	SLD/40	-0,56
Y-	SLD/36	-1,01	Y-	SLD/36	-1,59	Y-	SLD/36	-0,72	Y-	SLD/46	-0,57
598	SLD/1	-0,83	599	SLD/1	-1,03	600	SLD/1	-1,55	601	SLD/1	-2,41
	SLD/2	-0,79		SLD/2	-0,99		SLD/2	-1,51		SLD/2	-2,38
	SLD/3	-0,83		SLD/3	-1,03		SLD/3	-1,55		SLD/3	-2,43
	SLD/4	-0,79		SLD/4	-0,99		SLD/4	-1,52		SLD/4	-2,40
	SLD/5	-0,79		SLD/5	-0,99		SLD/5	-1,50		SLD/5	-2,37
	SLD/6	-0,83		SLD/6	-1,02		SLD/6	-1,53		SLD/6	-2,37
	SLD/7	-0,79		SLD/7	-0,98		SLD/7	-1,49		SLD/7	-2,33
	SLD/8	-0,78		SLD/8	-0,97		SLD/8	-1,45		SLD/8	-2,26
	SLD/9	-0,83		SLD/9	-1,03		SLD/9	-1,54		SLD/9	-2,40
	SLD/10	-0,79		SLD/10	-0,99		SLD/10	-1,50		SLD/10	-2,36
	SLD/11	-0,79		SLD/11	-0,98		SLD/11	-1,48		SLD/11	-2,31
	SLD/12	-0,83		SLD/12	-1,04		SLD/12	-1,57		SLD/12	-2,46
	SLD/13	-0,79		SLD/13	-1,00		SLD/13	-1,53		SLD/13	-2,42
	SLD/14	-0,79		SLD/14	-1,00		SLD/14	-1,53		SLD/14	-2,41
X+	SLD/20	-0,55	X+	SLD/20	-0,73	X+	SLD/20	-1,22	X+	SLD/20	-2,04
X-	SLD/27	-0,56	X-	SLD/27	-0,71	X-	SLD/27	-1,05	X-	SLD/27	-1,61
Y+	SLD/41	-0,53	Y+	SLD/34	-0,62	Y+	SLD/34	-0,90	Y+	SLD/34	-1,38
Y-	SLD/43	-0,57	Y-	SLD/36	-0,78	Y-	SLD/36	-1,30	Y-	SLD/36	-2,18

PORTANZA GLOBALE PIASTRE - MOLTIPLICATORI DI COLLASSO - SLU

Comb	DRENATE				NON DRENATE				RISULTATI	
	Result	Resist	Moltip.	%PI.	Result	Resist	Moltip.	%PI.	Moltip.	STATUS

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RELAZIONE GEOTECNICA

N.ro	(t)	(t)	Collasso	Moll	(t)	(t)	Collasso	Moll	Minimo	(m)
A1 / 1	2015	2015	1,000	0					1,000	OK
A1 / 2	1968	1968	1,000	0						OK
A1 / 3	2015	2015	1,000	0						OK
A1 / 4	1968	1968	1,000	0						OK
A1 / 5	1933	1933	1,000	0						OK
A1 / 6	2015	2015	1,000	0						OK
A1 / 7	1968	1968	1,000	0						OK
A1 / 8	1933	1933	1,000	0						OK
A1 / 9	2015	2015	1,000	0						OK
A1 / 10	1968	1968	1,000	0						OK
A1 / 11	1933	1933	1,000	0						OK
A1 / 12	2015	2015	1,000	0						OK
A1 / 13	1968	1968	1,000	0						OK
A1 / 14	1933	1933	1,000	0						OK
A1 / 15	1336	1336	1,000	0						OK
A1 / 16	1336	1336	1,000	0						OK
A1 / 17	1336	1336	1,000	0						OK
A1 / 18	1336	1336	1,000	0						OK
A1 / 19	1336	1336	1,000	0						OK
A1 / 20	1336	1336	1,000	0						OK
A1 / 21	1336	1336	1,000	0						OK
A1 / 22	1336	1336	1,000	0						OK
A1 / 23	1336	1336	1,000	0						OK
A1 / 24	1336	1336	1,000	0						OK
A1 / 25	1336	1336	1,000	0						OK
A1 / 26	1336	1336	1,000	0						OK
A1 / 27	1336	1336	1,000	0						OK
A1 / 28	1336	1336	1,000	0						OK
A1 / 29	1336	1336	1,000	0						OK
A1 / 30	1336	1336	1,000	0						OK
A1 / 31	1336	1336	1,000	0						OK
A1 / 32	1336	1336	1,000	0						OK
A1 / 33	1336	1336	1,000	0						OK
A1 / 34	1336	1336	1,000	0						OK
A1 / 35	1336	1336	1,000	0						OK
A1 / 36	1336	1336	1,000	0						OK
A1 / 37	1336	1336	1,000	0						OK
A1 / 38	1336	1336	1,000	0						OK
A1 / 39	1336	1336	1,000	0						OK
A1 / 40	1336	1336	1,000	0						OK
A1 / 41	1336	1336	1,000	0						OK
A1 / 42	1336	1336	1,000	0						OK
A1 / 43	1336	1336	1,000	0						OK
A1 / 44	1336	1336	1,000	0						OK
A1 / 45	1336	1336	1,000	0						OK
A1 / 46	1336	1336	1,000	0						OK

PORTANZA GLOBALE PIASTRE - ABBASSAMENTI COMBINAZ.: A1/1														
Nodo3d N.ro	DRENATE		NON DRENATE		Nodo3d N.ro	DRENATE		NON DRENATE		Nodo3d N.ro	DRENATE		NON DRENATE	
	SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI		SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI		SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI
1	-0,042	ELAST.			3	-0,039	ELAST.			4	-0,031	ELAST.		
5	-0,031	ELAST.			7	-0,031	ELAST.			8	-0,039	ELAST.		
9	-0,031	ELAST.			10	-0,055	ELAST.			12	-0,045	ELAST.		
14	-0,032	ELAST.			15	-0,039	ELAST.			16	-0,031	ELAST.		
17	-0,032	ELAST.			18	-0,035	ELAST.			19	-0,046	ELAST.		
20	-0,044	ELAST.			21	-0,035	ELAST.			22	-0,030	ELAST.		
23	-0,030	ELAST.			24	-0,038	ELAST.			25	-0,048	ELAST.		
31	-0,054	ELAST.			32	-0,061	ELAST.			65	-0,043	ELAST.		
66	-0,041	ELAST.			67	-0,031	ELAST.			68	-0,032	ELAST.		
69	-0,031	ELAST.			70	-0,037	ELAST.			71	-0,034	ELAST.		
72	-0,032	ELAST.			73	-0,031	ELAST.			74	-0,035	ELAST.		
75	-0,033	ELAST.			76	-0,031	ELAST.			77	-0,031	ELAST.		
78	-0,036	ELAST.			79	-0,033	ELAST.			80	-0,031	ELAST.		
81	-0,031	ELAST.			82	-0,037	ELAST.			83	-0,034	ELAST.		
84	-0,033	ELAST.			85	-0,031	ELAST.			86	-0,031	ELAST.		
87	-0,031	ELAST.			88	-0,031	ELAST.			89	-0,032	ELAST.		

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RELAZIONE GEOTECNICA

PORTANZA GLOBALE PIASTRE - ABBASSAMENTI COMBINAZ.: A1/I															
Nodo3d N.ro	DRENATE		NON DRENATE		Nodo3d N.ro	DRENATE		NON DRENATE		Nodo3d N.ro	DRENATE		NON DRENATE		Nodo3d N.ro
	SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI		SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI		SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI	
90	-0,032	ELAST.			91	-0,032	ELAST.			92	-0,033	ELAST.			
93	-0,034	ELAST.			94	-0,040	ELAST.			95	-0,041	ELAST.			
96	-0,042	ELAST.			97	-0,043	ELAST.			98	-0,030	ELAST.			
99	-0,031	ELAST.			100	-0,032	ELAST.			101	-0,033	ELAST.			
102	-0,031	ELAST.			103	-0,030	ELAST.			104	-0,030	ELAST.			
105	-0,030	ELAST.			106	-0,031	ELAST.			107	-0,030	ELAST.			
108	-0,030	ELAST.			109	-0,030	ELAST.			110	-0,036	ELAST.			
111	-0,037	ELAST.			112	-0,038	ELAST.			113	-0,038	ELAST.			
114	-0,036	ELAST.			115	-0,038	ELAST.			116	-0,041	ELAST.			
117	-0,044	ELAST.			118	-0,030	ELAST.			119	-0,030	ELAST.			
120	-0,033	ELAST.			121	-0,037	ELAST.			122	-0,030	ELAST.			
123	-0,031	ELAST.			124	-0,033	ELAST.			125	-0,037	ELAST.			
126	-0,036	ELAST.			127	-0,035	ELAST.			128	-0,037	ELAST.			
129	-0,042	ELAST.			130	-0,052	ELAST.			131	-0,052	ELAST.			
132	-0,053	ELAST.			133	-0,056	ELAST.			134	-0,038	ELAST.			
135	-0,039	ELAST.			136	-0,040	ELAST.			137	-0,043	ELAST.			
138	-0,047	ELAST.			139	-0,051	ELAST.			140	-0,039	ELAST.			
141	-0,041	ELAST.			142	-0,043	ELAST.			143	-0,037	ELAST.			
144	-0,035	ELAST.			145	-0,033	ELAST.			146	-0,032	ELAST.			
147	-0,031	ELAST.			148	-0,031	ELAST.			149	-0,031	ELAST.			
150	-0,031	ELAST.			151	-0,031	ELAST.			152	-0,031	ELAST.			
153	-0,031	ELAST.			154	-0,030	ELAST.			155	-0,030	ELAST.			
156	-0,031	ELAST.			157	-0,031	ELAST.			158	-0,032	ELAST.			
159	-0,034	ELAST.			160	-0,037	ELAST.			161	-0,037	ELAST.			
162	-0,034	ELAST.			163	-0,032	ELAST.			164	-0,031	ELAST.			
165	-0,031	ELAST.			166	-0,031	ELAST.			167	-0,030	ELAST.			
168	-0,031	ELAST.			169	-0,032	ELAST.			170	-0,032	ELAST.			
171	-0,032	ELAST.			172	-0,032	ELAST.			173	-0,033	ELAST.			
174	-0,034	ELAST.			175	-0,036	ELAST.			176	-0,039	ELAST.			
177	-0,041	ELAST.			178	-0,043	ELAST.			179	-0,043	ELAST.			
180	-0,040	ELAST.			181	-0,037	ELAST.			182	-0,033	ELAST.			
183	-0,032	ELAST.			184	-0,030	ELAST.			185	-0,029	ELAST.			
186	-0,029	ELAST.			187	-0,029	ELAST.			188	-0,030	ELAST.			
189	-0,031	ELAST.			190	-0,033	ELAST.			191	-0,035	ELAST.			
192	-0,043	ELAST.			193	-0,041	ELAST.			194	-0,037	ELAST.			
195	-0,040	ELAST.			196	-0,038	ELAST.			197	-0,039	ELAST.			
198	-0,036	ELAST.			199	-0,035	ELAST.			200	-0,033	ELAST.			
201	-0,035	ELAST.			202	-0,037	ELAST.			203	-0,033	ELAST.			
204	-0,040	ELAST.			205	-0,041	ELAST.			206	-0,037	ELAST.			
207	-0,036	ELAST.			208	-0,034	ELAST.			209	-0,033	ELAST.			
210	-0,035	ELAST.			211	-0,032	ELAST.			212	-0,032	ELAST.			
213	-0,031	ELAST.			214	-0,031	ELAST.			215	-0,031	ELAST.			
216	-0,031	ELAST.			217	-0,031	ELAST.			218	-0,034	ELAST.			
219	-0,033	ELAST.			220	-0,031	ELAST.			221	-0,033	ELAST.			
222	-0,037	ELAST.			223	-0,036	ELAST.			224	-0,036	ELAST.			
225	-0,033	ELAST.			226	-0,031	ELAST.			227	-0,031	ELAST.			
228	-0,031	ELAST.			229	-0,032	ELAST.			230	-0,031	ELAST.			
231	-0,031	ELAST.			232	-0,031	ELAST.			233	-0,031	ELAST.			
234	-0,031	ELAST.			235	-0,031	ELAST.			236	-0,031	ELAST.			
237	-0,030	ELAST.			238	-0,031	ELAST.			239	-0,039	ELAST.			
240	-0,039	ELAST.			241	-0,035	ELAST.			242	-0,033	ELAST.			
243	-0,031	ELAST.			244	-0,031	ELAST.			245	-0,035	ELAST.			
246	-0,036	ELAST.			247	-0,033	ELAST.			248	-0,032	ELAST.			
249	-0,030	ELAST.			250	-0,031	ELAST.			251	-0,035	ELAST.			
252	-0,032	ELAST.			253	-0,036	ELAST.			254	-0,034	ELAST.			
255	-0,031	ELAST.			256	-0,030	ELAST.			257	-0,031	ELAST.			
258	-0,030	ELAST.			259	-0,032	ELAST.			260	-0,031	ELAST.			
261	-0,031	ELAST.			262	-0,031	ELAST.			263	-0,031	ELAST.			
264	-0,031	ELAST.			265	-0,031	ELAST.			266	-0,032	ELAST.			
267	-0,031	ELAST.			268	-0,032	ELAST.			269	-0,032	ELAST.			
270	-0,032	ELAST.			271	-0,032	ELAST.			272	-0,032	ELAST.			
273	-0,032	ELAST.			274	-0,032	ELAST.			275	-0,032	ELAST.			
276	-0,031	ELAST.			277	-0,032	ELAST.			278	-0,032	ELAST.			
279	-0,032	ELAST.			280	-0,031	ELAST.			281	-0,032	ELAST.			
282	-0,032	ELAST.			283	-0,030	ELAST.			284	-0,038	ELAST.			
285	-0,035	ELAST.			286	-0,035	ELAST.			287	-0,039	ELAST.			
288	-0,041	ELAST.			289	-0,037	ELAST.			290	-0,032	ELAST.			
291	-0,033	ELAST.			292	-0,030	ELAST.			293	-0,031	ELAST.			
294	-0,036	ELAST.			295	-0,039	ELAST.			296	-0,042	ELAST.			
297	-0,030	ELAST.			298	-0,030	ELAST.			299	-0,030	ELAST.			
300	-0,030	ELAST.			301	-0,031	ELAST.			302	-0,030	ELAST.			
303	-0,030	ELAST.			304	-0,031	ELAST.			305	-0,031	ELAST.			
306	-0,030	ELAST.			307	-0,030	ELAST.			308	-0,030	ELAST.			
309	-0,031	ELAST.			310	-0,030	ELAST.			311	-0,031	ELAST.			
312	-0,034	ELAST.			313	-0,033	ELAST.			314	-0,031	ELAST.			
315	-0,033	ELAST.			316	-0,035	ELAST.			317	-0,037	ELAST.			
318	-0,033	ELAST.			319	-0,030	ELAST.			320	-0,031	ELAST.			
321	-0,031	ELAST.			322	-0,030	ELAST.			323	-0,030	ELAST.			
324	-0,038	ELAST.			325	-0,042	ELAST.			326	-0,045	ELAST.			
327	-0,042	ELAST.			328	-0,039	ELAST.			329	-0,035	ELAST.			
330	-0,032	ELAST.			331	-0,034	ELAST.			332	-0,038	ELAST.			
333	-0,030	ELAST.			334	-0,030	ELAST.			335	-0,030	ELAST.			

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

PORTANZA GLOBALE PIASTRE - ABBASSAMENTI COMBINAZ.: A1/1														
Nodo3d N.ro	DRENATE		NON DRENATE		Nodo3d N.ro	DRENATE		NON DRENATE		Nodo3d N.ro	DRENATE		NON DRENATE	
	SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI		SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI		SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI
336	-0,029	ELAST.			337	-0,030	ELAST.			338	-0,031	ELAST.		
339	-0,029	ELAST.			340	-0,029	ELAST.			341	-0,031	ELAST.		
342	-0,031	ELAST.			343	-0,032	ELAST.			344	-0,031	ELAST.		
345	-0,030	ELAST.			346	-0,031	ELAST.			347	-0,032	ELAST.		
348	-0,030	ELAST.			349	-0,029	ELAST.			350	-0,029	ELAST.		
351	-0,030	ELAST.			352	-0,029	ELAST.			353	-0,030	ELAST.		
354	-0,030	ELAST.			355	-0,031	ELAST.			356	-0,034	ELAST.		
357	-0,037	ELAST.			358	-0,030	ELAST.			359	-0,029	ELAST.		
360	-0,029	ELAST.			361	-0,030	ELAST.			362	-0,032	ELAST.		
363	-0,030	ELAST.			364	-0,029	ELAST.			365	-0,029	ELAST.		
366	-0,029	ELAST.			367	-0,029	ELAST.			368	-0,030	ELAST.		
369	-0,031	ELAST.			370	-0,032	ELAST.			371	-0,033	ELAST.		
372	-0,035	ELAST.			373	-0,038	ELAST.			374	-0,037	ELAST.		
375	-0,036	ELAST.			376	-0,033	ELAST.			377	-0,036	ELAST.		
378	-0,035	ELAST.			379	-0,035	ELAST.			380	-0,033	ELAST.		
381	-0,032	ELAST.			382	-0,036	ELAST.			383	-0,032	ELAST.		
384	-0,029	ELAST.			385	-0,029	ELAST.			386	-0,031	ELAST.		
387	-0,030	ELAST.			388	-0,029	ELAST.			389	-0,031	ELAST.		
390	-0,030	ELAST.			391	-0,029	ELAST.			392	-0,030	ELAST.		
393	-0,033	ELAST.			394	-0,037	ELAST.			395	-0,037	ELAST.		
396	-0,034	ELAST.			397	-0,032	ELAST.			398	-0,030	ELAST.		
399	-0,029	ELAST.			400	-0,030	ELAST.			401	-0,030	ELAST.		
402	-0,031	ELAST.			403	-0,032	ELAST.			404	-0,031	ELAST.		
405	-0,031	ELAST.			406	-0,032	ELAST.			407	-0,031	ELAST.		
408	-0,031	ELAST.			409	-0,032	ELAST.			410	-0,032	ELAST.		
411	-0,032	ELAST.			412	-0,031	ELAST.			413	-0,031	ELAST.		
414	-0,030	ELAST.			415	-0,030	ELAST.			416	-0,031	ELAST.		
417	-0,032	ELAST.			418	-0,032	ELAST.			419	-0,031	ELAST.		
420	-0,033	ELAST.			421	-0,034	ELAST.			422	-0,032	ELAST.		
423	-0,033	ELAST.			424	-0,032	ELAST.			425	-0,030	ELAST.		
426	-0,037	ELAST.			427	-0,036	ELAST.			428	-0,033	ELAST.		
429	-0,032	ELAST.			430	-0,032	ELAST.			431	-0,039	ELAST.		
432	-0,029	ELAST.			433	-0,031	ELAST.			434	-0,030	ELAST.		
435	-0,029	ELAST.			436	-0,031	ELAST.			437	-0,030	ELAST.		
438	-0,029	ELAST.			439	-0,029	ELAST.			440	-0,035	ELAST.		
441	-0,030	ELAST.			442	-0,031	ELAST.			443	-0,030	ELAST.		
444	-0,042	ELAST.			445	-0,038	ELAST.			446	-0,046	ELAST.		
447	-0,033	ELAST.			448	-0,033	ELAST.			449	-0,033	ELAST.		
450	-0,036	ELAST.			451	-0,034	ELAST.			452	-0,032	ELAST.		
453	-0,032	ELAST.			454	-0,033	ELAST.			455	-0,036	ELAST.		
456	-0,033	ELAST.			457	-0,035	ELAST.			458	-0,037	ELAST.		
459	-0,039	ELAST.			460	-0,035	ELAST.			461	-0,038	ELAST.		
462	-0,038	ELAST.			463	-0,041	ELAST.			464	-0,041	ELAST.		
465	-0,044	ELAST.			466	-0,030	ELAST.			467	-0,029	ELAST.		
468	-0,029	ELAST.			469	-0,029	ELAST.			470	-0,030	ELAST.		
471	-0,030	ELAST.			472	-0,030	ELAST.			473	-0,031	ELAST.		
474	-0,030	ELAST.			475	-0,029	ELAST.			476	-0,029	ELAST.		
477	-0,030	ELAST.			478	-0,030	ELAST.			479	-0,033	ELAST.		
480	-0,033	ELAST.			481	-0,036	ELAST.			482	-0,035	ELAST.		
483	-0,034	ELAST.			484	-0,037	ELAST.			485	-0,037	ELAST.		
486	-0,034	ELAST.			487	-0,030	ELAST.			488	-0,029	ELAST.		
489	-0,030	ELAST.			490	-0,032	ELAST.			491	-0,033	ELAST.		
492	-0,035	ELAST.			493	-0,030	ELAST.			494	-0,038	ELAST.		
495	-0,037	ELAST.			496	-0,032	ELAST.			497	-0,031	ELAST.		
498	-0,031	ELAST.			499	-0,035	ELAST.			500	-0,033	ELAST.		
501	-0,032	ELAST.			502	-0,034	ELAST.			503	-0,035	ELAST.		
504	-0,034	ELAST.			505	-0,036	ELAST.			506	-0,040	ELAST.		
507	-0,037	ELAST.			508	-0,025	ELAST.			509	-0,031	ELAST.		
510	-0,032	ELAST.			511	-0,025	ELAST.			512	-0,026	ELAST.		
513	-0,021	ELAST.			514	-0,020	ELAST.			515	-0,020	ELAST.		
516	-0,019	ELAST.			517	-0,017	ELAST.			518	-0,032	ELAST.		
519	-0,027	ELAST.			520	-0,034	ELAST.			521	-0,021	ELAST.		
522	-0,019	ELAST.			523	-0,028	ELAST.			524	-0,026	ELAST.		
525	-0,039	ELAST.			526	-0,037	ELAST.			527	-0,025	ELAST.		
528	-0,019	ELAST.			529	-0,017	ELAST.			530	-0,048	ELAST.		
531	-0,048	ELAST.			532	-0,036	ELAST.			533	-0,050	ELAST.		
534	-0,037	ELAST.			535	-0,029	ELAST.			536	-0,017	ELAST.		
537	-0,020	ELAST.			538	-0,022	ELAST.			539	-0,018	ELAST.		
540	-0,019	ELAST.			541	-0,020	ELAST.			542	-0,026	ELAST.		
543	-0,028	ELAST.			544	-0,037	ELAST.			545	-0,049	ELAST.		
546	-0,052	ELAST.			547	-0,039	ELAST.			548	-0,048	ELAST.		
549	-0,045	ELAST.			550	-0,041	ELAST.			551	-0,041	ELAST.		
552	-0,041	ELAST.			553	-0,040	ELAST.			554	-0,040	ELAST.		
555	-0,040	ELAST.			556	-0,041	ELAST.			557	-0,039	ELAST.		
558	-0,039	ELAST.			559	-0,042	ELAST.			560	-0,033	ELAST.		
561	-0,042	ELAST.			562	-0,025	ELAST.			563	-0,020	ELAST.		
564	-0,020	ELAST.			565	-0,026	ELAST.			566	-0,038	ELAST.		
567	-0,052	ELAST.			568	-0,046	ELAST.			569	-0,043	ELAST.		
570	-0,040	ELAST.			571	-0,039	ELAST.			572	-0,043	ELAST.		
573	-0,039	ELAST.			574	-0,039	ELAST.			575	-0,038	ELAST.		
576	-0,042	ELAST.			577	-0,040	ELAST.			578	-0,038	ELAST.		
579	-0,038	ELAST.			580	-0,038	ELAST.			581	-0,038	ELAST.		

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RELAZIONE GEOTECNICA

PORTANZA GLOBALE PIASTRE - ABBASSAMENTI COMBINAZ.: A1/1														
DRENATE			NON DRENATE			DRENATE			NON DRENATE			DRENATE		
Nodo3d N.ro	SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI		Nodo3d N.ro	SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI		Nodo3d N.ro	SpostZ (cm)	SpostZ/ SpostEI
582	-0,038	ELAST.				583	-0,038	ELAST.				584	-0,050	ELAST.
585	-0,042	ELAST.				586	-0,036	ELAST.				587	-0,036	ELAST.
588	-0,038	ELAST.				589	-0,040	ELAST.				590	-0,042	ELAST.
591	-0,044	ELAST.				592	-0,047	ELAST.				593	-0,044	ELAST.
594	-0,029	ELAST.				595	-0,035	ELAST.				596	-0,023	ELAST.
597	-0,020	ELAST.				598	-0,021	ELAST.				599	-0,027	ELAST.
600	-0,038	ELAST.				601	-0,050	ELAST.						

PORTANZA GLOBALE PIASTRE - MOLTIPLICATORI DI COLLASSO - SLD											
		DRENATE				NON DRENATE				RISULTATI	
Comb N.ro		Risult (t)	Resist (t)	Moltip. Collasso	%Pl. Moll	Risult (t)	Resist (t)	Moltip. Collasso	%Pl. Moll	Moltip. Minimo	STATUS (m)
A1 / 1	2015	2015	1,000	0						1,000	OK
A1 / 2	1968	1968	1,000	0							OK
A1 / 3	2015	2015	1,000	0							OK
A1 / 4	1968	1968	1,000	0							OK
A1 / 5	1933	1933	1,000	0							OK
A1 / 6	2015	2015	1,000	0							OK
A1 / 7	1968	1968	1,000	0							OK
A1 / 8	1933	1933	1,000	0							OK
A1 / 9	2015	2015	1,000	0							OK
A1 / 10	1968	1968	1,000	0							OK
A1 / 11	1933	1933	1,000	0							OK
A1 / 12	2015	2015	1,000	0							OK
A1 / 13	1968	1968	1,000	0							OK
A1 / 14	1933	1933	1,000	0							OK
A1 / 15	1336	1336	1,000	0							OK
A1 / 16	1336	1336	1,000	0							OK
A1 / 17	1336	1336	1,000	0							OK
A1 / 18	1336	1336	1,000	0							OK
A1 / 19	1336	1336	1,000	0							OK
A1 / 20	1336	1336	1,000	0							OK
A1 / 21	1336	1336	1,000	0							OK
A1 / 22	1336	1336	1,000	0							OK
A1 / 23	1336	1336	1,000	0							OK
A1 / 24	1336	1336	1,000	0							OK
A1 / 25	1336	1336	1,000	0							OK
A1 / 26	1336	1336	1,000	0							OK
A1 / 27	1336	1336	1,000	0							OK
A1 / 28	1336	1336	1,000	0							OK
A1 / 29	1336	1336	1,000	0							OK
A1 / 30	1336	1336	1,000	0							OK
A1 / 31	1336	1336	1,000	0							OK
A1 / 32	1336	1336	1,000	0							OK
A1 / 33	1336	1336	1,000	0							OK
A1 / 34	1336	1336	1,000	0							OK
A1 / 35	1336	1336	1,000	0							OK
A1 / 36	1336	1336	1,000	0							OK
A1 / 37	1336	1336	1,000	0							OK
A1 / 38	1336	1336	1,000	0							OK
A1 / 39	1336	1336	1,000	0							OK
A1 / 40	1336	1336	1,000	0							OK
A1 / 41	1336	1336	1,000	0							OK
A1 / 42	1336	1336	1,000	0							OK
A1 / 43	1336	1336	1,000	0							OK
A1 / 44	1336	1336	1,000	0							OK
A1 / 45	1336	1336	1,000	0							OK
A1 / 46	1336	1336	1,000	0							OK

PORTANZA GLOBALE PIASTRE - ABBASSAMENTI COMBINAZ.: SLD/1														
DRENATE			NON DRENATE			DRENATE			NON DRENATE			DRENATE		
Nodo3d	SpostZ	SpostZ/	SpostZ	SpostZ/		Nodo3d	SpostZ	SpostZ/	SpostZ	SpostZ/		Nodo3d	SpostZ	SpostZ/

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RELAZIONE GEOTECNICA

N.ro	(cm)	SpostEI	(cm)	SpostEI	N.ro	(cm)	SpostEI	(cm)	SpostEI	N.ro	(cm)	SpostEI	(cm)	SpostEI
1	-0,042	ELAST.			3	-0,039	ELAST.			4	-0,031	ELAST.		
5	-0,031	ELAST.			7	-0,031	ELAST.			8	-0,039	ELAST.		
9	-0,031	ELAST.			10	-0,055	ELAST.			12	-0,045	ELAST.		
14	-0,032	ELAST.			15	-0,039	ELAST.			16	-0,031	ELAST.		
17	-0,032	ELAST.			18	-0,035	ELAST.			19	-0,046	ELAST.		
20	-0,044	ELAST.			21	-0,035	ELAST.			22	-0,030	ELAST.		
23	-0,030	ELAST.			24	-0,038	ELAST.			25	-0,048	ELAST.		
31	-0,054	ELAST.			32	-0,061	ELAST.			65	-0,043	ELAST.		
66	-0,041	ELAST.			67	-0,031	ELAST.			68	-0,032	ELAST.		
69	-0,031	ELAST.			70	-0,037	ELAST.			71	-0,034	ELAST.		
72	-0,032	ELAST.			73	-0,031	ELAST.			74	-0,035	ELAST.		
75	-0,033	ELAST.			76	-0,031	ELAST.			77	-0,031	ELAST.		
78	-0,036	ELAST.			79	-0,033	ELAST.			80	-0,031	ELAST.		
81	-0,031	ELAST.			82	-0,037	ELAST.			83	-0,034	ELAST.		
84	-0,033	ELAST.			85	-0,031	ELAST.			86	-0,031	ELAST.		
87	-0,031	ELAST.			88	-0,031	ELAST.			89	-0,032	ELAST.		
90	-0,032	ELAST.			91	-0,032	ELAST.			92	-0,033	ELAST.		
93	-0,034	ELAST.			94	-0,040	ELAST.			95	-0,041	ELAST.		
96	-0,042	ELAST.			97	-0,043	ELAST.			98	-0,030	ELAST.		
99	-0,031	ELAST.			100	-0,032	ELAST.			101	-0,033	ELAST.		
102	-0,031	ELAST.			103	-0,030	ELAST.			104	-0,030	ELAST.		
105	-0,030	ELAST.			106	-0,031	ELAST.			107	-0,030	ELAST.		
108	-0,030	ELAST.			109	-0,030	ELAST.			110	-0,036	ELAST.		
111	-0,037	ELAST.			112	-0,038	ELAST.			113	-0,038	ELAST.		
114	-0,036	ELAST.			115	-0,038	ELAST.			116	-0,041	ELAST.		
117	-0,044	ELAST.			118	-0,030	ELAST.			119	-0,030	ELAST.		
120	-0,033	ELAST.			121	-0,037	ELAST.			122	-0,030	ELAST.		
123	-0,031	ELAST.			124	-0,033	ELAST.			125	-0,037	ELAST.		
126	-0,036	ELAST.			127	-0,035	ELAST.			128	-0,037	ELAST.		
129	-0,042	ELAST.			130	-0,052	ELAST.			131	-0,052	ELAST.		
132	-0,053	ELAST.			133	-0,056	ELAST.			134	-0,038	ELAST.		
135	-0,039	ELAST.			136	-0,040	ELAST.			137	-0,043	ELAST.		
138	-0,047	ELAST.			139	-0,051	ELAST.			140	-0,039	ELAST.		
141	-0,041	ELAST.			142	-0,043	ELAST.			143	-0,037	ELAST.		
144	-0,035	ELAST.			145	-0,033	ELAST.			146	-0,032	ELAST.		
147	-0,031	ELAST.			148	-0,031	ELAST.			149	-0,031	ELAST.		
150	-0,031	ELAST.			151	-0,031	ELAST.			152	-0,031	ELAST.		
153	-0,031	ELAST.			154	-0,030	ELAST.			155	-0,030	ELAST.		
156	-0,031	ELAST.			157	-0,031	ELAST.			158	-0,032	ELAST.		
159	-0,034	ELAST.			160	-0,037	ELAST.			161	-0,037	ELAST.		
162	-0,034	ELAST.			163	-0,032	ELAST.			164	-0,031	ELAST.		
165	-0,031	ELAST.			166	-0,031	ELAST.			167	-0,030	ELAST.		
168	-0,031	ELAST.			169	-0,032	ELAST.			170	-0,032	ELAST.		
171	-0,032	ELAST.			172	-0,032	ELAST.			173	-0,033	ELAST.		
174	-0,034	ELAST.			175	-0,036	ELAST.			176	-0,039	ELAST.		
177	-0,041	ELAST.			178	-0,043	ELAST.			179	-0,043	ELAST.		
180	-0,040	ELAST.			181	-0,037	ELAST.			182	-0,033	ELAST.		
183	-0,032	ELAST.			184	-0,030	ELAST.			185	-0,029	ELAST.		
186	-0,029	ELAST.			187	-0,029	ELAST.			188	-0,030	ELAST.		
189	-0,031	ELAST.			190	-0,033	ELAST.			191	-0,035	ELAST.		
192	-0,043	ELAST.			193	-0,041	ELAST.			194	-0,037	ELAST.		
195	-0,040	ELAST.			196	-0,038	ELAST.			197	-0,039	ELAST.		
198	-0,036	ELAST.			199	-0,035	ELAST.			200	-0,033	ELAST.		
201	-0,035	ELAST.			202	-0,037	ELAST.			203	-0,033	ELAST.		
204	-0,040	ELAST.			205	-0,041	ELAST.			206	-0,037	ELAST.		
207	-0,036	ELAST.			208	-0,034	ELAST.			209	-0,033	ELAST.		
210	-0,035	ELAST.			211	-0,032	ELAST.			212	-0,032	ELAST.		
213	-0,031	ELAST.			214	-0,031	ELAST.			215	-0,031	ELAST.		
216	-0,031	ELAST.			217	-0,031	ELAST.			218	-0,034	ELAST.		
219	-0,033	ELAST.			220	-0,031	ELAST.			221	-0,033	ELAST.		
222	-0,037	ELAST.			223	-0,036	ELAST.			224	-0,036	ELAST.		
225	-0,033	ELAST.			226	-0,031	ELAST.			227	-0,031	ELAST.		
228	-0,031	ELAST.			229	-0,032	ELAST.			230	-0,031	ELAST.		
231	-0,031	ELAST.			232	-0,031	ELAST.			233	-0,031	ELAST.		
234	-0,031	ELAST.			235	-0,031	ELAST.			236	-0,031	ELAST.		
237	-0,030	ELAST.			238	-0,031	ELAST.			239	-0,039	ELAST.		
240	-0,039	ELAST.			241	-0,035	ELAST.			242	-0,033	ELAST.		
243	-0,031	ELAST.			244	-0,031	ELAST.			245	-0,035	ELAST.		
246	-0,036	ELAST.			247	-0,033	ELAST.			248	-0,032	ELAST.		
249	-0,030	ELAST.			250	-0,031	ELAST.			251	-0,035	ELAST.		
252	-0,032	ELAST.			253	-0,036	ELAST.			254	-0,034	ELAST.		
255	-0,031	ELAST.			256	-0,030	ELAST.			257	-0,031	ELAST.		
258	-0,030	ELAST.			259	-0,032	ELAST.			260	-0,031	ELAST.		
261	-0,031	ELAST.			262	-0,031	ELAST.			263	-0,031	ELAST.		
264	-0,031	ELAST.			265	-0,031	ELAST.			266	-0,032	ELAST.		
267	-0,031	ELAST.			268	-0,032	ELAST.			269	-0,032	ELAST.		
270	-0,032	ELAST.			271	-0,032	ELAST.			272	-0,032	ELAST.		
273	-0,032	ELAST.			274	-0,032	ELAST.			275	-0,032	ELAST.		
276	-0,031	ELAST.			277	-0,032	ELAST.			278	-0,032	ELAST.		
279	-0,032	ELAST.			280	-0,031	ELAST.			281	-0,032	ELAST.		
282	-0,032	ELAST.			283	-0,030	ELAST.			284	-0,038	ELAST.		
285	-0,035	ELAST.			286	-0,035	ELAST.			287	-0,039	ELAST.		
288	-0,041	ELAST.			289	-0,037	ELAST.			290	-0,032	ELAST.		
291	-0,033	ELAST.			292	-0,030	ELAST.			293	-0,031	ELAST.		
294	-0,036	ELAST.			295	-0,039	ELAST.			296	-0,042	ELAST.		

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

PORTANZA GLOBALE PIASTRE - ABBASSAMENTI COMBINAZ.: SLD/1

		DRENATE		NON DRENATE				DRENATE		NON DRENATE				DRENATE		NON DRENATE	
Nodo3d N.ro	SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI	Nodo3d N.ro	SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI	Nodo3d N.ro	SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI	Nodo3d N.ro	SpostZ (cm)	SpostZ/ SpostEI
297	-0,030	ELAST.			298	-0,030	ELAST.			299	-0,030	ELAST.			299	-0,030	ELAST.
300	-0,030	ELAST.			301	-0,031	ELAST.			302	-0,030	ELAST.			302	-0,030	ELAST.
303	-0,030	ELAST.			304	-0,031	ELAST.			305	-0,031	ELAST.			305	-0,031	ELAST.
306	-0,030	ELAST.			307	-0,030	ELAST.			308	-0,030	ELAST.			308	-0,030	ELAST.
309	-0,031	ELAST.			310	-0,030	ELAST.			311	-0,031	ELAST.			311	-0,031	ELAST.
312	-0,034	ELAST.			313	-0,033	ELAST.			314	-0,031	ELAST.			314	-0,031	ELAST.
315	-0,033	ELAST.			316	-0,035	ELAST.			317	-0,037	ELAST.			317	-0,037	ELAST.
318	-0,033	ELAST.			319	-0,030	ELAST.			320	-0,031	ELAST.			320	-0,031	ELAST.
321	-0,031	ELAST.			322	-0,030	ELAST.			323	-0,030	ELAST.			323	-0,030	ELAST.
324	-0,038	ELAST.			325	-0,042	ELAST.			326	-0,045	ELAST.			326	-0,045	ELAST.
327	-0,042	ELAST.			328	-0,039	ELAST.			329	-0,035	ELAST.			329	-0,035	ELAST.
330	-0,032	ELAST.			331	-0,034	ELAST.			332	-0,038	ELAST.			332	-0,038	ELAST.
333	-0,030	ELAST.			334	-0,030	ELAST.			335	-0,030	ELAST.			335	-0,030	ELAST.
336	-0,029	ELAST.			337	-0,030	ELAST.			338	-0,031	ELAST.			338	-0,031	ELAST.
339	-0,029	ELAST.			340	-0,029	ELAST.			341	-0,031	ELAST.			341	-0,031	ELAST.
342	-0,031	ELAST.			343	-0,032	ELAST.			344	-0,031	ELAST.			344	-0,031	ELAST.
345	-0,030	ELAST.			346	-0,031	ELAST.			347	-0,032	ELAST.			347	-0,032	ELAST.
348	-0,030	ELAST.			349	-0,029	ELAST.			350	-0,029	ELAST.			350	-0,029	ELAST.
351	-0,030	ELAST.			352	-0,029	ELAST.			353	-0,030	ELAST.			353	-0,030	ELAST.
354	-0,030	ELAST.			355	-0,031	ELAST.			356	-0,034	ELAST.			356	-0,034	ELAST.
357	-0,037	ELAST.			358	-0,030	ELAST.			359	-0,029	ELAST.			359	-0,029	ELAST.
360	-0,029	ELAST.			361	-0,030	ELAST.			362	-0,032	ELAST.			362	-0,032	ELAST.
363	-0,030	ELAST.			364	-0,029	ELAST.			365	-0,029	ELAST.			365	-0,029	ELAST.
366	-0,029	ELAST.			367	-0,029	ELAST.			368	-0,030	ELAST.			368	-0,030	ELAST.
369	-0,031	ELAST.			370	-0,032	ELAST.			371	-0,033	ELAST.			371	-0,033	ELAST.
372	-0,035	ELAST.			373	-0,038	ELAST.			374	-0,037	ELAST.			374	-0,037	ELAST.
375	-0,036	ELAST.			376	-0,033	ELAST.			377	-0,036	ELAST.			377	-0,036	ELAST.
378	-0,035	ELAST.			379	-0,035	ELAST.			380	-0,033	ELAST.			380	-0,033	ELAST.
381	-0,032	ELAST.			382	-0,036	ELAST.			383	-0,032	ELAST.			383	-0,032	ELAST.
384	-0,029	ELAST.			385	-0,029	ELAST.			386	-0,031	ELAST.			386	-0,031	ELAST.
387	-0,030	ELAST.			388	-0,029	ELAST.			389	-0,031	ELAST.			389	-0,031	ELAST.
390	-0,030	ELAST.			391	-0,029	ELAST.			392	-0,030	ELAST.			392	-0,030	ELAST.
393	-0,033	ELAST.			394	-0,037	ELAST.			395	-0,037	ELAST.			395	-0,037	ELAST.
396	-0,034	ELAST.			397	-0,032	ELAST.			398	-0,030	ELAST.			398	-0,030	ELAST.
399	-0,029	ELAST.			400	-0,030	ELAST.			401	-0,030	ELAST.			401	-0,030	ELAST.
402	-0,031	ELAST.			403	-0,032	ELAST.			404	-0,031	ELAST.			404	-0,031	ELAST.
405	-0,031	ELAST.			406	-0,032	ELAST.			407	-0,031	ELAST.			407	-0,031	ELAST.
408	-0,031	ELAST.			409	-0,032	ELAST.			410	-0,032	ELAST.			410	-0,032	ELAST.
411	-0,032	ELAST.			412	-0,031	ELAST.			413	-0,031	ELAST.			413	-0,031	ELAST.
414	-0,030	ELAST.			415	-0,030	ELAST.			416	-0,031	ELAST.			416	-0,031	ELAST.
417	-0,032	ELAST.			418	-0,032	ELAST.			419	-0,031	ELAST.			419	-0,031	ELAST.
420	-0,033	ELAST.			421	-0,034	ELAST.			422	-0,032	ELAST.			422	-0,032	ELAST.
423	-0,033	ELAST.			424	-0,032	ELAST.			425	-0,030	ELAST.			425	-0,030	ELAST.
426	-0,037	ELAST.			427	-0,036	ELAST.			428	-0,033	ELAST.			428	-0,033	ELAST.
429	-0,032	ELAST.			430	-0,032	ELAST.			431	-0,039	ELAST.			431	-0,039	ELAST.
432	-0,029	ELAST.			433	-0,031	ELAST.			434	-0,030	ELAST.			434	-0,030	ELAST.
435	-0,029	ELAST.			436	-0,031	ELAST.			437	-0,030	ELAST.			437	-0,030	ELAST.
438	-0,029	ELAST.			439	-0,029	ELAST.			440	-0,035	ELAST.			440	-0,035	ELAST.
441	-0,030	ELAST.			442	-0,031	ELAST.			443	-0,030	ELAST.			443	-0,030	ELAST.
444	-0,042	ELAST.			445	-0,038	ELAST.			446	-0,046	ELAST.			446	-0,046	ELAST.
447	-0,033	ELAST.			448	-0,033	ELAST.			449	-0,033	ELAST.			449	-0,033	ELAST.
450	-0,036	ELAST.			451	-0,034	ELAST.			452	-0,032	ELAST.			452	-0,032	ELAST.
453	-0,032	ELAST.			454	-0,033	ELAST.			455	-0,036	ELAST.			455	-0,036	ELAST.
456	-0,033	ELAST.			457	-0,035	ELAST.			458	-0,037	ELAST.			458	-0,037	ELAST.
459	-0,039	ELAST.			460	-0,035	ELAST.			461	-0,038	ELAST.			461	-0,038	ELAST.
462	-0,038	ELAST.			463	-0,041	ELAST.			464	-0,041	ELAST.			464	-0,041	ELAST.
465	-0,044	ELAST.			466	-0,030	ELAST.			467	-0,029	ELAST.			467	-0,029	ELAST.
468	-0,029	ELAST.			469	-0,029	ELAST.			470	-0,030	ELAST.			470	-0,030	ELAST.
471	-0,030	ELAST.			472	-0,030	ELAST.			473	-0,031	ELAST.			473	-0,031	ELAST.
474	-0,030	ELAST.			475	-0,029	ELAST.			476	-0,029	ELAST.			476	-0,029	ELAST.
477	-0,030	ELAST.			478	-0,030	ELAST.			479	-0,033	ELAST.			479	-0,033	ELAST.
480	-0,033	ELAST.			481	-0,036	ELAST.			482	-0,035	ELAST.			482	-0,035	ELAST.
483	-0,034	ELAST.			484	-0,037	ELAST.			485	-0,037	ELAST.			485	-0,037	ELAST.
486	-0,034	ELAST.			487	-0,030	ELAST.			488	-0,029	ELAST.			488	-0,029	ELAST.
489	-0,030	ELAST.			490	-0,032	ELAST.			491	-0,033	ELAST.			491	-0,033	ELAST.
492	-0,035	ELAST.			493	-0,030	ELAST.			494	-0,038	ELAST.			494	-0,038	ELAST.
495	-0,037	ELAST.			496	-0,032	ELAST.			497	-0,031	ELAST.			497	-0,031	ELAST.
498	-0,031	ELAST.			499	-0,035	ELAST.			500	-0,033	ELAST.			500	-0,033	ELAST.
501	-0,032	ELAST.			502	-0,034	ELAST.			503	-0,035	ELAST.			503	-0,035	ELAST.
504	-0,034	ELAST.			505	-0,036	ELAST.			506	-0,040	ELAST.			506	-0,040	ELAST.
507	-0,037	ELAST.			508	-0,025	ELAST.			509	-0,031	ELAST.			509	-0,031	ELAST.
510	-0,032	ELAST.			511	-0,025	ELAST.			512	-0,026	ELAST.			512	-0,026	ELAST.
513	-0,021	ELAST.			514	-0,020	ELAST.			515	-0,020	ELAST.			515	-0,020	ELAST.
516	-0,019	ELAST.			517	-0,017	ELAST.			518	-0,032	ELAST.			518	-0,032	ELAST.
519	-0,027	ELAST.			520	-0,034	ELAST.			521	-0,021	ELAST.			521	-0,021	ELAST.
522	-0,019	ELAST.			523	-0,028	ELAST.			524	-0,026	ELAST.			524	-0,026	ELAST.
525	-0,039	ELAST.			526	-0,037	ELAST.			527	-0,025	ELAST.			527	-0,025	ELAST.
528	-0,019	ELAST.			529	-0,017	ELAST.			530	-0,048	ELAST.			530	-0,048	ELAST.
531	-0,048	ELAST.			532	-0,036	ELAST.			533	-0,050	ELAST.			533	-0,050	ELAST.
534	-0,037	ELAST.			535	-0,029	ELAST.			536	-0,017	ELAST.			536	-0,017	ELAST.
537	-0,020	ELAST.			538	-0,022	ELAST.			539	-0,018	ELAST.			539	-0,018	ELAST.
540	-0,019	ELAST.			541	-0,020	ELAST.			542	-0,026	ELAST.			542	-0,026	ELAST.

Studio Tecnico Ing. Antonino Tricoli

SOFTWARE: C.D.G. - Computer Design Geo Structures - Rel.2020 - Lic. Nro: 5138

RELAZIONE GEOTECNICA

PORTANZA GLOBALE PIASTRE - ABBASSAMENTI COMBINAZ.: SLD/1

		DRENATE		NON DRENATE				DRENATE		NON DRENATE				DRENATE		NON DRENATE	
Nodo3d N.ro	SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI	Nodo3d N.ro	SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI	Nodo3d N.ro	SpostZ (cm)	SpostZ/ SpostEI	SpostZ (cm)	SpostZ/ SpostEI	Nodo3d N.ro	SpostZ (cm)	SpostZ/ SpostEI
543	-0,028	ELAST.			544	-0,037	ELAST.			545	-0,049	ELAST.					
546	-0,052	ELAST.			547	-0,039	ELAST.			548	-0,048	ELAST.					
549	-0,045	ELAST.			550	-0,041	ELAST.			551	-0,041	ELAST.					
552	-0,041	ELAST.			553	-0,040	ELAST.			554	-0,040	ELAST.					
555	-0,040	ELAST.			556	-0,041	ELAST.			557	-0,039	ELAST.					
558	-0,039	ELAST.			559	-0,042	ELAST.			560	-0,033	ELAST.					
561	-0,042	ELAST.			562	-0,025	ELAST.			563	-0,020	ELAST.					
564	-0,020	ELAST.			565	-0,026	ELAST.			566	-0,038	ELAST.					
567	-0,052	ELAST.			568	-0,046	ELAST.			569	-0,043	ELAST.					
570	-0,040	ELAST.			571	-0,039	ELAST.			572	-0,043	ELAST.					
573	-0,039	ELAST.			574	-0,039	ELAST.			575	-0,038	ELAST.					
576	-0,042	ELAST.			577	-0,040	ELAST.			578	-0,038	ELAST.					
579	-0,038	ELAST.			580	-0,038	ELAST.			581	-0,038	ELAST.					
582	-0,038	ELAST.			583	-0,038	ELAST.			584	-0,050	ELAST.					
585	-0,042	ELAST.			586	-0,036	ELAST.			587	-0,036	ELAST.					
588	-0,038	ELAST.			589	-0,040	ELAST.			590	-0,042	ELAST.					
591	-0,044	ELAST.			592	-0,047	ELAST.			593	-0,044	ELAST.					
594	-0,029	ELAST.			595	-0,035	ELAST.			596	-0,023	ELAST.					
597	-0,020	ELAST.			598	-0,021	ELAST.			599	-0,027	ELAST.					
600	-0,038	ELAST.			601	-0,050	ELAST.										